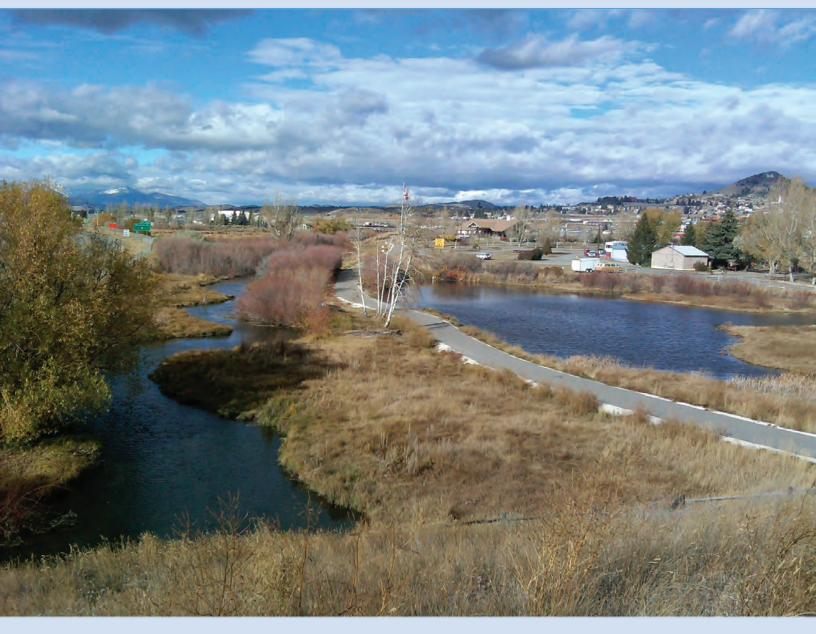
Montana Bureau of Mines and Geology Report of Investigation 22



STREAM CHARACTERIZATION OF BLACKTAIL AND SILVER BOW CREEKS:

A CONTINUOUS TRACER INJECTION INVESTIGATION CONDUCTED DURING BASEFLOW CONDITIONS IN AN URBAN AREA IMPACTED BY MINING: BUTTE, MONTANA



Nicholas J. Tucci 2014 Stream Characterization of Blacktail and Silver Bow Creeks, a Continuous Tracer Injection Investigation Conducted during Baseflow Conditions in an Urban Area Impacted by Mining: Butte, Montana

> MBMG Report of Investigation 22 Nicholas J. Tucci 2014

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LIST OF ACRONYMS

As-Arsenic AR-British Petroleum Atlantic Richfield Company **BTC**—Blacktail Creek Br–Bromide BMFOU—Butte Mine Flooding Operable Unit BPSOU-Butte Priority Soil Operable Unit °C-Degree centigrade Cd-Cadmium COCs-Contaminants of Concern cfs-cubic feet per second Cu-Copper EPA—Environmental Protection Agency Hg–Mercury ICP-MS-Inductively coupled plasma-mass spectrometry Kg-Kilogram L-Liter NaBr-Sodium bromide µg/L-Microgram per liter mg/L-Milligram per liter MBMG—Montana Bureau of Mines and Geology MDEQ-Montana Department of Environmental Quality MSD-Metro Storm Drain MSD-Subdrain-Metro Storm Drain-Subdrain NRD—Natural Resource Damages Program Pb-Lead SBC—Silver Bow Creek SBC/MSD-Upper Silver Bow Creek/Metro Storm Drain TR-Total recoverable Zn-Zinc

EXECUTIVE SUMMARY

In September 2011, scientists from the Montana Bureau of Mines and Geology conducted a continuous bromide tracer injection in the Blacktail Creek/Upper Silver Bow Creek confluence area in Butte, Montana. This work was funded by the Natural Resource Damage Program and performed during baseflow conditions, when groundwater contributions to surface-water flow were dominant. Blacktail Creek is the headwater stream for Upper Silver Bow Creek, which receives the majority of its baseflow contributions from Summit Valley groundwater in Butte, Montana. The stream is of interest because it intersects both the Butte Area One injured area restoration site and the Butte Priority Soils Operable Unit of the Silver Bow Creek/Butte Area National Priority List site, and is a focal point for past and current remediation/restoration activities.

The work evaluated streamflow, chemistry, metals loading, and groundwater/surface-water interactions in a reach of stream impacted by more than a century of mining- and milling-related activities, land development, land-use change, and streambed manipulation. A continuous tracer injection test was performed using a sodium bromide solution with a bromide concentration of 22.5 percent wt/wt to obtain creek bromide concentrations of roughly 3 mg/L. Manual measurements of discharge were obtained at 15 sites over a total stream length of 10,500 ft using a SonTek FlowTracker. Steady-state conditions with respect to bromide were reached after 11 h of injection. The tracer results were combined with synoptic sampling of mainstem, tributary, and drivepoint piezometer data. Samples from 30 groundwater wells, 17 mainstem locations, 8 tributary locations, and 5 drivepoint piezometer locations in the Blacktail streambed and two wetland sites were analyzed for bromide, common cations and anions, and 36 minor and trace analytes.

Results from the tracer injection and manual FlowTracker measurements were consistent, and suggest that discharge in Blacktail Creek between Oregon Avenue and George Street increased by 2.2 cfs (22 percent). Wetlands located adjacent to Blacktail Creek received the majority (99%) of recharge from local groundwater sources, and contributed 39 percent of the flow increase observed in the studied reach of Blacktail Creek (Oregon Avenue to George Street). The remaining baseflow contributions (61%) in Blacktail Creek were groundwater inputs into the stream. Results of the tracer study also indicate that two reaches of Blacktail Creek are non-gaining reaches, and may be net-losing reaches. Gains in streamflow were not observed in the upper reach of Silver Bow Creek, from the confluence to site SS-06. Gains in flow were not observed in Upper Silver Bow Creek.

Results from metals loading assessments indicate that while there appears to be source areas for copper and zinc loading to the stream, contaminants of concern (As, Cd, Cu, Pb, and Zn) concentrations remained below DEQ-7 acute and chronic life standards for dissolved concentrations throughout the study area. Total recoverable Cu and Zn concentrations were elevated in the Kaw Avenue reach of Blacktail Creek. One mainstem, one wetland, and two tributary samples exceeded DEQ-7 acute and chronic life standards for total recoverable Cu, while two tributary samples exceeded DEQ-7 acute and chronic life standards for total recoverable Cu, while two tributary samples exceeded DEQ-7 acute and chronic life standards for total recoverable zinc. The sources of total recoverable Cu and Zn to this area of Blacktail Creek are thought to be either bed sediment loads or nearby streambank sediment (i.e., BTC Berm) loading from historic Grove Gulch discharges. The two wetlands, located north of Blacktail Creek and adjacent to Kaw Avenue, exhibited water quality with elevated concentrations of copper and zinc. Both of the wetlands contributed measurable flow into Blacktail Creek and are potential point sources; however, metals concentrations of the groundwater that recharged the wetlands near Kaw Avenue were not assessed during this investigation. Therefore, groundwater entering the wetlands could not be ruled out as a potential source.

1.0 INTRODUCTION

The floodplains of lower Blacktail (BTC) and upper Silver Bow (SBC) Creeks in Butte traverse the southern flank of the Butte Priority Soils Operable Unit (BPSOU; fig. 1; EPA, 2006). Both floodplains have been heavily impacted by a century of mining operations that resulted in the deposition of metalladen tailings deposits [arsenic (As), cadmium (Cd), copper (Cu), mercury (Hg), lead (Pb), and zinc (Zn)] that serve as point sources of contamination to groundwater and surface water. To qualify and quantify known sources of Cu and Zn to surface water, synoptic sampling of groundwater and surface water was conducted during a tracer injection test under baseflow conditions (September 2011).

1.1 Site Background

Due to a varying array of water-management practices and water-demand issues (mining processes, milling processes, smelting processes, urbanization, and post-mining remediation efforts), the Silver Bow Creek and Blacktail Creek stream channel geographic setting, morphology, and hydrologic integrity have been heavily modified.

1.1.1 Blacktail Creek

Blacktail Creek is a north-northwest-flowing intermontane stream that drains the southern Summit Valley, and currently serves as the headwater stream for the Silver Bow Creek drainage basin. In Butte, tributaries to Blacktail Creek include Basin Creek, Sand Creek, Grove Gulch, and a series of wetlands located adjacent to the creek. The wetlands (fig. 1), both natural and constructed, are fed by groundwater from the north and south Summit Valley. Today, the perennial reach of Silver Bow Creek is formed just upstream of Montana Street (fig. 1) at the confluence of Blacktail Creek and the Upper Silver Bow Creek/Butte Metro Storm Drain (SBC/MSD), a dry streambed that historically drained the northern Summit Valley (fig. 1) and currently serves as a storm-water management channel.

1.1.2 Silver Bow Creek

In its upper reaches, Silver Bow Creek historically flowed southward from the confluence of two headwater streams, Yankee Doodle Gulch and Dixie

Gulch. As the creek continued south along the base of the Butte Hill, its valley widened as tributaries out of gulches from the East Ridge (Park Canyon and Horse Canyon, fig. 2A) joined the mainstem. Silver Bow Creek's channel then turned westward around the base of the ridge on the east end of the Butte Hill. As the creek flowed along the base of the Butte Hill, it entered the middle reaches of the Summit Valley, a marshy environment where it joined Blacktail Creek, in an area colloquially referred to as the 'confluence area.' Excavation and dewatering of the Berkeley Pit (1955), construction of the Weed Concentrator, and formation of the Yankee Doodle Tailings Impoundment Dam (May 1963) physically isolated the northernmost part of the Summit Valley, and these historic hydrologic conditions no longer exist. The historic headwaters of Silver Bow Creek have been filled by material excavated from the Berkeley Pit, and a local groundwater divide north of Harrison Avenue forms the northeastern boundary of the current Silver Bow Creek Drainage Basin (Tucci, 2010; EPA, 2011).

The former course of upper Silver Bow Creek that drained the north part of the valley (the Butte Hill, south of the Berkeley Pit between Montana Street and the Continental Drive) was extensively altered by a public works project in the 1930s. This action channelized the streambed for use as an industrial sewer and to collect storm-water runoff (Quivik, 1998). Today, this area is the primary focus for ongoing remediation efforts for BPSOU (EPA, 2006; EPA, 2011b), and is now referred to as the Metro Storm Drain (MSD) (fig. 1). A French-drain collection system, known as the Metro Storm Drain Subdrain (MSD Subdrain), buried directly under the current MSD channel, extends from the Civic Center to a pumping vault west of Kaw Avenue (fig. 1). The MSD Subdrain was designed to capture shallow contaminated groundwater and prevent it from discharging to surface water; dewatering and construction began in 2003 and the drain became operational in 2005 (EPA, 2006). The MSD Subdrain has had profound impacts on the hydrogeologic and hydrologic setting in the BTC/SBC confluence area (Tucci and Icopini, 2010, 2012).

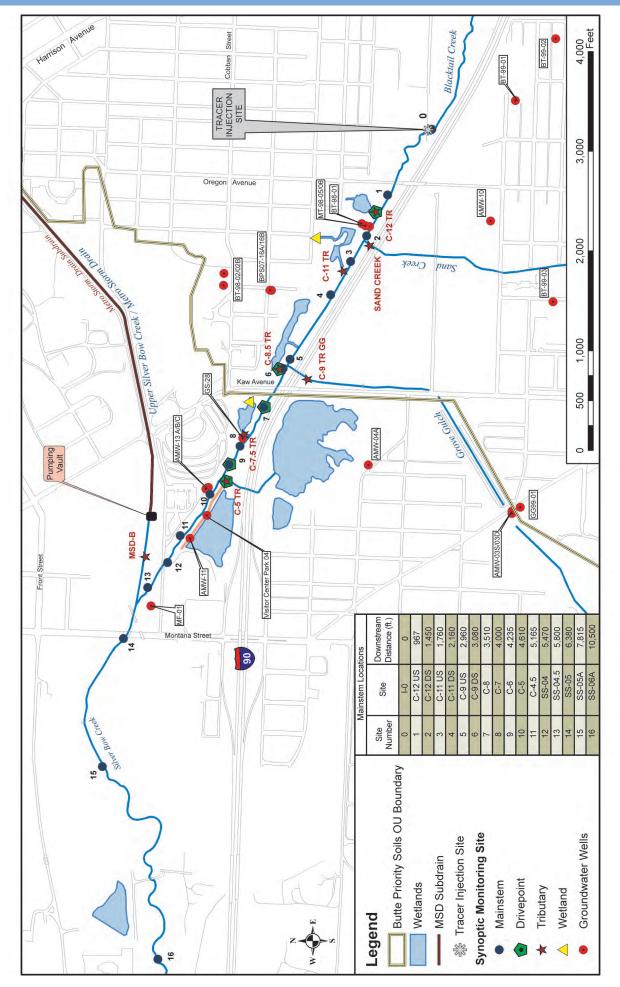


Figure 1. Location map showing tracer injection site, synoptic sampling locations, and groundwater monitoring wells. Mainstem site numbers labeled with black text. Tributary synoptic sampling sites labeled with dark red text. Survey source data: MBMG Navigational Grade GPS. Imagery: 2009 NAIP, Silver Bow County. Projection: NAD 83 Decimal Degrees.

1.1.3 Blacktail Creek/Silver Bow Creek Confluence Area

The pre-mining setting of the Blacktail/Silver Bow Creek confluence was described as a low-flow, low-gradient wetland environment with "luxuriant growth of grass and vegetation" (Meinzer, 1914). Many of Butte's earliest settlers reported that the valley was "swampy and peaty" before mining occurred (Meinzer, 1914). At present, an organic-rich silt layer remains throughout the BTC/SBC confluence area, although it is buried under varying quantities of fill and waste material. When identified in borehole logs, the organic silt is used by geoscientists to determine the valley's pre-mining original soil horizon (Tucci, 2012).

In 1879, the first large-scale mineral processing smelter (Colorado Smelter) was built on Silver Bow Creek, at the west end of the valley (fig. 2B; Ray and Leonard, 1890). Between 1879 and 1888, at least three more smelters of consequence (Butte Reduction Works, Parrot Smelter, and Montana Ore Purchasing; fig. 2A; Weed, 1904) were constructed, significantly altering the morphology and hydrology of both creeks. Water demands during this time increased dramatically, and at least six dams were constructed for water impoundment and tailings retention purposes (fig. 2B). Blacktail Creek, as far upstream as Harrison Avenue, was converted from a meandering stream to a linear channel in an effort to deliver more water to downstream smelters (Simons, 1915). By 1912, most smelting operations had been moved to Anaconda, and the industrial water demands in Butte declined (Quivik, 1998).

The consequences of aggradation in the confluence area caused by the construction of retention dams on Blacktail and Silver Bow Creeks were significant and are apparent today. Retained water soon became a flooding issue (Meinzer, 1914). Flood control berms adjacent to the streambeds were constructed from readily available mine-waste material. One berm, referred to as the 'BTC berm' (fig. 1), presents a potential point source of contamination to Blacktail Creek. Aggradation from the dam near Montana Street (fig. 2B; Weed, 1895), constructed sometime between 1890 and 1895, caused the BTC/SBC confluence to shift several hundred feet to the northwest (fig. 2C). By the late 1930s, all retention dams on Silver Bow and Blacktail Creeks were removed, and both streambeds were channelized to the extent to which they are geographically represented today. Current conditions bear no resemblance to the pre-mining morphology of the streambeds or the historic hydrologic environment (fig. 2C).

1.1.4 Grove Gulch

Grove Gulch (fig. 1, which joins Blacktail Creek east of Lexington Avenue) begins in mostly rolling open range land approximately 4 mi southwest of the city of Butte. Water from Grove Gulch currently enters Blacktail Creek approximately 75 ft upstream of the Lexington Avenue overpass (fig. 1). The creek has been heavily altered; the earliest recorded anthropogenic manipulation dates back to January 1879, when the five-stamp Grove Gulch Mill, located between Mount Moriah Cemetery and Timber Butte, began processing eight tons of ore per day (Wilcox, 1954).

Currently the stream is an intermittent tributary to Blacktail Creek, contributing negligible volumes during baseflow and low-to-moderate volumes during runoff events (unpublished BPSOU surfacewater monitoring data, Trek Environmental written commun., March 25, 2011). However, the current hydrologic conditions of Grove Gulch were not always the case. Historically, Grove Gulch discharged to Silver Bow Creek (fig. 2B; near the Butte Reduction Works) roughly 4,000 ft west of the confluence area. Operations at Clark's Timber Butte zinc mill began in 1914, and as a result, flow from Grove Gulch was routed underneath the Clark tailings impoundment by a combination of vitrified tile and wood stave pipes (Hydrometrics, 1983). At this time, during construction of the mill, the stream was redirected from its confluence with Silver Bow Creek upstream to its current confluence with Blacktail Creek (Simons, 1915).

Clark's zinc mill at Timber Butte operated between 1914 and 1949, generating roughly a million cubic yards of tailings that were poorly impounded within the Grove Gulch floodplain at the base of Timber Butte (Quivik, 1993). After closure of the mill, most ephemeral tributaries draining the north face of Timber Butte were allowed to discharge directly through the Clark Tailings. As a result, substantial erosion of the tailings into Grove Creek occurred

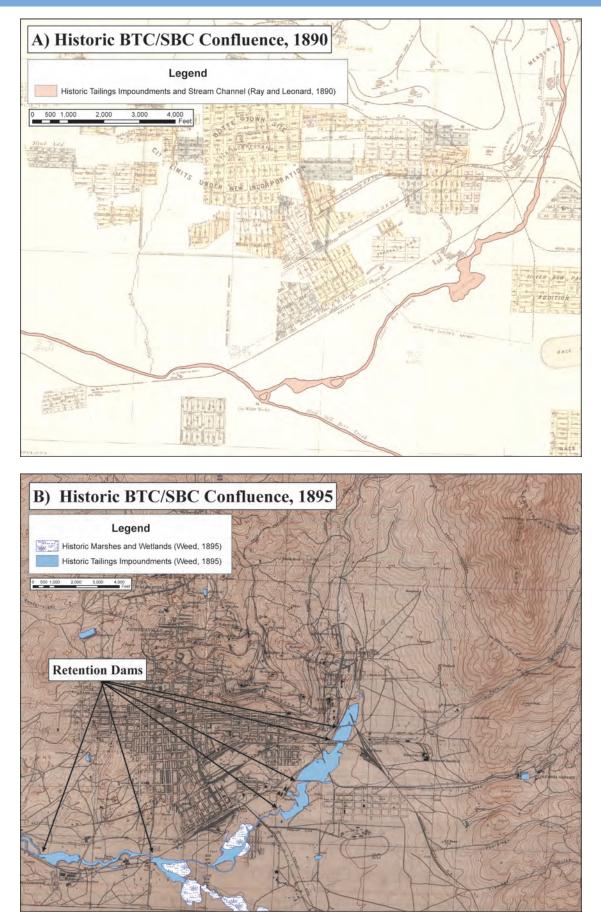


Figure 2. Time-series maps of the BTC/SBC confluence area demonstrating the significance of anthropogenic manipulation of the stream channels between 1890 (A), 1895 (B), and present day (C). The 1890 (pink) and 1895 (light blue) stream channels are overlain on present-day SBC/BTC creeks (dark blue) for comparison (C).

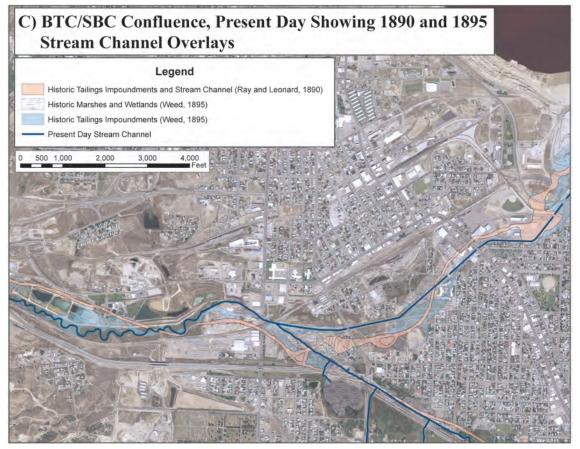


Figure 2, continued.

(Hydrometrics, 1983). Although Grove Creek is an ephemeral stream, large to moderate runoff events (fig. 3) that occurred prior to reclamation activities transported large volumes of tailings downstream, causing degradation in Blacktail Creek. Today the Clark Tailings are reclaimed and are part of a capped repository; however, the historic metal-laden tailings deposits to lower Grove Gulch and Blacktail Creek in streambank and streambed sediments may still be a point source of contamination to surface water.

Two large-scale remedial actions were implemented in upper Grove Gulch. The Grove Creek Flood Prevention Project was constructed in 1982 to correct



Figure 3. Grove Gulch streamflow at Rowe Road during a large run-off event in 1995. Picture taken at the gauging station on the south side of Rowe Road shows streamflows overtopping the weir. Historically (pre-1982), large sediment loads were transported into Blacktail Creek during similar events.

flooding and sediment deposition problems caused by the historic placement of the Clark Tailings in the stream's floodplain. Prior to this construction, materials that eroded from the Clark Tailings site were transported and deposited downstream to lower Grove Creek and Blacktail Creek (Hydrometrics, 1983). A 1-million cubic yard stabilized mine waste impoundment and a low-permeability cap were constructed to permanently contain the Clark Tailings in 1998 (Archibald and others, 2003). The tailings that deposited in lower Grove Gulch (from the tailings impoundment to the confluence) and within Blacktail Creek have been left in place, and have not been characterized.

1.1.5 Non-mining stream channel management of Blacktail and Silver Bow Creeks

Historic mining practices were not the only anthropogenic activities that altered the hydrology of the area. Interstate 90 (fig. 1) was constructed through the low-lying wetland area in 1962 (Montana Department of Transportation Aerial Photograph, 1962). Most likely both streambeds were manipulated to accommodate for the infrastructure improvement. The weight of the fill and infrastructure, and subsequent compaction of the alluvial material, most likely altered flow paths and mounded groundwater on both sides of the interstate.

Other than the aforementioned construction of the MSD Subdrain, which altered groundwater flow paths and most likely altered stream hydrology, wetlands have been reconstructed in the lower reach of Blacktail Creek. A large restoration project conducted in the late 1990s by the Montana Economic Revitalization and Development Institute enhanced a series of natural wetlands on the north side of Blacktail Creek between Harrison Avenue and George Street (fig. 1). Many of these wetlands receive groundwater originating from the northeastern portion of the Summit Valley and, prior to this investigation, the water quality of these wetlands were unknown.

1.2 Recent Investigations

Comprehensive monitoring programs were established for Blacktail and Silver Bow Creeks as part of ongoing Superfund-related activities. Surface water has been sampled for water quality on a frequent and consistent basis as part of the Consent Decree monitoring plan for the Butte Mine Flooding Operable Unit (BMFOU; EPA, 2002), and as an interim groundwater monitoring plan for BPSOU (EPA, 2012). Surface-water monitoring activities performed under BMFOU have been conducted since 1983; analytical data are available on the USGS website (http://waterdata.usgs.gov/nwis). Monitoring for BPSOU commenced on a more frequent and consistent basis in 2007; the most recent synopsis of these data was published in 2008 [Environmental Protection Agency (EPA), 2008]. Large datasets have been generated from these comprehensive monitoring programs. In addition, data from several narrowly scoped and focused synoptic sampling events conducted by the Montana Bureau of Mines and Geology (MBMG) has been released through informal reports to the Natural Resources Damages Program (NRD; Tucci, 2006, 2007, 2008) Basic data used in these reports also are available at the MBMG's online database (http://mbmggwic.mtech. edu).

Tucci and Icopini (2012) demonstrated that a source of Cu and Zn loading is present in Blacktail Creek between Oregon Avenue and Montana Street (fig. 1). Three unpublished synoptic sampling events conducted between 2006 and 2010 by the MBMG demonstrate similar results. Subsequent synoptic sampling conducted by the USGS (August 2010, unpublished MBMG split sampling data) showed results consistent with those found by Tucci and Icopini (2012). A review of data for BPSOU, a more comprehensive and extensive dataset for surface water, reveals that the impacts to water quality from this source is intermittent (unpublished BPSOU data, Trek Environmental, oral commun., March 25, 2011).

1.3 Objectives

In September 2011, scientists from the MBMG, with assistance from faculty of Montana Tech of the University of Montana, employees of the Montana Department of Environmental Quality (MDEQ), Trek Environmental [consultants for ARCO (AR)], and CDM-Smith (consultants for the EPA) conducted a series of surface-water/groundwater interaction investigations in Lower Blacktail and Upper Silver Bow Creeks in Butte, Montana. These investigations included synoptic groundwater sampling, streambed drivepoint sampling, and surface-water sampling of mainstem, tributaries, and wetlands samples. These activities were conducted during a continuous-injection sodium bromide (NaBr) tracer investigation in Lower Blacktail and Upper Silver Bow Creeks. The main objectives of the work were to:

- (1) Characterize gaining reaches of Blacktail Creek and Silver Bow Creek,
- (2) Determine the quantity and quality of groundwater entering the stream within this reach,
- (3) Characterize the water quality of tributaries entering the stream in this reach,
- (4) Isolate the reach of Blacktail Creek receiving Cu and Zn loading, and attempt to determine source areas, and
- (5) Quantify and qualify sources of metals loading to Blacktail and Silver Bow Creeks, if possible.

2.0 METHODS

2.1 Field Procedures

To quantify and qualify any sources of metals loading to Blacktail and Silver Bow Creeks, synoptic sampling was conducted during tracer injection under baseflow conditions (September 2011). The continuous tracer injection method (Kilpatrick and Cobb, 1985; Kimball, 1997; Wright and Moore, 2003) produces accurate flow calculations for the quantification of spatial, physical, and chemical profiles in stream environments.

Previous monitoring activity shows that the current study area along Blacktail Creek is a gaining reach. During baseflow conditions, significant increases in flow (20–40%) have been observed within the reach between Harrison Avenue and George Street (Unpublished BPSOU data, Trek Environmental, written commun., March 25, 2011). Both groundwater and surface water (Sand Creek, Grove Gulch, and numerous wetlands to the north and south of Blacktail Creek) inputs exist, all of which present themselves as possible sources of metal loading to Blacktail Creek. The current study was designed to quantify flow in this reach, identify the contribution of various inputs to the creek, and identify possible sources for metal loading.

Field methods and analytical procedures were published (appendix A) prior to the onset of this investigation and submitted for review by the federal (EPA) and State (MDEQ, NRD) agencies. A copy of the sampling and analysis plan (SAP) was also submitted to AR. The published SAP (appendix A), which outlines all field and analytical procedures, is included as appendix A of this report.

2.1.1 Tracer Injection Test

A concentrated bromide stock solution [Br = 312,000 mg/L] was prepared by mixing 220 kilograms (Kg) of sodium bromide with 750 liters (L) of upgradient Blacktail Creek water (fig. 4A). The injection site (fig. 1) was chosen to ensure an adequate mixing zone prior to the first downstream monitoring site. Constant injection rates (0.2 L/min) were maintained using a Cole Palmer L/S variable speed peristaltic pump (fig. 4B); the Br tracer solution was injected via flexible silicone tubing into Blacktail Creek at two points along the same stream transect (fig. 4C). During injection, an ISCO automated sampler was used to collect hourly surface-water samples at a downstream site (Montana Street, fig. 1) on Silver Bow Creek, and a bromide ion-selective probe was used to measure in-stream Br concentrations to ensure Br saturation prior to synoptic sampling.

Tracer injection began on September 20, 2012 at 07:45 h and continued at a constant rate until September 21, 2012 at 16:45 h. The injection rates were measured via bucket-and-stopwatch method at hourly intervals. Synoptic sampling of surface water began on September 21, 2012 at 08:15 h and continued until September 21, 2012 at 13:32 h.

2.1.2 Stream Discharge

Stream discharge was measured at mainstem sites and some tributaries using a SonTek Handheld-ADV FlowTracker. Discharge from small tributary sites (fig. 1; C-5TR, C-8.5 TR) was measured with Parshall flumes. Field crews from MBMG and Trek Environmental were responsible for measuring discharge.

2.1.3 Synoptic Sample Collection

Synoptic water-quality samples of mainstem, tributary, and wetland sites in Blacktail and Silver Bow Creeks were collected by MBMG personnel 24.5 h after tracer injection commenced, and all sampling activities were completed within 5 h. In all, 17 mainstem, 8 tributary, and 2 wetland samples



Figure 4. Bromide-tracer injection site on Blacktail Creek: (A) bulk injection tank containing 22.5% Br tracer solution. (B) A constant injection rate (0.2 L/min) was maintained via variable-speed peristaltic pump. (C) Tracer was injected into a stream transect via plastic tube containing two discharge points. (D) Bulk, 1-gal synoptic samples collected by MBMG sampling team were transported to the MBMG sample processing team located at the injection site for processing and preservation.

GWIC No.	Downstream Distance (ft)	Site	Туре	GWIC No.	Downstream Distance (ft)	Site	Туре
262809	0	I-0 C-12	Mainstem	217884	10,500	SS-06A	Mainstem
262796	967	US C-12	Mainstem	262795	1,201	C-12 TR SAND	Tributary
262793	1,450	DS C-11	Mainstem	262812	1,527	CREEK	Tributary
262791	1,760	US C-11	Mainstem	262790	1,910	C-11 TR	Tributary
262789	2,160	DS	Mainstem	262808	3,035	C-9 TR GG	Tributary
262807	2,960	C-9 US	Mainstem	262805	3,130	C-8.5 TR	Tributary
262806	3,080	C-9 DS	Mainstem	262803	3,717	C-7.5 TR	Tributary
262804	3,510	C-8	Mainstem	262799	4,770	C-5 TR	Tributary
262801	4,000	C-7	Mainstem	262811	5,343	MSD-B	Tributary
262800	4,235	C-8	Mainstem	262802	3,700	C-7.5 POND	Wetland
262798	4,610	C-9	Mainstem	262795	1,190	C-12 TR	Wetland
262797	5,165	C-10	Mainstem	262795	1,201	C-12 TR	Drivepoint
127593	5,470	C-11	Mainstem	262805	3,130	C-8.5 TR	Drivepoint
262810	5,800	C-12	Mainstem	262804	3,510	C-8	Drivepoint
127536	6,380	C-13	Mainstem	262803	3,717	C-7.5 TR	Drivepoint
249187	7,815	C-14	Mainstem	262800	4,235	C-6	Drivepoint

Table 1. List of synoptic monitoring sites sampled during tracer injection.

(fig. 1; table 1) were collected using techniques outlined in appendix A. Mainstem samples are defined as composite water samples collected from in-stream sampling locations, in either Blacktail or Silver Bow Creeks. Known tributary locations were bracketed by mainstem sites (fig. 1) in an attempt to differentiate between surface-water and groundwater contributions of discharge to the stream. Bulk 1-gal water-quality samples collected from each site were transported by an MDEQ representative to the MBMG sampling team located at the injection site (fig. 4D). Samples were collected in a downstreamto-upstream order.

Baseline groundwater sampling of monitoring wells (fig. 1) located adjacent to Blacktail and Silver Bow Creeks occurred in February 2011, 6 months prior to the tracer injection. The time lapse between the groundwater sampling and the injection test occurred because inclement weather conditions and abnormally high baseflows in the creek prevented tracer injection until September, when true baseflow conditions were observed. During injection, a field crew from CDM-Smith performed synoptic drivepoint groundwater sampling of streambanks (fig. 5). Streambank groundwater samples were collected using a custom-built stainless steel drivepoint sampling apparatus and a peristaltic pump (fig. 5). Bulk drivepoint samples were transported to the injection site, where aliquots were processed.

2.2 Quantification of Stream Gain

Quantification of metal loads in surface water requires accurate stream discharge measurements that are often difficult to obtain. Flow in gaining intermontane streams can be measured precisely by adding a dye or salt tracer to a stream, measuring the dilution of the tracer as it moves downstream, and calculating the change in flow discharge by the amount of dilution.

Stream discharge is calculated from a tracer injection by the conservation of mass; the mass injected by the pump equals the mass in the stream after accounting for the background concentration. A sodium bromide tracer of 311,860,000 mg/L (22.5% wt/wt) was injected at a constant rate into Blacktail Creek, starting at 7:45 on September 20, 2011. The mass of a tracer or a metal (in mg/s) is the product of the discharge (in L/s) and concentration (in mg/L).



Figure 5. Synoptic drive-point samples of streambank groundwater were collected at five locations during the tracer test. (A) CDM-Smith representative pushing sampler into streambed sediment. (B) CDM-Smith representative attaching tubing to sampler head. Samples were purged via peristaltic pump into bulk 1-gal containers.

Rearranging the equation for the conservation of mass, the flow in the stream downstream from the injection site is:

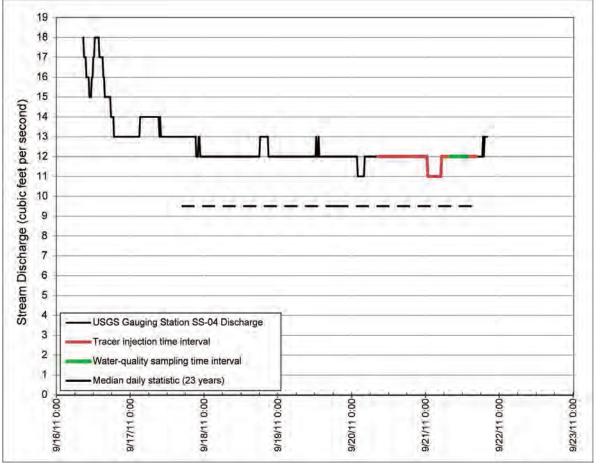
$$\boldsymbol{Q}_{S} = \left(\frac{QiCi}{C_{B}-C_{A}}\right),$$

where Qs is the discharge of the stream, in L/s; Qi is the discharge of the injection solution, in L/s; Ci is the tracer concentration in the injectate solution, in mg/L; C_B is the tracer concentration in the stream downstream from the injection, in mg/L; and C_A is the background concentration of the tracer in the stream upstream from the injection point in mg/L (Kimball and others, 2001).

Background Br concentrations were determined by reviewing historic water-quality reports at sites within the study area (Blacktail Creek @ Oregon, SS-04, and SS-05; GWIC, 2012), an analysis of pre-synoptic surface-water samples with a Br ion-selective probe, and the Br concentration at a site upgradient of the tracer injection site. A review of background Br concentrations in Blacktail Creek revealed that concentrations between Oregon Avenue and Montana Street are below 0.10 mg/L. Using these three techniques, a background concentration of 0.087 mg/L Br was calculated.

3.0 RESULTS

All field and laboratory data collected in this study are available in appendix B (groundwater), appendix C (synoptic sampling data during tracer injection), and appendix D (FlowTracker discharge reports). All chemical analysis of groundwater and surface-water data gathered during this investigation can be found on the MBMG Ground Water Information Center's projects page, Superfund group data, under the name BPSOU2011BTS (http://mbmggwic.mtech.edu). Results of the tracer injection and chemical analysis are presented graphically in figure 6.



Tracer injection began on September 20, 2012

Figure 6. Stream discharge (cubic feet per second) hydrograph for Blacktail Creek at USGS Gauging Station SS-04. Baseflow conditions were observed in Blacktail Creek between September 17, 2012 and September 21, 2012 during tracer injection (shown in red) and synoptic surface-water sampling (shown in green). Streamflow data available at USGS online database (http://waterwatch.usgs.gov/new/index.php).

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at 07:45 h and continued at a constant rate until September 21, 2012 at 16:45 h. Synoptic sampling of surface water began on September 21, 2012 at 08:15 h and continued until September 21, 2012 at 13:32 h. Typically, baseflow conditions in Blacktail Creek range between 8 and 12 cfs, and the 23-y daily mean value is 9.5 cfs; baseflow during this test was on the upper end (12 cfs). Baseflow conditions were observed in Blacktail Creek for 4 days prior to the initiation of the tracer injection, and Blacktail Creek remained at baseflow until after sampling was completed; small amplitude diel fluctuations in flow were observed throughout the duration of the experiment (fig. 6).

3.1 Tracer Injection

Tracer injection rates were measured in triplicate with a graduated cylinder throughout the duration of the experiment. Data demonstrated low percent error (2.6%) between triplicate measurements and indicate that constant injection rates (~0.2 L/min) were maintained (fig. 7). Analysis of hourly ISCO samples collected at Montana Street (SS-05) indicate that travel time in Blacktail and Silver Bow Creeks between the injection site (upgradient of Oregon Avenue) and Montana Street was roughly 5.0 h (fig. 7). The bromide tracer concentration reached steady-state conditions at Montana Street approximately 11 h after the injection began (fig. 7).

Bromide concentrations in mainstem, tributary, wetland, and drivepoint samples are shown in figure 8B. The precision of analysis for the Br tracer was used to determine significant changes downstream. A difference in Br concentrations had to exceed 8% (represented by error bars) to be considered a real increase in flow, whereas minor differences (<8.4%) in concentrations were considered experimental error. Some sampling sites exhibited Br concentrations that were greater than upgradient Br concentrations (i.e., SS-04.5–SS-04; SS-05–SS-05A); however, the differences between sites were less than 3 percent, and considered to be within the margin of error.

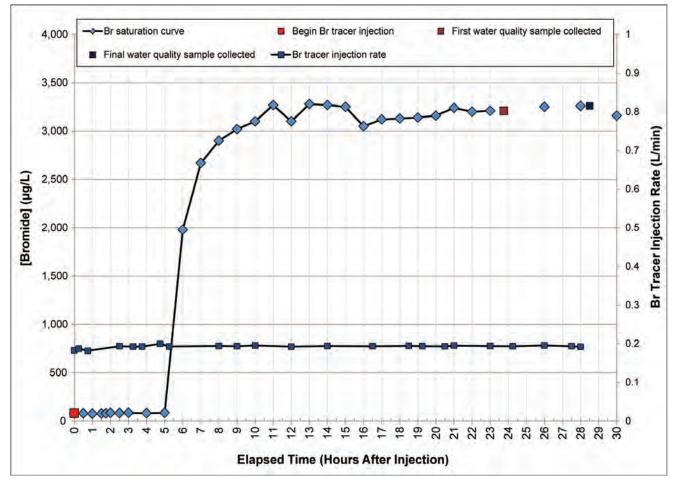


Figure 7. Tracer injection rates (L/min) and changes in concentrations of dissolved Br versus time in ISCO samples collected in SBC at Montana Street.

The dissolved Br concentrations decreased by 20 percent (between Oregon Avenue and 5,165 ft downstream of the tracer injection, site C-4.5). Downstream of sampling station C-4.5 (5,165 ft), dissolved Br concentrations in mainstem samples remain stable, indicating that Blacktail and Silver Bow Creeks were either non-gaining or net-losing reach beyond this station. Concentrations of Br in wetland and drivepoint samples were consistent with background concentrations. Three tributary sites (C-12 TR, Sand Creek, and C-9 TR GG) exhibited elevated Br concentrations (fig. 8B). Elevated Br concentrations may be an indication that Blacktail Creek is losing to tributaries C-12TR (wetland), Sand Creek, and C-9 TR (Grove Gulch).

3.2 Stream Discharge

Measured discharge (green) and calculated discharge (red) at mainstem sites are plotted against downstream distance (from right to left, consistent with flow in map) in figure 8C. Discharge values calculated from tracer-concentration data give a continuous accounting of stream gain, but cannot account for stream loss. The increase in discharge between two stream sites represents the total inflow from surface and subsurface sources to the stream. Stream loss was determined through a review of the FlowTracker data and statistical error. Discharge data are provided in tabular form in figure 8A for comparative purposes.

Error bars associated with each manual discharge measurement (5%) were determined from the FlowTracker data reports (appendix D). Two types of error, observational (Br-injection rates) and instrumental (ICP-MS), were used to estimate the uncertainty associated with calculated discharge value. The error associated with the Table 2

calculated discharge values (8.4%) were determined using an arithmetic calculation of error propagation (Bevington and Robinson, 1992), assuming a calculated error of 2.6% for the injection rate and an estimated error of 8% for the bromide concentration.

Flow measurements from tributary inputs (i.e., wetlands and streams) are presented in table 2. Overall, manual

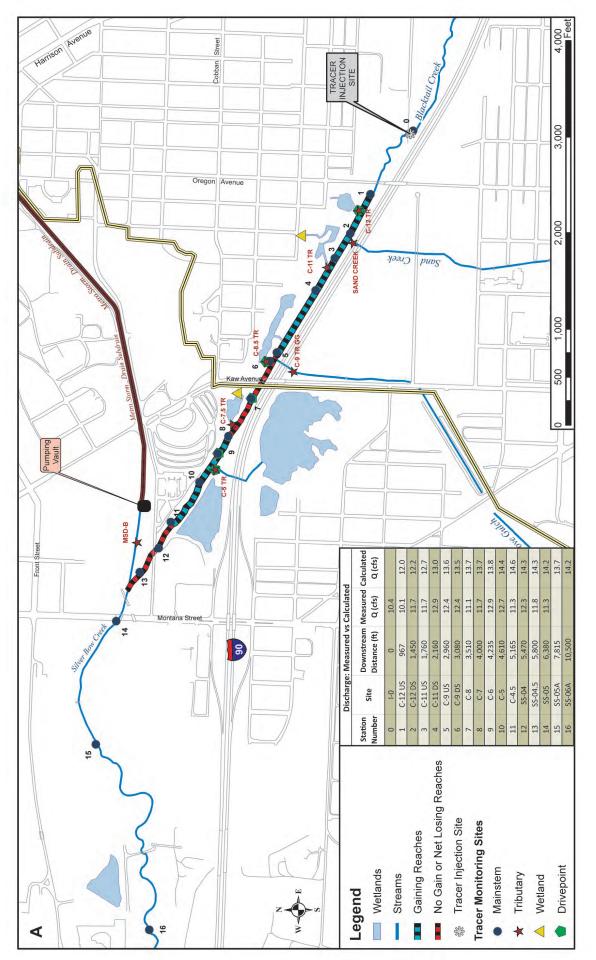
measurements of flow in tributaries were difficult to perform. In order to obtain more accurate and precise measurements, Parshall flumes were installed in selected tributaries (C-8.5 TR and C-7.5 TR). Discharge measurements on remaining tributaries were performed using a SonTek Flow Tracker. Errors associated with FlowTracker measurements in tributaries varied considerably (appendix D), and sometimes resulted in statistically invalid data. The quality of each discharge measurement was evaluated (table 2); data associated with high percent errors (C-12TR and C-9.5TR GG, >100% errors) were flagged as poor quality. Discharge was not measured in Sand Creek or the Metro Storm Drain (site MSD-B), due in large part to poor gauging conditions and interferences from low-flow conditions.

In total, surface-water contributions from tributaries with detectable flow (table 2, C-11 TR, C-8.5 TR, C-7.5 TR, and C-5TR) accounted for 0.84 cfs, or 39 percent of the total gains observed over the study area. It is assumed that the remainder of gain (61%) observed throughout the Blacktail Creek study area were direct inputs to the stream from groundwater sources. It is important to note that all tributaries that had detectable flow were wetlands that are, by definition, surface-water expressions of groundwater (received the majority of recharge from local groundwater sources).

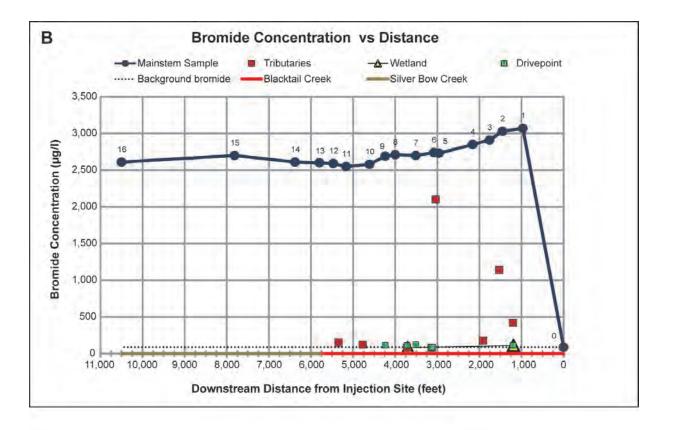
The uncertainty in gauging flow in four tributaries [C-12TR, Sand Creek, Grove Gulch (C-9TRGG), and MSD-B] was too large to ascertain flow conditions from discharge data. However, flow conditions in these tributaries could be inferred using other data. Significantly elevated Br concentrations observed in samples from these tributaries (fig. 8B,

Table 2. Measured discharge at tributary sites.

Site	Downstream Distance (ft)	Q (cfs)	Method	Quality
C-12 TR	1,201	-2.97E-02	FT*	Poor
SAND CREEK	1,527	_	ND**	
C-11 TR	1,910	1.81E-01	FT*	Ok
C-9 TR GG	3,035	-5.40E-03	FT*	Poor
C-8.5 TR	3,130	2.59E-01	Flume	Good
C-7.5 TR	3,717	4.32E-02	Flume	Good
C-5 TR	4,398	3.57E-01	FT	Ok
MSD-B	5,343	_	ND**	



BTC ID numbers are provided on A, B, and C for comparison. Calculated charges (C) obtained via tracer dilution method using known tracer injection rates sured discharge (C) during tracer injection. Distance from tracer injection (B and C) are plotted in reverse order, consistent with the direction of streamflow. Figure 8. Map of study area (A), with bromide concentrations in primary, tributary, drivepoint, and wetland synoptic samples (B), and calculated vs. meaand in-stream concentrations of bromide. Gaining reaches are depicted in A. Measured discharges (C) obtained via SonTek FlowTracker flowmeter.



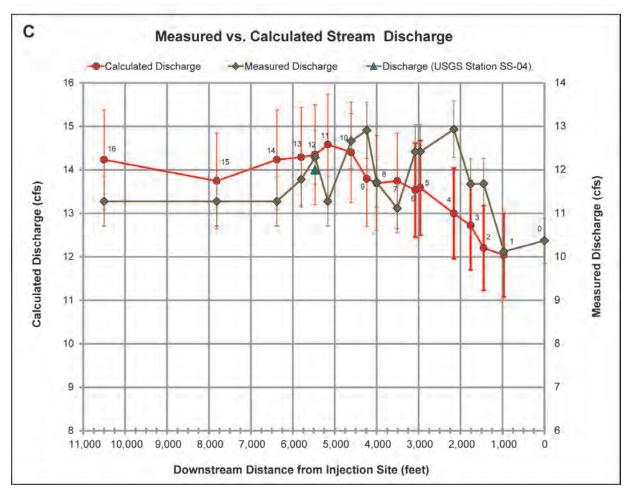


Figure 8, continued.

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orders of magnitude above all other Br concentrations) may be an indication that Blacktail Creek is losing flow to three tributaries: C-12 TR, Sand Creek, and Grove Gulch (C-9 TR GG). Elevated Br concentrations were not detected in the MSD sample (MSD-B), which indicates that Blacktail Creek is not losing to the MSD channel.

Combined, all methods of discharge measurement indicate that:

- Discharge in Blacktail Creek increased 2.2 cfs (22%) across the BTC study area.
- The majority (61%) of gains observed in Blacktail Creek were from direct groundwater inputs into the stream. The remainder of inputs were from adjacent wetlands under the influence of groundwater.
- Blacktail Creek in the reach between sampling stations 1 and 5 (fig. 8A, C-12US to C-9 US) is a gaining stream (as denoted by blue/black dashed line in fig. 8A), receiving inputs almost exclusively from groundwater with minor surface-water contribution (<10%, C-11 TR).
- Blacktail Creek in the reach between sampling stations 5 and 8 (fig. 8A, C-9 US to C-7) was either a non-gaining or net-losing reach (as denoted by red/black dashed line in fig. 8A), and was potentially losing a significant amount of flow to Grove Gulch (based upon elevated Br concentrations in Grove Gulch sample).
- Blacktail Creek in the reach between field stations 8 and 11 (fig. 8A, C-7 to C-4.5) was a gaining reach (as denoted by blue/black dashed line in fig. 8A), receiving inputs from groundwater and surface-water sources.
- Blacktail Creek is either a non-gaining or net-losing reach downstream of field station 11 (fig. 8A, site C-4.5, as denoted by the red/ black dashed line).
- Flow increases were not observed in the studied reach of Silver Bow Creek.

3.3 General Trends in Synoptic Data

Mainstem sampling operations took roughly 6 h to complete, began at the farthest downstream site (at 08:15 h), and finished at the tracer injection site (at 13:03 h). Other than water temperature, diel fluctuations in physical parameters were not observed over the sampling duration. In general, pH (range: 7.18–7.69), specific conductivity (SC) (range: $300-324 \mu$ s/cm), and Eh (range: 359-406 mV) remained stable in mainstem samples collected during the synoptic event (fig. 9A). Subsequently, concentrations of hardness remained consistent with one another over the study site, while water temperatures increased 6°C (consistent with increasing air temperature) over the sampling duration (fig. 9B).

Downward trends in dissolved oxygen (DO) concentrations are shown with stable trends in dissolved organic carbon (fig. 10A). As expected, diel fluctuations in DO are consistent with temperature fluctuations (fig. 9B). Generally, stable trends were observed for concentrations of most major cations and anions except Na and Cl (fig. 10B).

3.4 Downstream Trends of Copper and Zinc Concentrations

Downstream trends for Cu (fig. 11B, total recoverable and dissolved) and Cu loading (fig. 11C) are presented. Upgradient (upstream of injection site) Cu concentrations in mainstem samples during synoptic sampling were 1.4 µg/L (dissolved) and 2.5 µg/L (total recoverable). Overall, concentrations of Cu in mainstem samples increased through the study area (dissolved = 1.4-3.6 µg/L; total recoverable = $2.5-7.9 \,\mu$ g/L); however, all dissolved Cu concentrations and most total recoverable (TR) Cu concentrations remained below MDEQ-7 acute and chronic aquatic-life hardness-based standards for copper (MDEO, 2010). Increased TR Cu concentrations were observed in samples collected near Kaw Avenue, between C-11 US and C-7. The Kaw Avenue reach was the only area in either stream where mainstem samples exceeded acute and chronic DEO-7 aquatic-life standards for TR copper (C-9 US, station 5; fig. 11A). Samples from two tributary (C-5 TR and MSD-B; fig. 10) and one wetland (near Kaw Avenue; fig. 10) had concentrations of TR Cu

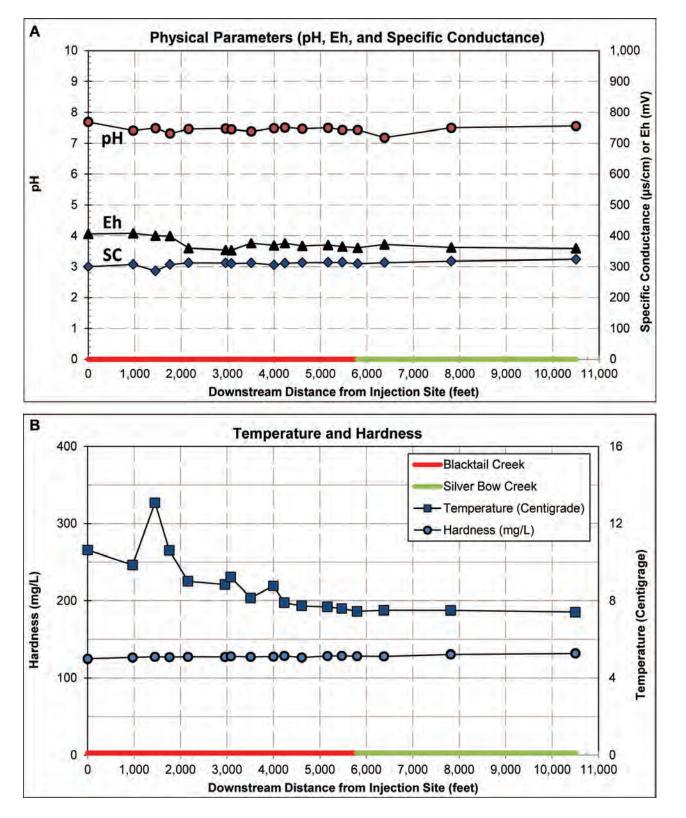


Figure 9. Distance from injection site versus: (A) pH, SC, and Eh; and (B) hardness and water temperature measured in synoptic samples collected on September 21, 2012.

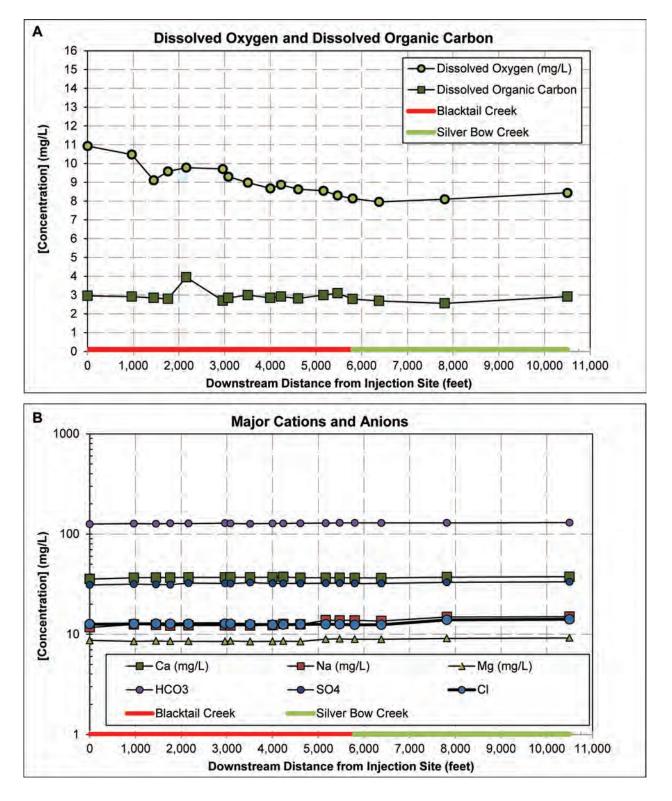


Figure 10. Distance from injection site versus: (A) DO and dissolved organic carbon, and (B) major cations (Ca, Na, Mg) and anions (Cl, HCO3, and SO4) in synoptic samples collected on September 21, 2012.

that exceeded acute and chronic aquatic-life standards (MDEQ, 2010). Samples from two tributaries (TR-8.5TR and MSD-B; fig. 12A) exhibited concentrations of TR Cu that exceeded acute and chronic aquatic-life standards (MDEQ, 2010). Elevated concentrations of Cu in streambed and bank sediments are a likely explanation for increased TR concentration of Cu observed in mainstem water samples, but not for Cu and Zn concentration in the tributaries. Groundwater quality entering the two wetlands to the north of Blacktail Creek (near Kaw Avenue, fig. 1) was not assessed in the current investigation, and could also be potential sources for contamination.

Downstream trends in copper loading in mainstem samples are shown in figure 11B. Upgradient (upstream of injection site) Cu loads were calculated to be 0.1 lb per day (dissolved) and 0.15 lb per day (TR). Cu load doubled within Blacktail Creek reaches below the injection site (0.1 to 0.28 lb/day), and increased by a factor of four in total recoverable samples (0.15 to 0.61 lb/day). Large increases in TR Cu load consistent with observations noted for Cu concentrations are observed in the Kaw Avenue reach of Blacktail Creek.

Trends observed in mainstem samples for dissolved and TR Zn concentration (fig. 12A) were consistent with those observed for copper. Upgradient (upstream of tracer injection) Zn concentrations in mainstem samples were 1.5 µg/L (dissolved) and 2.3 µg/L (TR). Concentrations of Zn in mainstem samples increased through the study area (dissolved, 1.5-12.8 µg/L; TR, 2.3-18.8 µg/L); all concentrations remained below MDEQ-7 acute and chronic aquatic-life hardness-based standards (MDEO, 2010). Increases in TR Zn were observed in samples collected near Kaw Avenue, between C-11DS and C-7, consistent with the trends observed in copper. Unlike Cu, dissolved and total Zn concentrations in most tributary samples (C-12 TR. C-11TR, C-8.5TR, C-7.5, C-5TR, and MSD-B; fig. 11A) were elevated above those from mainstem samples. Two tributary samples (C-8.5 TR and MSD-B) had TR Zn concentrations that exceeded acute and chronic aquatic-life standards for Zn (MDEQ, 2010). Concentrations of dissolved Zn in two drivepoint samples were elevated above that from surface-water samples, but below DEQ-7 standards (C-8.5 and C-7.5).

Zinc loading in mainstem samples is shown in figure 11B. Background Zn loads were observed at 0.1 lb per day (dissolved) and 0.15 lb per day (TR). Dissolved (0.1–1.0 lb/day) and TR (0.15–1.44 lb/ day) Zn load increased by an order of magnitude across the study area. Large increases in TR Zn load, consistent with observations noted for Zn concentrations, were observed in the Kaw Avenue reach of Blacktail Creek.

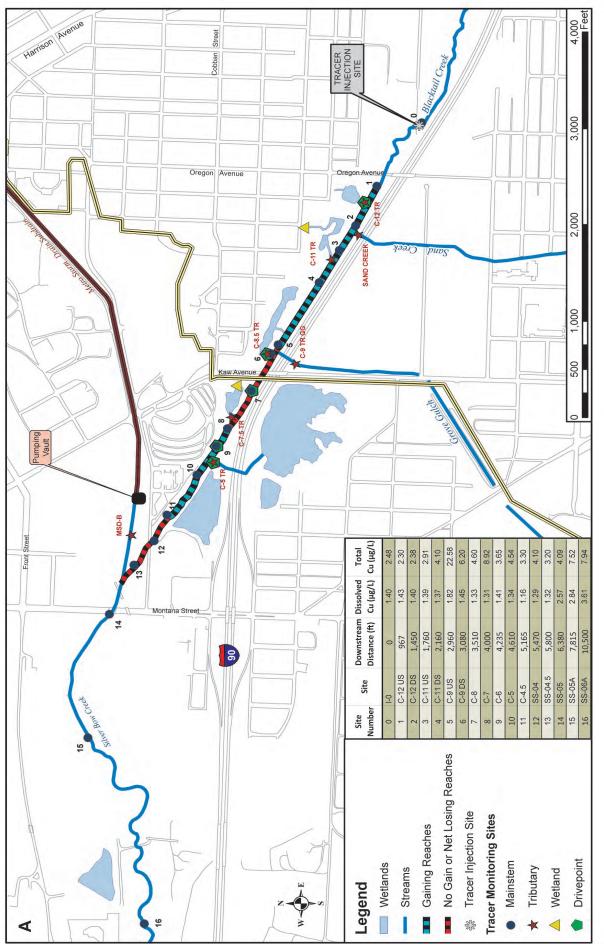
4.0 DISCUSSION

4.1 Tracer Study

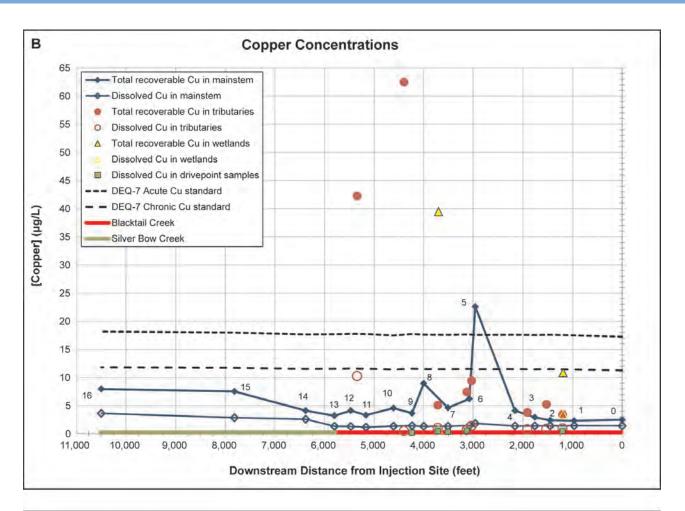
Review of the stream hydrograph at USGS gauging station SS-04 (fig. 5), Br-tracer injection rates, and the downstream Br concentration curve at Montana Street (fig. 6) suggest that:

- Baseflow conditions were present for 4 days prior to the initiation of the experiment,
- Baseflow conditions were observed throughout the tracer injection and synoptic sampling,
- Diel fluctuations in flow were minimal throughout the experiment;
- Travel times of the tracer between Oregon Avenue and Montana Street in Blacktail and Silver Bow Creeks are on the order of 5 h,
- Near-constant Br concentrations from samples collected at Montana Street were observed prior to, and maintained during, all synoptic sampling activities, and
- Constant tracer injection rates (0.2 L/min) were maintained.

Combined, these data suggest that the requirements necessary to conduct a tracer injection experiment were fulfilled, and the test was conducted under optimal conditions. For the purposes of this study, synoptic means that all samples were collected during a 5-h window during the time that Br concentrations and diel fluctuations of physical parameters in Silver Bow Creek were constant.







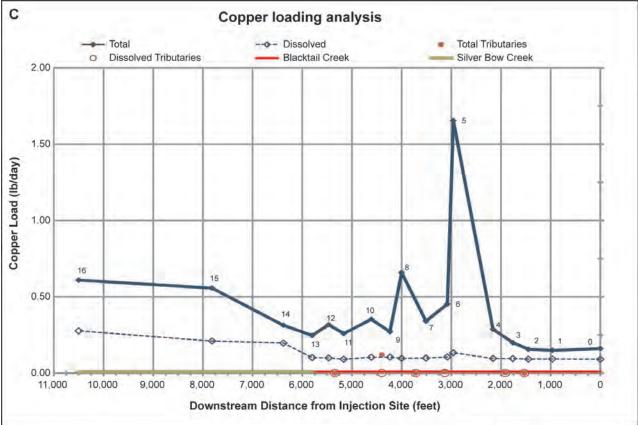


Figure 11, continued.



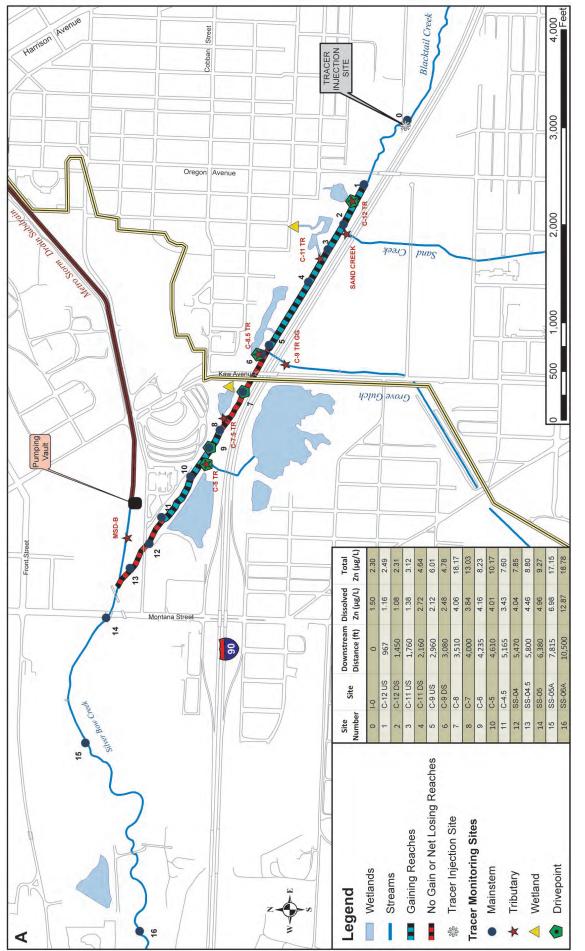
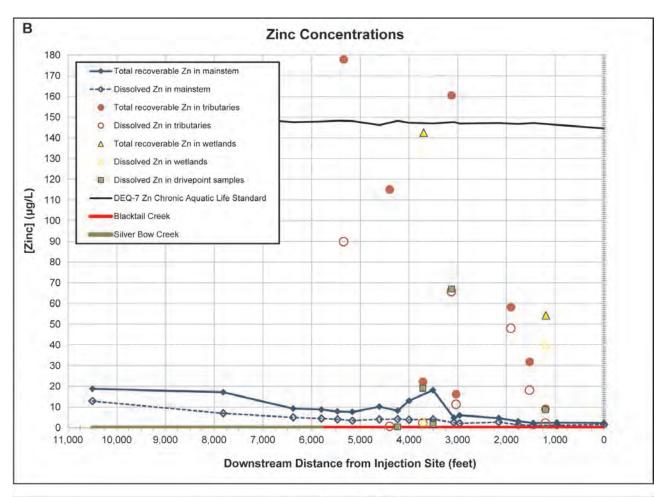


Figure 12. Map of study area (A), with dissolved and total recoverable Zn concentrations (B) and Zn loading analysis (C) for mainstem, tributary, wetland, and drivepoint samples. Site ID numbers are plotted in A, B, and C for comparison purposes. Gaining reaches of Blacktail Creek are shown. Dissolved and total recoverable Zn concentrations are shown in table. Distance from tracer injection are plotted (B and C) in reverse order. Hardness-based DEQ-7 acute and chronic aquatic-life standards presented in B. Zn loading analyses (C) were calculated using calculated discharges from tracer dilution method.



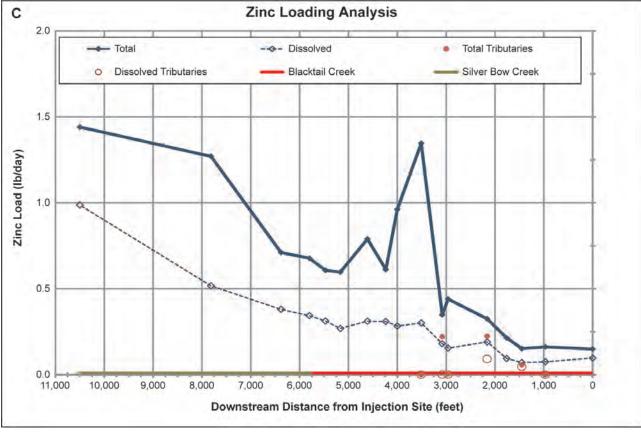


Figure 12, continued.

4.2 Hydrologic Evaluation

Although the two methods of discharge measurement generated data that differed in some cases, they both agreed that Blacktail Creek (fig. 1, stations 1 to 12) had a net-gain in flow of 2.2 cfs (~22 percent) between the injection site and site C-4.5 (fig. 8, site 11). Discharge data obtained from the FlowTracker measurements were much more variable than calculated data, because the method was able to account for stream loss within each reach. The largest increases in calculated discharge (between C-12 US and C-4.5) were determined in two reaches:

- Oregon Avenue reach (fig. 8, stations 1–4):
 1.0 cfs gain
- Downstream of Kaw Avenue (fig. 8, stations 8–11): 0.9 cfs gain

Combined, these reaches account for 86 percent of the gain observed in Blacktail Creek.

Groundwater (61%) and adjacent wetlands under the influence of groundwater (39%) accounted for the vast majority (>99%) of flow increase observed in Blacktail Creek. Wetlands were inspected for surface-water recharge sources (i.e., surfacewater channels, storm drains flowing into wetlands); only one site (fig. 1, C-11TR, yellow triangle) had surface-water baseflow inputs contributing to recharge. The surface-water contribution to wetland C-11TR had unquantifiable flows (<0.1 cfs), and water-quality results revealed compliance with DEQ-7 aquatic-life standards.

Downstream of C-4.5 (fig. 8C, site 11), both methods of flow measurement agreed that Blacktail and Silver Bow Creeks were either non-gaining, or net-losing streams. Unfortunately, discharge was not measured at the two synoptic sites located farthest downstream (SS-05A and SS-06), and Br-obtained discharge rates cannot account for stream loss. Tracer-calculated measurements of discharge rely on the conservation of Br in surface water. A losing reach of stream violates this requirement (USGS, 1997). Therefore, calculated discharge values were unreliable downstream of site C-4.5 (fig. 8, station 11).

Discrepancies were observed in the two types of discharge measurements (fig. 8C, measured vs. cal-26 culated discharge) in the reach between sampling sites C-9 US and C-7 (fig. 8, stations 5–8), where calculated discharge measurements remained stable while manual discharge measurements decreased across the reach. This discrepancy suggests one of two scenarios:

- 1. Blacktail Creek is losing to tributaries in this reach [Grove Gulch (C-9 TR GG)], and/or
- 2. Blacktail Creek is losing to hyporheic flow downstream of C-9 US (5).

Manually measured discharge suggests a 2 cfs loss within this reach, while Br-calculated discharge rates are stable. The magnitude of the difference is far greater than the calculated experimental errors provided in the discharge reports in appendix D.

Measured discharge rates (table 2) and Br concentrations (fig. 8C) for the two tributaries within this reach [C-8.5 TR and C-9 TR GG (Grove Gulch)] suggest that only Grove Gulch was receiving Br load from Blacktail Creek. The tributary and wetland to the north (C-8.5 TR) had measureable discharge into the creek (0.25 cfs). Blacktail Creek loss to Grove Gulch is a possible explanation for the discrepancy, but the discharge measured in Grove Gulch should have accounted for the loss measured within this reach of Blacktail Creek (2 cfs). Discharge data in Grove Gulch showed negligible flow with a calculated error of 202 percent (appendix D). The high error calculated at this site was a function of high signal-to-noise ratios caused from extremely low-flow conditions. Grove Gulch most likely received flow from the creek, but the quantity was insignificant compared to the magnitude of the decrease in discharge observed in this reach of Blacktail Creek (2 cfs). Some other explanation must account for the loss of discharge in this reach of Blacktail Creek.

Grove Gulch (fig. 1; site C-9 TR GG) was sampled on the south side of Interstate I-90 (fig. 1) approximately 300 ft south of its confluence with Blacktail Creek. The elevated Br concentration (fig. 8B, analytical value at ~3,080 μ g/L downstream from the injection site) in the Grove Gulch sample suggests that this site is receiving Br from Blacktail Creek, either through surface water or groundwater. A parallel baseflow investigation done in coordination with the current study was conducted by AR in 2011. An analysis of radon (²²²Rn) concentrations from four shallow groundwater wells located adjacent to Blacktail Creek showed "very low" ²²²Rn concentrations, concentrations too low to be representative of background radon in groundwater. These results suggest the possibility of subsurface hyporheic flow, as indicated by "mixing between recent (days) surface water and shallow groundwater" in the subsurface (AR, 2012).

Industrial water demands in Butte and stream channelization in the early 20th century changed Blacktail Creek from a meandering intermontane stream to a linear channel between Harrison Avenue and its confluence with Silver Bow Creek (fig. 1). Furthermore, the construction of I-90 in the 1960s most likely further altered Blacktail Creek's morphology. Preferential subsurface flow paths may exist within Blacktail Creek's original stream channel, and may be masked by the anthropomorphic manipulation and infrastructure upgrades now present near the stream. It seems possible that these actions resulted in enhanced hyporheic flows in the streambed, where the stream is preferentially following its original course. The hypothesis of anthropogenically enhanced hyporheic flow in this reach of Blacktail Creek is supported by the discrepancy observed in flow measurements, increased concentrations of Br observed in Grove Gulch, and the observations reported by AR (2012), but would need further evaluation to advance as a probable hypothesis.

4.3 Downstream Trends in Contaminants of Concern

Dissolved and TR Cu concentrations increased downstream from the injection point in the Blacktail Creek reaches within the study area (fig. 10). Total recoverable analytical results from one mainstem site (C-9 US) exceeded MDEQ-7 aquatic-life standards, while all dissolved Cu concentrations remained below the aquatic-life standards (MDEQ, 2010). Consistent with Cu concentrations, dissolved and TR Zn concentrations in mainstem samples increased over the entire study area (fig. 11); however, all concentrations in mainstem samples remained below standards. Dissolved concentrations of As, Cd, Cu, and Zn in all mainstem samples remained below MDEQ-7 aquatic-life standards (MDEQ, 2010).

In the Kaw Avenue reach of Blacktail Creek (stations 5–8), elevated concentrations of Cu (fig. 10) and Zn (fig. 11) in mainstem samples were observed. This reach of Blacktail Creek was heavily impacted by historic sediment transport from the Grove Gulch confluence, which may explain the elevated TR concentrations of Cu and Zn found in mainstem samples within this reach. However, wetland, drivepoint, and tributary samples collected within this reach suggest that groundwater discharging to this area may have elevated Cu and Zn concentrations. Unfortunately, the quality of the groundwater recharging the wetlands was not a focal point of this investigation, and cannot be ruled out as a potential source.

The reach of Blacktail Creek where elevated Cu and Zn concentrations were observed in mainstem, tributary, wetland, and drivepoint samples overlie the area where historic impacts to Blacktail Creek have occurred from Grove Gulch, and hyporheic flow may be occurring.

Whether elevated Cu and Zn concentrations in samples collected near the downstream end of this reach are the result of increased pore water interactions between groundwater and/or surface water with metal-laden sediment is speculative, but possible. Streambed sediment data sampled in Blacktail Creek, roughly 100 m downstream of the Grove Gulch confluence, show elevated concentrations of Cu (1,000 mg/L) and Zn (1,000 mg/L) in streambed sediments. The streambed and bank sediments within this reach should be further characterized to see if restoration activities (e.g., removal) are needed.

A detailed analysis of streambed and bank sediments is needed in the Kaw Avenue reach of Blacktail Creek (from Grove Gulch confluence to George Street). If streambed sediments with elevated concentrations of COCs are present in the Kaw Avenue reach, then these sediments present potential point sources for downgradient sites during high flow or storm-water events. Tucci and Icopini (2012) and several unpublished water-quality sampling events showed an increasing trend in dissolved Cu in Blacktail Creek (between Oregon Avenue and George Street). While dissolved Cu concentrations increased slightly in Silver Bow Creek (~2 ppb), the previously reported trend in Blacktail Creek was not observed in the current study. However, an increase similar to previously observed increasing trends in TR Cu, dissolved Zn, and TR Zn was observed in this reach during the current investigation. The most likely sources of Cu and Zn in Blacktail Creek (fig. 1, stations 5-12) is from sediment (i.e., historic Grove Gulch sediment loads or mine waste from the BTC Berm) in, or adjacent to, the streambed.

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APPENDIX A

SAMPLING AND ANALYSIS PLAN

INTRODUCTION

An unidentified loading source to Blacktail Creek, for both total recoverable and dissolved constituents of copper and zinc, has been identified in the reach between Oregon Avenue and Montana Street. This reach of Blacktail Creek represents the eastern boundary of the Butte Priority Soil Operable Unit (BPSOU) in Butte, MT. In order to identify this source clearly, a base flow sodium bromide tracer study on Blacktail Creek has been scheduled for late February/early March. The timeframe for this study is dependent upon flows in the creek and temperature conditions, and therefore schedules and timelines for this project have not been finalized.

The current study area along Blacktail Creek is a gaining reach. At base flow conditions, significant increases in flow (40% increases) are seen within this reach. Both groundwater and surface water (Sand Creek, Grove Gulch, and multiple wetlands to the north and south of Blacktail Creek) inputs occur within this reach, all of which present themselves as possible sources of metal loading to Blacktail Creek. The current study was designed to quantify flow to this reach, identify the contribution of various inputs to the creek, and identify possible point sources for metal loading.

The primary goal of a tracer injection study is demonstrating a direct linkage between waste sources and seeps where discharge into surface water occurs. In this case, a number of possible sources of contamination to the area of concern are possible, and therefore a sizable and detailed sampling regime of both groundwater and surface water was constructed to pin point the area of loading. Prior to the tracer injection, a complete synoptic groundwater sampling event will be conducted on selected groundwater wells located adjacent to the reach of Blacktail Creek between Oregon Avenue and George Street. In addition to the sampling of wells, the quality of groundwater seepage into the streambed will be monitored in selected locations with drive-point piezometers. Understanding the link between groundwater/surface water interactions may be crucial to understanding the fate of dissolved constituents within Blacktail Creek; therefore, pore water sediment dialyses samplers (Hesslein peepers) will be used for this purpose. The groundwater sampling will be conducted in close proximity to the tracer injection study. In addition to groundwater discharge, surface water inputs within this reach are numerous and will be sampled during the tracer injection study.

METHODS AND SAMPLING PROTOCOL

Tracer Injection Protocol

A sodium bromide tracer study will be conducted on Blacktail Creek in Butte Montana between Oregon Avenue and Montana Street. Concentrated NaBr (256,800 mg/L) will be injected into Blacktail Creek near the gazebo east of Oregon Avenue using a constant rate peristaltic pump at a rate of 130 mL/minute. The injection rate and concentration of NaBr tracer solution have been selected to assure a residual concentration of Br in the most downstream sampling site (SS-05) of 1 mg/L. Tracer will be injected into Blacktail Creek for a minimum of 24 hours prior to sampling. To assure stable bromide concentrations are obtained in the creek, a breakthrough curve will be generated using a bromide ion selective probe on samples collected on an hourly basis (ISCO Sampler) from the farthest down-stream sampling site (SS-05).

Bulk 25% Bromide tracer solution will be pre-mixed in a 250 gallon polyethylene storage tank by mixing 140 gallons of Blacktail Creek water with six 55-pound bags of sodium bromide. Since this study will be conducted during freezing conditions, precautionary measures will have to be taken to assure the tracer solution does not freeze. The concentration of tracer solution will be of sufficient salinity to significantly lower the freezing point of the solution. If need be, a generator and electric heater will be present to keep the ambient temperature in the tracer solution above freezing. The injection line will be guarded from freezing by installing foam insulation over the discharge line. The tracer apparatus will be checked frequently to assure freezing does not occur. Constant mixing will be conducted inside the tracer tank with a small submersible pump. Furthermore, temperatures of the tracer will be monitored on a frequent basis.

Sampling Procedures

All groundwater and surface water monitoring will be conducted in accordance with methods and practices established in the Butte Mine Flooding Operable Unit Sampling and Analysis Plan released in 2002 (EPA Docket No. CERCLA – VIII-96-19).

Physical Parameter Measurement

Physical parameters (temperature, pH, Eh, SC, LDO, and turbidity) will be measured in-situ using a Hach Hydrolab Minisonde-5 for all groundwater and surface water samples. A total of 30 groundwater samples and 25 surface water samples will be collected for this project.

Stream Flow Measurement

Stream flow will be measured during the tracer injection according to the tracer dilution method of a gaining stream, which involves adding a known strong concentration of tracer (sodium bromide) solution at a constant rate to a known flow. Through chemical analysis of bromide, the flow downstream can be measured. In addition to chemical analysis of bromide, flow measurements will be obtained using a SonTek FlowTracker ADV flow meter using the Marsh McBirney method of calculating stream flow. Percent error for flow measurement is typically between 3-4 percent using a Flow Tracker.

Groundwater Sampling

A total of 30 groundwater samples will be collected; 22 samples collected from groundwater wells, and eight samples collected from drive point sampling of the stream bed. Groundwater wells will be sampled using 2-in submerisble 12 volt pumps. A minimum of three well casing volumes will be purged and stable physical parameters obtained prior to sampling. The sampling matrix for groundwater is listed in table 1, and a list of monitoring sites is found in table 2. Physical parameters of temperature, pH, Eh, specific conductance, dissolved oxygen, and turbidity will be measured.

Analysis	Method	Matrix	Sample Preparation
Dissolved metals	EPA 200.7 & 200.8	water	1-500mL Filtered (0.45micron) + Acidified (2% HNO ₃)
Major cations and anion	EPA 200.7 & 300.0	water	1-250 filtered (0.45 micron) + untreated
Physical parameters and alkalinity	EPA 150.1, SM2510B & 2302B	water	1-500mL unfiltered + untreated
Nitrate/Nitrite/Total Nitrogen	USGS Method I-2650-03	water	1-250mL filtered (0.45 micron) + acidified (0.5% H ₂ SO ₄)
Total organic carbon	Standard Method D5904	water	1-60mL unfiltered + acidified (2% HCl)
Dissolved organic carbon	Standard Method D5904	water	1-60mL filtered (0.45 micron) + acidified (2% HCl)

Table 1. Sampling Matrix for Groundwater.

Wells	GWIC #	Comments
GS-28	150389	Northwest wetland
AMW-11	161962	BTL Berm south
Berm Well		BTL Berm south
AMW-13	137597	BTL shallow Floodplain (Visitors Center)
AMW-13B	240863	BTL middle alluvial (Visitors Center)
AMW-13C	255975	BTL deep alluvial (Visitors Center)
BPS07-16A	248566	Northeast wetland
BPS07-16B	248565	Northeast wetland
AMW-04A	162029	Wetland South
AMW-04B	162043	Wetland South
AMW-03S	137599	Grove Gulch shallow alluvial
AMW-03D	137600	Grove Gulch deep alluvial
GG99-01	191293	Grove Gulch shallow alluvial
BT99-03	171291	Sand Creek shallow alluvial
AMW-10	137602	Sand Creek shallow alluvial
BT99-01	171289	Butte south shallow alluvial
BT99-02	171290	Butte south shallow alluvial
BT98-05	171288	BTL Creek floodplain (Oregon Ave)
BT98-06		BTL Creek floodplain (Oregon Ave)
BT98-01	171295	BTL Creek floodplain (Oregon Ave)
BT98-02	171294	Butte North Shallow Alluvial (Cobben)
BT98-02B	240865	Butte North Middle Alluvial (Cobben)

Table 2. Groundwater sampling list of sites.

Drive Point Piezometer Sampling

Eight drive point piezometer will be installed in the Blacktail Creek streambed for collection of water samples. , The drive points are specialized small diameter stainless steel samplers custom made for members of CDM, designed specifically to be attached to a peristaltic pump tubing for purging purposes. Locations will be chosen upon completion of ARCO's thermal imaging study to determine areas of groundwater recharge. The timing of this work and choice of piezometer locations will be tied in closely with the tracer injection test. For instance, chosen surface water monitoring sites during the tracer study will be located adjacent to the piezometer sampling locations. Table 1 lists the sampling matrix for this sampling.

Dialysis Membrane Peeper Sampling

The peeper investigation will be conducted by a Montana Tech graduate student under the direct supervision of Dr. Chris Gammons, a Geology Professor at Montana Tech. One modified 28 cell Hesslein peeper was purchased from Rickly Hydrological, along with a set of pre-cut dialysis membranes (5 micron pore diameter). The peepers will be assembled with each of the chambers (28 chambers) filled with deionized and deaerated water. The peepers will be placed upright in a cylinder through which N₂ gas is bubbled slowly and steadily for a period of 48-h. The N₂ tank and cylinder filled with water are taken out in the field, to maintain anoxic conditions.

The peeper will be deployed in the north wetland west of Kaw Avenue, by partially immersing it into the sediment. At least four rows will be exposed to open water, while the remainder will be submerged in the sediment of the wetland. The peepers will be left in the sediment for a period of 2 to 3 weeks to allow equilibration between the pore water and the dialysis chambers. The peepers will then be withdrawn from the sediment, placed in a cooler containing a stream of N_2 gas, and transported to the laboratory for sampling.

The sampling matrix for the peepers is a modified version of that shown in table 1. Each peeper row will be assigned a number from 1 to 28. Every 2^{nd} row consists of a pair of cells, labeled "A" or "B". The even-numbered rows have a single cell that had more than twice the volume (~ 12 mL) of the smaller A and B cells (~ 5 mL each). The large even-numbered cells will be used for pH/Eh determination (EPA 150.1, SM2510B & 2302B), extraction of samples for ICP-metals (EPA 200.7 & 200.8). The A cells will be used for extraction of samples for colorimetric analysis of phosphate and H₂S. The B cells will be used for extraction, and anions (EPA 200.7 and 200.8).

Surface Water Sampling

A total of 25 surface water samples will be collected from in-stream and tributary locations along the Blacktail Creek reach between Oregon Avenue and Montana Street (SS-05). In-stream surface water sites will comprise both up-gradient and down-gradient reaches of all surface water tributaries, and reaches of significant groundwater gain.

Areas of significant groundwater gain will be determined during ARCO's thermal imaging study. Additionally, all tributaries (wetlands, streams, storm water inputs) will be sampled in this reach. Sampling locations will be selected upon completion of ARCO thermal imaging studies and several recon field trips.

During the tracer study, a sampling preparation station will be set up near the Butte Chamber of Commerce Visitor Center on George Street. Bulk composite samples will be collected in 3.6-liter acid washed HDPE sampling bottles at both in-stream and tributary locations and transported to the sampling preparation station. After samples have been processed (table 3), they will be stored on ice and transported to MBMG Laboratories. Table 3 shows the sampling matrices for surface water.

Analysis	Method	Matrix	Sample Prep
Dissolved metals	EPA 200.7 & 200.8	water	1-250mL Filtered (0.45micron) + Acidified (2% HNO ₃)
Major cations and anion	EPA 200.7 & 300.0	water	1-250 filtered (0.45 micron) + untreated
Physical parameters and alkalinity	EPA 150.1, SM2510B & 2302B	water	1-250mL unfiltered + untreated
Nitrate/Nitrite/Total Nitrogen	USGS Method I-2650-03	water	1-250mL filtered (0.45 micron) + acidified (0.5% H ₂ SO ₄)
Total recoverable metals	EPA 200.7, &200.8	water	1-250mL unfiltered + acidified (2% HNO ₃)
Total organic carbon	Standard Method D5904	water	1-60mL unfiltered + acidified (2% HCl)
Dissolved organic carbon	Standard Method D5904	water	1-60mL filtered (0.45 micron) + acidified (2% HCL)

Table 3. Sampling matrix for surface water.

QUALITY ASSURANCE/QUALITY CONTROL

Quality Assurance/Quality Control procedures for the tracer study will involve one field blank and one field duplicate sample per sampling event (groundwater and surface water). Additionally, the bromide tracer solution will be sampled twice during the course of the experiment.

Calibration of field equipment is described in Table 4. Field equipment will be calibrated daily. Prior to using field instrumentation, equipment will be washed thoroughly using deionized water (DI). Furthermore, decontamination procedures of sampling equipment (sampling pumps, hoses, etc...) will involve flushing and washing thoroughly with DI water.

Probe/meter	Calibration Method	Frequency
рН	Buffer: 7, 4	daily
Eh	Zobelle's Solution (428mV)	daily
Specific Conductance	SC standard 1470us/cm	daily
Dissolved Oxygen (LDO)	100% Saturation	daily
Turbidity (NTU)	0, 100 point NTU	daily
Marsh McBirney Flow	0 Point calibration	daily
Br Ion Selective Probe	Calibration Curve (1,10, 100 ppm)	daily

Table 4. Calibration procedures of field equipment.

TIME LINE

As previously mentioned, the time line for this project have not been finalized as sample site selection for surface water is dependent upon ARCO's completion of the thermal imaging study, and the tracer study itself is dependent upon weather conditions. Table 5 gives a general timeline for this project however.

Table 5. Time-line for MBMG tracer study

Event	Date
Groundwater sampling	2/6/11 - 2/18/11
Tracer study injection	3/7/11 - 3/15/11
Surface water sampling	2/28/11 - 3/15/11
Drive point groundwater sampling	2/28/11 - 3/15/11
All samples submitted to MBMG Labs	4/1/2011
Preliminary MBMG lab Results	5/15/2011

SampleTeam PROCEDURES

Garret Smith (MBMG) Matt Berzel (MBMG) Tina Donovan (Trec)

Please follow the procedures outlined below

- Work from farthest downstream sites up.
- Label container with a sharpie prior to getting wet. Label with sample ID, date and time.
- Wash out sampling container three times with sample water, similar to BMF sampling methods.
- Collect depth-integrated sample by dipping sample container in flowing portion of the stream (no pools or eddy's) along a single transect. Depending on width of channel chose between 5 and 20 locations along the transect, starting at the surface dipping down to the floor of the channel.
- Make sure there is no head space in bulk sampling containers.
- If the channel is not deep enough to fully saturate the 1-gallon bulk sample, smaller sampling containers are provided to ensure zero head-space in 1-gallon sampling container. Do not re-use the smaller sampling containers.

Sam	pling Prep Team	
	Team: GI, TP, AB	
	Vehicle: Suburban	1
1)	Sample bottles	
	A) 120- 250 mL sample bottles	
	B) 75 glass vials for TOC and DOC	
2)	Acid	
	A) 40 total Sulfuric	
2	B) 80 total Nictric	
3)	nitrile gloves	
4)	A) m and L	
4)	Cart Tables- 2, one from house and cart table	
5)	tubing	
5)	Filters	
7)	A) 40 medium flow	
7) 2)	DI water-2 Carboys HNO3 acid DI- 1 carboy	
3) 9)	spray bottles	
9) 10)	chem wipes	
11)	paper towels	
12)	NaBr Tracer probe box	
13) 14)	2- peristaltic pumps	+
14)	All peristaltic batteries log book	+
16)	First aid Kit	+
10)	Towels	+
18)	Coolers	+
19)	Ice (GI pick up couple bags weds am)	<u> </u>
20)	zip locs	+
	tion Site	-
njec		
	Team: GI, TP, AB vehicle: Canyon	
1)	Tracer	1
1)		
<u>2)</u>	peristaltic pump	
3)	tubing	
4)	batteries- charged car batterie	
5) 6)	extra gasoline	
- /	Tool box	
7)	zip ties	
Sam	pling Team	-
	Team: MB, GS	
4.)	vehicle: truck with topper	
1)	2 - MS-5 hydrolabs w/ tubidity	
2)	Location map of sites and spreadsheet of sites	
3)	Cages for MS-5	
4)	charged surveyors -2 (1 is for back-up)	
5)	2 - cables	-
6) 7)	pig-tailed adaptors	
7)	cigarette lighter chargers for surveyors	-
B)	1-gallon jugs, both boxes	
9)	log books	-
10)	pens/penncils	
11) 12)	small transer containers (1-bag)	
12)	DI water, 1-carboy	
13) 14)	spray bottles for DI water Waders	
14) 15)	Wading Shoes	+
15) 16)		
	nitrile gloves Bucket	
17)		1
TIOW	reasurement team	-
	Team: NJT, JV	+
1)	vehicle: Cherokee	+
1)	Flow Tracker	+
2)	8 spare batteries	
3) 1)	Tape measurer	
4) 5)	log book waders	
5)	waders	
<u>5)</u>	bicycle	
7)	back pack	+
3)	water Shorping popp	+
	Sharpies, pens	
	stakes	
10)	Flumes, both big and small	1
10) 11)		
10) 11)) Sampler (Tuesday)	1
9) 10) 11) <mark>SCC</mark>	Team: MB, ZB	
10) 11) <mark>SCC</mark>	Team: MB, ZB vehicle: Cherokee	
10) 11) <mark>SCC</mark> 1)	Team: MB, ZB vehicle: Cherokee ISCO Sampler	
10) 11) SCC 1) 2)	Team: MB, ZB vehicle: Cherokee ISCO Sampler 24 sampling containers	
10) 11) <mark>SCC</mark> 1)	Team: MB, ZB vehicle: Cherokee ISCO Sampler	

APPENDIX B

GROUNDWATER DATA

						FIELD	FIELD PARAMETERS	RS			Organic	nic			MBMG LAB	MBMG LAB Parameters	
							FIELD				Carbon	uo			LAB		
Site	GWIC	DATE	TIME	SWL	FLOW	Нd	SC	TEMP	Еh	Q	DOC	TOC	TDS	Hd	SC	HARDNESS	ALKALINITY
			(HRS)	(FT)	(GPM)		(NMHOS)	(C)	(mv)	MG/I	mg/L	mg/L	mg/L		(NMHOS)	(MG/L)	(MG/L)
BT-98-02	171294	02/14/11	14:30	11.48	3.3	5.80	340	9.24	302	1.75	<0.25	1.82	203	5.94	376	100	26.25
BT-98-02B	240865	02/14/11	16:00	9.86	3.3	6.46	743	10.03	298	4.9	<0.25	1.37	514	6.58	777	320	45.93
BPS07-16A	248566	02/14/11	17:46	7.47	3.3	7.03	143	5.29	295	10.38	<0.25	<0.25	87	6.82	157	58	51.67
BPS07-16B	248565	02/14/11	17:00	8.18	3.3	7.08	284	10.09	294	4.92	<0.25	1.18	190	7.55	326	103	82.02
AMW-03S	137599	02/10/11	14:20	7.62		4.86	408	6.82	541	2.84	<0.25	3.17	386	5.61	594	217	35.27
AMW-03D	137600	137600 02/10/11	15:02	NR		6.59	1,694	7.37	485	3.11	1.94	2.6	968	7.22	1,624	670	370.72
GG99-01	171293	02/10/11	15:48	5.71		6.22	465	4.99	524	3.89	0.72	2.86	294	6.49	516	164	100.88
AMW-04A	162029	02/11/11	11:48	13.61		6.55	789	8.32	440	4.61	<0.25	1.24	482	7.19	834	321	228.01
BT-99-03	171291	02/11/11	13:32	9.1		6.87	533	7.35	451	5.18	<0.25	1.76	306	7.25	579	206	171.42
AMW-10	137602	02/14/11	12:03	5.85		6.67	651	5.69	451	4.38	<0.25	0.77	374	7.17	669	257	174.70
BT-99-01	171289	02/14/11	15:48	5.59		6.94	443	6.75	268	3.63	<0.25	2.14	263	7.16	490	187	127.13
BT-99-02	171290	02/15/11	11:46	7.1	3.3	6.30	417	7.01	464	7.63	<0.25	1.11	237	7.12	459	168	100.88
BT-98-01	171295	02/10/11	14:05	9.83	3.3	7.08	220	10.91	196	2.9	<0.25	0.87	141	7.1	200	81	86.12
MT-98-06	260255	02/10/11	13:00	3.55	3.3	7.04	242	8.09	196	2.08	<0.25	1.4	151	6.94	248	93	88.58
MT-98-05	261583	02/10/11	13:32	5.03	3.3	6.67	353	8.62	183	2.92	<0.25	1.99	213	6.8	369	125	102.52
BERM WELL	260331	02/11/11	15:10	3.75	2	7.05	267	9.7	213	3.81	<0.25	0.61	172	7.03	268	77	86.12
GS-28	150389	02/08/11	14:45	5.3	<1.0	7.06	386	5.56	166	2.65	0.41	2.97	233	7.08	412	138	157.47
AMW-13	137597	02/08/11	13:00	11.58	<1.0	6.76	2,914	6.55	134	2.9	4.11	4.11	2,310	6.56	2,596	1,568	509.33
AMW-13B	240863	02/08/11	12:00	11	3.3	7.79	309	NR	334	2.06	<0.25	2	203	7.17	347	88	82.84
AMW-13C	255975	02/08/11	13:30	10.24	3.3	6.84	834	9.52	167	0.97	<0.25	2.15	615	6.6	851	305	50.85
AMW-11	161962	02/11/11	13:50	6.86	3.3	7.25	334	5.55	195	2.1	<0.25	1.53	206	7.08	364	114	118.92
WELL MF-01	5038	02/18/11	11:20	6.5	3.3	NR	NR	NR	NR	NR	<0.25	1.14	277	7.01	450	162	118.92
QA/QC Samples																	
Field Blank		02/18/11		NR		NR	NR	NR	RN	NR	<0.25	<0.25	7	6.2	1	0	2.46
WELL MF-01 Duplicate	5038	02/18/11	11:22	NR		7.01	462	8.69	336	1.18	<0.25	1.84	276	7.07	467	159	118.92

						MAJ	MAJOR CATIONS	NS				MA	MAJOR ANIONS	SNC		NUT	NUTRIENTS
							Cations						Anions				
Site	GWIC	DATE	TIME	Са	Mg	Na	¥	Fe	Mn	SiO ₂	HCO ₃	co ₃	C	SO_4	Ч	Total N	NO ₃ +NO ₂
			(HRS)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
BT-98-02	171294	02/14/11	14:30	27.10	7.85	17.90	3.19	<0.002	0.10	32.90	31.75	0.00	33.46	55.9	0.55	6.27	5.98
BT-98-02B	240865	02/14/11	16:00	92.00	22.00	23.00	4.18	<0.002	<0.001	31.00	55.67	0.00	13.53	294.2	0.21	5.59	5.25
BPS07-16A	248566	02/14/11	17:46	16.20	4.17	4.93	1.72	0.00	<0.001	12.50	63.45	0.00	4.12	11.3	0.11	<1.0	<0.2
BPS07-16B	248565	02/14/11	17:00	30.60	6.35	15.30	2.28	<0.002	<0.001	31.60	99.68	0.00	5.17	49.9	0.32	<1.0	0.39
AMW-03S	137599	02/10/11	14:20	65.50	13.10	25.60	4.55	<0.002	0.73	14.40	42.83	0.00	21.75	215.0	0.13	1.76	0.60
AMW-03D	137600	02/10/11	15:02	192.00	46.30	96.20	6.32	<0.01	<0.005	30.70	451.50	0.00	122.70	220.7	0.21	120.00	8.01
GG99-01	171293	02/10/11	15:48	47.00	11.40	23.30	6.53	0.02	1.79	20.10	123.40	0.00	20.01	99.8	1.04	<1.0	<0.2
AMW-04A	162029	02/11/11	11:48	91.80	22.30	36.50	3.77	0.00	<0.001	34.60	278.00	0.00	49.52	98.8	0.15	5.51	5.23
ВТ-99-03	171291	02/11/11	13:32	57.80	14.90	25.20	5.29	<0.002	<0.001	26.20	209.00	0.00	30.21	38.6	0.74	3.92	3.80
AMW-10	137602	02/14/11	12:03	75.30	16.70	28.30	5.18	<0.002	<0.001	27.00	213.40	0.00	51.17	59.2	1.95	5.20	4.83
BT-99-01	171289	02/14/11	15:48	56.30	11.20	13.00	4.52	0.08	0.01	25.80	155.40	0.00	21.61	46.6	0.59	4.87	4.66
ВТ-99-02	171290	02/15/11	11:46	48.80	11.10	13.20	3.89	<0.002	<0.001	24.50	122.50	0.00	30.74	36.8	0.34	6.42	6.07
BT-98-01	171295	02/10/11	14:05	23.10	5.69	12.60	2.19	<0.002	<0.001	24.20	104.50	0.00	4.68	14.7	0.23	1.26	0.73
MT-98-06	260255	02/10/11	13:00	26.40	6.53	11.60	2.30	<0.002	<0.001	23.90	108.40	0.00	5.68	19.6	0.19	<1.0	0.95
MT-98-05	261583	02/10/11	13:32	36.30	8.46	18.30	2.34	<0.002	<0.001	25.60	124.60	0.00	10.87	47.0	0.28	2.96	2.81
BERM WELL	260331	02/11/11	15:10	21.90	5.37	23.80	2.89	0.01	<0.001	29.30	105.30	0.00	9.50	25.5	1.27	1.14	0.78
GS-28	150389	02/08/11	14:45	38.60	10.10	21.90	3.99	0.14	0.11	28.80	192.40	0.00	9.63	24.1	0.55	<1.0	<0.2
AMW-13	137597	02/08/11	13:00	475.00	92.90	62.90	42.40	27.90	1.14	19.30	620.70	0.00	24.19	1,259.0	0.16	1.83	<0.2
AMW-13B	240863	02/08/11	12:00	25.20	5.99	25.10	2.76	<0.002	<0.001	29.50	100.60	0.00	6.69	55.9	1.08	<1.0	0.32
AMW-13C	255975	02/08/11	13:30	88.30	20.60	50.30	8.28	<0.002	0.01	41.20	62.32	0.00	7.21	368.3	0.91	<1.0	<0.2
AMW-11	161962	02/11/11	13:50	33.60	7.31	20.70	3.11	0.53	1.26	27.40	144.60	0.00	14.16	26.0	0.96	<1.0	<0.2
WELL MF-01	5038	02/18/11	11:20	46.20	11.30	24.10	3.73	<0.002	0.01	27.80	144.90	0.00	29.81	59.4	0.73	2.28	2.21
QA/QC Samples																	
Field Blank		02/18/11		<0.015	<0.105	<0.124	<0.006	<0.002	<0.001	<0.16	3.26	0.00	<0.5	<2.5	<0.05	<1.0	<0.2
WELL MF-01 Duplicate	5038	02/18/11	11:22	45.40	11.10	23.90	3.66	<0.002	0.01	27.70	144.90	0.00	29.98	59.0	0.72	2.20	2.20

		Ĵ																										
	Hg	(µg/L)	NR	NR	NR	R	NR	NR	NR	NR	NR	NR	NR			NR	NR											
	С	(µg/L)	6.5	1.2	1.8	<0.5	1,058.0	2.7	426.0	1.8	0.9	2.8	1.8	1.8	<0.5	<0.5	0.5	1.7	1.0	<2.5	1.4	2.1	1.2				<0.5	20.7
	J	(µg/L)	<0.2	<0.2	<0.2	0.58	<0.02	<1.0	<0.2	0.44	0.35	0.36	0.37	0.48	0.49	0.32	0.42	0.43	<0.2	<1.0	0.41	<0.2	<1.0	0.26			<0.2	0.26
	C	(µg/L)	<0.2	<0.2	<0.2	<0.2	2.21	<0.9	1.55	0.21	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	0.35	1.00	<0.2	<0.2	1.24	<0.2			<0.2	<0.2
ALS	Cd	(µg/L)	8.64	1.50	0.29	0.34	1.80	<1.0	2.43	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	0.53	<0.2	<1.0	0.28	2.64	0.74	1.30			<0.2	1.34
DISSOLVED METALS	Be	(µg/L)	<0.2	<0.2	<0.2	<0.2	<0.2	<1.0	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<1.0	<0.2	<0.2	<0.2	<0.2			<0.2	<0.2
DISSOL	Ba	(µg/L)	53.90	16.10	12.50	21.50	15.80	44.30	31.20	152.00	112.00	147.00	99.20	106.00	29.90	32.30	36.10	14.90	58.40	49.90	27.20	13.40	1041.00	60.50			<0.2	61.70
	В	(µg/L)	54.40	14.90	25.30	12.80	69.50	108.00	32.60	55.10	89.10	51.50	35.60	32.70	10.40	10.70	21.50	23.90	27.70	2290.00	27.00	21.80	20.10	25.20			<2.0	25.40
	As	(µg/L)	0.96	0.84	1.25	1.50	0.47	2.39	1.02	4.41	1.88	33.70	1.79	2.38	1.12	1.07	1.38	4.58	3.30	5.95 2	3.69	5.69	15.40	3.82			<0.2	4.03
	Ag	(µg/L) (<0.2	<0.2	<0.2	<0.2	<0.2	<1.0	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<1.0	<0.2	<0.2	<0.2	<0.2			<0.2	<0.2
	A	(µg/L)	29.00	<2.0	6.59	5.88	885.00	<10	35.60	5.88	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	13.50	<2.0	<10	<2.0	<2.0	<2.0	<2.0			<2.0	<2.0
	٦	(mg/L)	0.03	0.06	0.04	0.05	<0.025	0.11	0.07	0.12	0.12	0.20	0.13	0.21	0.05	0.05	0.06	0.06	0.09	0.15	0.05	0.07	0.15	0.05			<0.025	0.05
ENTS	TKN	(mg/L)	0.29	0.34	<1.0	<1.0	1.16	111.99	<1.0	0.28	0.12	0.37	0.21	0.35	0.54	<0.05	0.15	0.37	<1.0	1.83	<1.0	<1.0	<1.0	0.07				0.00
NUTRIENTS	NO ₂ -N	(mg/L)	<0.05	<0.05	<0.05	<0.05	0.06	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05			<0.05	<0.05
	NO ₃ -N	(mg/L)	5.98	5.25	0.18	0.39	0.54	8.01	<0.2	5.23	3.80	4.83	4.66	6.07	0.73	0.95	2.81	0.78	0.14	<0.05	0.45	0.16	<0.05	2.21			<0.05	2.34
	TIME	(HRS)	14:30	16:00	17:46	17:00	14:20	15:02	15:48	11:48	13:32	12:03	15:48	11:46	14:05	13:00	13:32	15:10	14:45	13:00	12:00	13:30	13:50	11:20				11:22
	DATE		02/14/11	02/14/11	02/14/11	02/14/11	02/10/11	02/10/11	02/10/11	02/11/11	02/11/11	02/14/11	02/14/11	02/15/11	02/10/11	02/10/11	02/10/11	02/11/11	02/08/11	02/08/11	02/08/11	02/08/11	02/11/11	02/18/11			02/18/11	02/18/11
	GWIC		171294	240865	248566	248565	137599	137600	171293	162029	171291	137602	171289	171290	171295	260255	261583	260331	150389	137597	240863	255975	161962	5038				5038
	Site		BT-98-02	BT-98-02B	BPS07-16A 2	BPS07-16B 2	AMW-03S	AMW-03D	GG99-01	AMW-04A	ВТ-99-03	AMW-10	ВТ-99-01	ВТ-99-02	BT-98-01	MT-98-06	MT-98-05	BERM WELL	GS-28	AMW-13	AMW-13B	AMW-13C	AMW-11	WELL MF-01		QA/QC Samples	Field Blank	WELL MF-01 Duplicate

						Δ	DISSOLVED METALS	D METAI	S					R/	RARE EARTH	王		
Site	GWIC	DATE	TIME		Мо	ïz	Pb	Se	Sr	∍	Zn	Ce	Cs	Ga	La	qN	pN	Pd
			(HRS)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)
BT-98-02	171294	02/14/11	14:30	25.50	<0.2	11.90	<0.2	0.84	249	<0.2	2,685.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
BT-98-02B	240865	02/14/11	16:00	9.83	4.34	0.88	<0.2	1.01	526	0.67	62.8	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
BPS07-16A	248566	02/14/11	17:46	3.70	0.97	0.33	<0.2	0.20	106	0.39	113.0	<0.2	<0.2	<0.2	<0.2	<0.5	<0.2	<0.5
BPS07-16B	248565	02/14/11	17:00	<2.0	22.30	0.25	<0.2	0.48	221	5.18	9.4	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
AMW-03S	137599	02/10/11	14:20	2.51	1.11	2.29	0.49	0.59	276	5.34	135.0	9.35	<0.5	<0.2	5.44	<0.5	3.47	<0.5
AMW-03D	137600	02/10/11	15:02	12.10	5.22	1.35	<1.0	1.63	1,043	108.00	<5	<1.0	<2.5	6.0>	<1.0	<2.5	<1.0	<2.5
GG99-01	171293	02/10/11	15:48	5.38	3.84	4.20	<0.2	0.45	286	1.17	1,063.0	0.43	<0.5	<0.2	0.31	<0.5	<0.2	<0.5
AMW-04A	162029	02/11/11	11:48	7.87	3.85	0.67	<0.2	0.99	606	41.40	<1.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
BT-99-03	171291	02/11/11	13:32	3.90	5.12	0.40	<0.2	1.12	393	19.70	<1.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
AMW-10	137602	02/14/11	12:03	4.73	5.26	0.67	<0.2	0.92	503	30.20	<1.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
BT-99-01	171289	02/14/11	15:48	4.28	8.17	0.50	<0.2	0.76	253	21.00	<1.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
ВТ-99-02	171290	02/15/11	11:46	3.84	2.35	0.36	<0.2	0.57	311	3.53	1.8	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
BT-98-01	171295	02/10/11	14:05	<2.0	8.18	<0.2	<0.2	0.27	171	2.56	<1.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
MT-98-06	260255	02/10/11	13:00	<2.0	7.44	<0.2	<0.2	0.32	188	3.30	<1.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
MT-98-05	261583	02/10/11	13:32	2.19	15.00	<0.2	<0.2	0.64	239	7.70	<1.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
BERM WELL	260331	02/11/11	15:10	9.58	38.30	0.22	<0.2	0.51	201	4.50	61.4	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
GS-28	150389	02/08/11	14:45	14.80	32.80	0.35	<0.2	0.32	362	12.20	21.3	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
AMW-13	137597	02/08/11	13:00	79.80	1.24	3.06	<1.0	<0.9	4,410	1.79	197.0	<1.0	<2.5	<0.9	<1.0	<2.5	<1.0	<2.5
AMW-13B	240863	02/08/11	12:00	6.60	30.80	0.20	<0.2	0.45	199	3.45	25.1	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
AMW-13C	255975	02/08/11	13:30	37.60	158.00	1.21	<0.2	0.30	695	1.60	251.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
AMW-11	161962	02/11/11	13:50	9.70	11.90	0.67	1.04	0.20	291	1.66	121.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
WELL MF-01	5038	02/18/11	11:20	12.60	10.70	0.36	<0.2	0.73	411	6.52	125.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
QA/QC Samples																		
Field Blank		02/18/11		<2.0	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<1.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5
WELL MF-01 Duplicate	5038	02/18/11	11:22	12.70	10.70	0.35	<0.2	0.79	416	6.76	129.0	<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.5

							RARE EARTH	EARTH		
Site	GWIC	DATE	TIME	Pr	Rb	П	Th	Sn	ц	>
			(HRS)	(µg/L)	(µg/L)	(µg/L)	$(\mu g/L)$	(µg/L)	(μg/L)	(µg/L)
	171294	02/14/11	14:30	<0.2	<0.5	<0.2	<0.2	<0.5	0.75	<0.5
BT-98-02B	240865	02/14/11	16:00	<0.2	1.10	<0.2	<0.2	<0.5	3.90	<0.2
3PS07-16A	248566	02/14/11	17:46	<0.2	<0.5	<0.2	<0.2	<0.5	0.46	<0.2
BPS07-16B	248565	02/14/11	17:00	<0.2	0.93	<0.2	<0.2	<0.5	06.0	1.02
AMW-03S	137599	02/10/11	14:20	0.99	1.74	<0.2	<0.2	<0.5	3.05	<0.2
AMW-03D	137600	02/10/11	15:02	<1.0	<2.5	<1.0	<1.0	<2.5	3.79	1.73
	171293	02/10/11	15:48	<0.2	0.93	<0.2	<0.2	1.54	2.14	<0.2
AMW-04A	162029	02/11/11	11:48	<0.2	<0.5	<0.2	<0.2	4.55	2.06	0.33
BT-99-03	171291	02/11/11	13:32	<0.2	<0.5	<0.2	<0.2	3.61	0.58	<0.2
AMW-10	137602	02/14/11	12:03	<0.2	<0.5	<0.2	<0.2	4.03	0.89	<0.2
BT-99-01	171289	02/14/11	15:48	<0.2	<0.5	<0.2	<0.2	3.30	0.66	<0.2
	171290	02/15/11	11:46	<0.2	<0.5	<0.2	<0.2	3.07	0.58	<0.2
	171295	02/10/11	14:05	<0.2	<0.5	<0.2	<0.2	<0.5	0.28	1.62
MT-98-06	260255	02/10/11	13:00	<0.2	<0.5	<0.2	<0.2	<0.5	0.30	1.03
MT-98-05	261583	02/10/11	13:32	<0.2	<0.5	<0.2	<0.2	<0.5	0.71	0.64
3ERM WELL	260331	02/11/11	15:10	<0.2	1.30	<0.2	<0.2	<0.5	0.92	5.75
	150389	02/08/11	14:45	<0.2	<0.5	<0.2	<0.2	<0.5	0.46	0.59
AMW-13	137597	02/08/11	13:00	<1.0	17.00	<1.0	<1.0	<2.5	19.20	<1.0
AMW-13B	240863	02/08/11	12:00	<0.2	0.98	<0.2	<0.2	<0.5	0.81	13.30
AMW-13C	255975	02/08/11	13:30	<0.2	5.26	<0.2	<0.2	<0.5	4.38	0.43
AMW-11	161962	02/11/11	13:50	<0.2	0.51	<0.2	<0.2	<0.5	0.32	2.53
WELL MF-01	5038	02/18/11	11:20	<0.2	<0.5	<0.2	<0.2	<0.5	0.86	3.68
QA/QC Samples										
Field Blank		02/18/11		<0.2	<0.5	<0.2	<0.2	<0.5	<0.2	<0.2
WELL ME-01 Duplicate	5038	02/18/11	11.77	< 0 >	ц С	< 0 >	< 0 >	ч С/	0.86	2 7 2

APPENDIX C

SURFACE-WATER DATA

						NAV-GPS	NAV-GPS Coordinates			FLOW	
Site Name	Distance	Stream	Type	Sample	GWIC	Lat	Long	DATE	Measu	Measured Flow	Calculated Flow
	(km)			Q	₽	Decima	Decimal Degrees		(cfs)	notes	(cfs)
C-12 TR	0.31	Tributary	Drivepoint	200837	262795	45.9893060	-112.5219890	9/21/11 11:20	na		
C-8.5 TR	0.89	Tributary	Drivepoint	200836	262805	45.9917860	-112.5283220	9/21/11 10:55	na		
C-8	1.00	Primary	Drivepoint	200835	262804	45.9921550	-112.5298490	9/21/11 10:10	na		
C-7.5 TR	1.05	Tributary	Drivepoint	200838	262803	45.9931230	-112.5328300	9/21/11 8:55	na		
C-6	1.20	Primary	Drivepoint	200839	262800	45.9930470	-112.5321580	9/21/11 9:25	na		
C-7.5 POND	1.01	Pond	Surface	200799	262802	45.9925810	-112.5296670	9/21/11 10:28	na		
I-0	0.00	Primary	Surface	200823	262809	45.9878290	-112.5186340	9/21/11 13:03	10.3721	Very Good	12.0391
C-12 US	0.24	Primary	Surface	200821	262796	45.9889780	-112.5212960	9/21/11 12:52	10.1238	Very Good	12.0391
C-12 DS	0.39	Primary	Surface	200819	262793	45.9895110	-112.5229340	9/21/11 12:46	11.6812	Very Good	12.2028
C-11 US	0.48	Primary	Surface	200811	262791	45.9899270	-112.5239740	9/21/11 11:45	11.6718	Very Good	12.7215
C-11 DS	0.59	Primary	Surface	200807	262789	45.9904350	-112.5253210	9/21/11 11:16	12.9308	ОК	12.9977
C-9 US	0.83	Primary	Surface	200805	262807	45.9914780	-112.5279250	9/21/11 11:07	12.4177	ОК	13.5879
C-9 DS	0.86	Primary	Surface	200803	262806	45.9916620	-112.5282890	9/21/11 11:01	na		13.5367
C-8	1.00	Primary	Surface	200797	262804	45.9921550	-112.5298490	9/21/11 10:24	11.1156	Very Good	13.7439
C-7	1.13	Primary	Surface	200793	262801	45.9927610	-112.5314250	9/21/11 10:08	11.7164	Very Good	13.6915
C-6	1.20	Primary	Surface	200791	262800	45.9930470	-112.5321580	9/21/11 9:55	12.9092	Very Good	13.7967
C-5	1.31	Primary	Surface	200787	262798	45.9935380	-112.5333580	9/21/11 9:38	12.6594	ОК	14.4054
C-4.5	1.47	Primary	Surface	200785	262797	45.9943120	-112.5350410	9/21/11 9:27	11.2747		14.5809
SS-04.5	1.56	Primary	Surface	200783	127593	45.9946292	-112.5361219	9/21/11 9:16	12.2859	Good	14.3479
SS-04.5	1.65	Primary	Surface	200775	262810	45.9951480	-112.5371380	9/21/11 8:38	11.7803		14.2908
SS-05	1.82	Primary	Surface	200773	127536	45.9957626	-112.5391870	9/21/11 8:17	11.2747	Very Good	14.2341
SS-05A	2.66	Primary	Surface	200778	249187	45.9962074	-112.5442602	9/21/11 8:50	na		13.7439
SS-06A	3.00	Primary	Surface	200779	217884	45.9944757	-112.5517715	9/21/11 8:55	na		14.2341
C-12 TR	0.31	Tributary	Surface	200816	262795	45.9893060	-112.5219890	9/21/11 12:40	-2.97E-02	1.5574	-2.97E-02
SAND CREEK	0.41	Tributary	Surface	200813	262812	45.98944	-112.52333	9/21/11 11:50	0.00E+00	assume	0.00E+00
C-11 TR	0.51	Tributary	Surface	200809	262790	45.9901410	-112.5243680	9/21/11 11:21	1.81E-01		1.81E-01
C-9 TR GG	0.85	Tributary	Surface	200827	262808	45.9910070	-112.5286920	9/21/11 13:32	-5.40E-03		-5.40E-03
C-8.5 TR	0.89	Tributary	Surface	200801	262805	45.9917860	-112.5283220	9/21/11 10:56	2.59E-01		2.59E-01
C-7.5 TR	1.05	Tributary	Surface	200795	262803	45.9926890	-112.5309570	9/21/11 10:14	4.32E-02		4.32E-02
C-5 TR	1.25	Tributary	Surface	200789	262799	45.9931230	-112.5328300	9/21/11 9:47	3.57E-01		3.57E-01
MSD-B	1.58	Tributary	Surface	200781	262811	45.9952670	-112.5359320	9/21/11 9:11	0.00E+00	very close	0.00E+00

					4	HYSICAL	PHYSICAL PARAMETERS	ERS				MAJOR CATIOS	CATIOS	
Site Name	Distance	Stream	Ηd	sc	TEMP		DO	РН	sc	Hardness	Са	Ca, TR	Mg	Mg, TR
	(km)			(SOHMU)	(C)	(mv)	(mg/L)		(SOHMU)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
			Field	Field	Field	Field	Field	LAB	LAB		Dissolved	TR	Dissolved	TR
C-12 TR	0.31	Tributary	NR	NR	NR	NR	NR	7.18	298.90		29.30	NR	7.49	NR
C-8.5 TR	0.89	Tributary	NR	NR	NR	NR	NR	7.13	344.50		31.61	NR	7.32	NR
C-8	1.00	Primary	NR	NR	NR	NR	NR	7.59	848.10		33.21	NR	7.80	NR
C-7.5 TR	1.05	Tributary	NR	NR	NR	NR	NR	7.19	329.00		28.03	NR	6.98	NR
C-6	1.20	Primary	NR	NR	NR	NR	NR	7.48	140.40		41.11	NR	10.04	NR
C-7.5 POND	1.01	Pond	7.47	381.70	9.93	372.00	2.92	7.51	415.70		41.52	44.16	11.63	13.26
0-1	0.00	Primary	7.69	299.70	10.63	406.00	10.93	7.74	384.20	124.78	35.63	38.48	8.70	9.29
C-12 US	0.24	Primary	7.41	307.60	9.85	408.00	10.48	7.73	390.40	126.53	36.66	38.72	8.50	9.30
C-12 DS	0.39	Primary	7.49	286.20	13.08	400.00	9.11	7.71	369.70	127.40	36.88	38.90	8.58	9.32
C-11 US	0.48	Primary	7.31	306.90	10.61	399.00	9.58	7.67	339.00	126.96	36.80	36.71	8.52	8.82
C-11 DS	0.59	Primary	7.46	312.60	9.01	360.00	9.78	7.73	345.50	127.40	37.03	37.81	8.52	9.07
C-9 US	0.83	Primary	7.48	311.90	8.84	354.00	9.71	7.66	339.60	127.16	36.93	38.39	8.49	9.24
C-9 DS	0.86	Primary	7.45	310.20	9.23	353.00	9.30	7.73	335.10	127.90	37.08	38.06	8.58	9.15
C-8	1.00	Primary	7.38	312.00	8.15	376.00	8.98	7.59	334.50	127.24	36.98	37.69	8.48	9.05
C-7	1.13	Primary	7.49	305.70	8.77	369.00	8.68	7.58	342.30	127.55	37.07	38.20	8.50	9.18
C-6	1.20	Primary	7.51	311.50	7.90	376.00	8.87	7.56	338.50	128.50	37.35	38.17	8.56	9.11
C-5	1.31	Primary	7.47	313.20	7.74	367.00	8.63	7.58	320.00	126.44	36.66	37.44	8.48	9.07
C-4.5	1.47	Primary	7.50	313.90	7.68	370.00	8.55	7.55	319.40	128.42	36.66	36.49	8.96	8.86
SS-04.5	1.56	Primary	7.43	314.40	7.60	365.00	8.30	7.53	312.50	128.58	36.66	37.46	9.00	9.05
SS-04.5	1.65	Primary	7.43	309.70	7.45	361.00	8.14	7.50	336.50	128.17	36.61	37.83	8.93	9.17
SS-05	1.82	Primary	7.18	313.30	7.51	372.00	7.96	7.43	328.60	127.86	36.50	36.64	8.92	8.94
SS-05A	2.66	Primary	NR	NR	NR	NR	NR	7.56	313.80	130.41	37.21	37.61	9.11	9.13
SS-06A	3.00	Primary	7.56	323.90	7.41	359.00	8.44	7.59	346.00	131.70	37.58	38.47	9.20	9.35
C-12 TR	0.31	Tributary	7.40	462.20	12.72	403.00	5.85	7.48	506.10	154.66	56.61	59.75	11.55	12.49
SAND CREEK	0.41	Tributary	7.14	363.70	9.35	397.00	9.72	7.57	395.70	147.10	42.61	41.93	9.89	10.11
C-11 TR	0.51	Tributary	6.92	412.70	9.08	366.00	7.19	7.15	456.90	163.20	48.23	48.41	10.39	10.84
C-9 TR GG	0.85	Tributary	7.17	418.40	11.99	409.00	10.89	7.65	454.50	143.20	40.29	39.95	10.35	10.75
C-8.5 TR	0.89	Tributary	7.03	322.80	12.43	291.00	8.49	7.21	349.00	121.71	35.87	36.09	7.81	8.25
C-7.5 TR	1.05	Tributary	7.55	383.00	9.95	367.00	2.03	7.59	391.20	154.13	41.27	40.85	12.41	12.95
C-5 TR	1.25	Tributary	8.24	349.20	9.73	368.00	5.53	7.95	353.40	125.40	32.07	35.63	11.01	12.51
MSD-B	1.58	Tributary	7.21	479.60	8.95	364.00	6.79	7.16	492.40	173.01	48.73	49.24	12.47	12.77

						MAJOR CATIONS	ATIONS				1	ANIONS	
Site Name	Distance	Stream	Na	Na, TR	х	K, TR	Fe	Fe, TR	Mn	Mn, TR	HCO3	CO3	Br
	(km)		(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(ng/L)
			Dissolved	TR	Dissolved	TR	DISS	TR	DISS	TR	DISS		Dissolved
C-12 TR	0.31	Tributary	11.32	NR	3.33	NR	<0.002 U	NR	<0.001 U	NR	123.08		113.00
C-8.5 TR	0.89	Tributary	17.22	NR	3.35	NR	0.10	NR	0.01	NR	116.93		81.00
C-8	1.00	Primary	14.64	NR	4.04	NR	3.55	NR	0.83	NR	161.64		121.00
C-7.5 TR	1.05	Tributary	17.50	NR	3.08	NR	0.008 J	NR	<0.001 U	NR	110.95		112.00
C-6	1.20	Primary	14.00	NR	3.92	NR	2.07	NR	1.24	NR	167.98		114.00
C-7.5 POND	1.01	Pond	18.89	20.67	4.78	5.77	0.10	2.94	0.34	0.44	173.56		81.00
1-0	0.00	Primary	11.74	12.15	2.80	2.95	0.06	0.50	0.04	0.05	125.97		87
C-12 US	0.24	Primary	12.55	13.20	2.67	3.00	0.06	0.45	0.04	0.05	127.33		3070
C-12 DS	0.39	Primary	12.42	13.21	2.75	3.01	0.05	0.46	0.04	0.05	126.68		3030
C-11 US	0.48	Primary	12.17	12.33	2.78	2.92	0.06	0.50	0.04	0.05	128.07		2910
C-11 DS	0.59	Primary	12.26	13.25	2.76	2.96	0.05	0.43	0.04	0.05	127.62		2850
C-9 US	0.83	Primary	12.26	13.76	2.73	3.05	0.05	0.56	0.05	0.06	128.49		2730
C-9 DS	0.86	Primary	12.22	13.54	2.74	3.01	0.09	0.47	0.05	0.06	127.62		2740
C-8	1.00	Primary	12.22	13.80	2.78	2.96	0.08	0.52	0.05	0.06	126.84		2700
C-7	1.13	Primary	12.33	13.84	2.76	3.01	0.07	0.57	0.06	0.07	127.69		2710
C-6	1.20	Primary	12.67	13.58	2.71	2.97	0.10	0.43	0.06	0.07	127.81		2690
C-5	1.31	Primary	12.53	13.79	2.81	2.99	0.08	0.47	0.06	0.07	128.24		2580
C-4.5	1.47	Primary	13.85	13.35	2.89	2.88	0.08	0.39	0.06	0.06	128.80		2550
SS-04.5	1.56	Primary	13.77	13.54	2.89	3.04	0.12	0.42	0.06	0.07	129.31		2590
SS-04.5	1.65	Primary	13.76	13.76	2.92	3.07	0.09	0.43	0.06	0.07	129.32		2600
SS-05	1.82	Primary	13.59	13.63	2.94	2.99	0.10	0.40	0.06	0.07	129.06		2610
SS-05A	2.66	Primary	14.90	14.37	2.96	3.06	0.09	0.51	0.07	0.08	129.49		2700
SS-06A	3.00	Primary	15.00	14.99	2.95	3.07	0.08	0.41	0.07	0.09	130.21		2610
C-12 TR	0.31	Tributary	23.06	24.25	3.60	3.89	0.006 J	0.33	0.05	0.16	179.80		418
SAND CREEK	0.41	Tributary	14.41	14.76	3.44	3.57	0.02	0.82	0.10	0.10	146.94		1140
C-11 TR	0.51	Tributary	19.36	19.64	3.20	3.38	0.01	0.27	0.09	0.10	139.79		177
C-9 TR GG	0.85	Tributary	15.79	16.33	3.29	3.39	0.03	0.59	0.12	0.14	140.34		2100
C-8.5 TR	0.89	Tributary	16.09	17.15	2.63	3.02	0.07	0.40	0.11	0.13	103.03		81
C-7.5 TR	1.05	Tributary	18.93	19.79	4.77	5.07	0.06	0.54	0.27	0.31	178.61		80
C-5 TR	1.25	Tributary	21.79	23.67	4.60	5.38	0.16	4.68	0.08	0.32	148.78		121
MSD-B	1.58	Tributary	29.98	29.65	6.42	6.63	0.07	1.63	0.24	0.32	126.84		149

			ANIC	ANIONS			NON-METALS		
Site Name	Distance	Stream	C	S04	SiO2	NO3-N	PO4	Carbon	Carbon
	(km)		(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
			DISS	DISS	Dissolved	Dissolved	Dissolved	TOC	DOC
C-12 TR	0.31	Tributary	6.86	20.59	25.26	0.61	0.12	NR	NR
C-8.5 TR	0.89	Tributary	7.34	43.65	30.90	0.14	0.27	NR	NR
C-8	1.00	Primary	8.51	11.48	30.30	<0.010 U	<0.020 U	NR	NR
C-7.5 TR	1.05	Tributary	6.00	41.22	26.11	0.40	0.14	NR	NR
C-6	1.20	Primary	12.84	26.12	28.08	<0.010 U	0.16	NR	NR
C-7.5 POND	1.01	Pond	8.82	45.31	21.22	<0.010 U	<0.020 U	NR	NR
1-0	0.00	Primary	12.62	31.07	23.53	1.14	<0.020 U	2.96	2.96
C-12 US	0.24	Primary	12.71	31.73	24.91	1.22	<0.020 U	2.92	2.92
C-12 DS	0.39	Primary	12.77	31.40	24.26	1.21	<0.020 U	NR	NR
C-11 US	0.48	Primary	12.71	31.26	24.75	1.20	<0.020 U	4.24	2.80
C-11 DS	0.59	Primary	12.75	32.43	24.63	1.23	<0.020 U	NR	NR
C-9 US	0.83	Primary	12.78	32.24	24.73	1.20	<0.020 U	2.70	2.70
C-9 DS	0.86	Primary	12.72	32.08	24.20	1.21	<0.020 U	NR	NR
C-8	1.00	Primary	12.58	32.83	24.71	1.18	<0.020 U	NR	NR
C-7	1.13	Primary	12.47	32.22	24.62	1.16	<0.020 U	NR	NR
C-6	1.20	Primary	12.48	32.17	25.17	1.15	<0.020 U	NR	NR
C-5	1.31	Primary	12.58	32.19	23.84	1.10	<0.020 U	NR	NR
C-4.5	1.47	Primary	12.60	32.39	23.47	1.09	<0.020 U	NR	NR
SS-04.5	1.56	Primary	12.57	32.35	23.29	1.12	<0.020 U	3.10	3.10
SS-04.5	1.65	Primary	12.45	32.14	23.57	1.08	<0.020 U	2.79	2.79
SS-05	1.82	Primary	12.47	32.16	23.26	1.08	<0.020 U	2.69	2.69
SS-05A	2.66	Primary	13.94	33.02	23.35	1.07	<0.020 U	NR	NR
SS-06A	3.00	Primary	14.12	33.41	23.04	1.07	<0.020 U	NR	NR
C-12 TR	0.31	Tributary	18.71	69.45	27.82	1.05	0.12	3.20	3.20
SAND CREEK	0.41	Tributary	17.72	36.50	25.38	0.87	<0.020 U	2.19	2.19
C-11 TR	0.51	Tributary	13.85	70.26	26.68	2.18	<0.020 U	1.38	1.38
C-9 TR GG	0.85	Tributary	18.98	38.18	23.21	0.99	<0.020 U	2.95	2.95
C-8.5 TR	0.89	Tributary	8.09	64.75	30.02	0.75	0.13	1.43	1.43
C-7.5 TR	1.05	Tributary	8.81	44.67	20.73	<0.010 U	0.11	3.77	3.77
C-5 TR	1.25	Tributary	16.74	33.43	4.75	<0.010 U	<0.020 U	5.87	5.87
MSD-B	1.58	Tributary	17.66	110.50	18.16	0.07	<0.020 U	NR	NR

						MINOR	MINOR AND TRACEMETALS	EMETALS			
Site Name	Distance	Stream	Ag	Ag, TR	AI	AI, TR	As	As, TR	В	B, TR	Ba
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
			Dissolved	TR	Dissolved	TR	Dissolved	TR	Dissolved	TR	Dissolved
C-12 TR	0.31	Tributary	<0.100 U	NR	2.35	NR	2.64	NR	12.54	NR	33.41
C-8.5 TR	0.89	Tributary	<0.100 U	NR	2.72	NR	7.34	NR	20.09	NR	28.88
C-8	1.00	Primary	<0.100 U	NR	4.08	NR	14.54	NR	17.16	NR	66.81
C-7.5 TR	1.05	Tributary	<0.100 U	NR	4.30	NR	1.93	NR	22.57	NR	3.70
C-6	1.20	Primary	<0.100 U	NR	14.13	NR	16.28	NR	23.03	NR	54.46
C-7.5 POND	1.01	Pond	<0.100 U	<0.250 U	16.94	1754.18	6.41	11.36	39.64	NR	29.79
I-0	0.00	Primary	<0.100 U	<0.250 U	0.722 J	66.49	2.89	3.80	19.20	NR	45.38
C-12 US	0.24	Primary	<0.100 U	<0.250 U	0.782 J	54.23	7.25	7.32	16.39	NR	45.22
C-12 DS	0.39	Primary	<0.100 U	<0.250 U	0.651 J	50.85	7.13	7.44	17.36	NR	45.01
C-11 US	0.48	Primary	<0.100 U	<0.250 U	0.928 J	105.74	6.64	7.20	17.84	NR	44.87
C-11 DS	0.59	Primary	8.78	<0.250 U	0.603 J	74.30	6.78	7.25	17.86	NR	44.86
C-9 US	0.83	Primary	<0.100 U	<0.250 U	0.603 J	142.17	6.65	7.50	18.05	NR	44.88
C-9 DS	0.86	Primary	<0.100 U	1.44	2.30	106.13	6.69	7.23	17.70	NR	45.83
C-8	1.00	Primary	<0.100 U	<0.250 U	12.18	134.99	7.31	7.76	17.96	NR	45.11
C-7	1.13	Primary	<0.100 U	<0.250 U	L 866.0	144.74	6.88	7.72	18.26	NR	45.60
C-6	1.20	Primary	<0.100 U	<0.250 U	1.570 J	81.95	6.79	7.35	19.29	NR	46.22
C-5	1.31	Primary	4.35	<0.250 U	8.00	105.34	6.83	7.61	22.09	NR	45.39
C-4.5	1.47	Primary	<0.100 U	<0.250 U	18.42	52.56	7.13	7.58	20.07	NR	45.56
SS-04.5	1.56	Primary	<0.100 U	<0.250 U	14.52	53.07	7.21	7.68	21.25	NR	46.18
SS-04.5	1.65	Primary	<0.100 U	<0.250 U	0.924 J	67.41	10.45	9.88	20.63	NR	46.41
SS-05	1.82	Primary	<0.100 U	<0.250 U	11.66	64.76	7.13	7.44	20.84	NR	46.45
SS-05A	2.66	Primary	<0.100 U	<0.250 U	12.98	119.81	8.05	10.70	22.41	NR	46.81
SS-06A	3.00	Primary	<0.100 U	<0.250 U	14.71	93.11	7.65	8.19	22.02	NR	46.87
C-12 TR	0.31	Tributary	<0.100 U	<0.250 U	0.610 J	91.14	4.63	8.03	39.63	NR	53.39
SAND CREEK	0.41	Tributary	0.231 J	<0.250 U	12.95	323.47	4.66	6.30	22.45	NR	52.83
C-11 TR	0.51	Tributary	<0.100 U	<0.250 U	11.57	100.34	2.68	3.05	26.37	NR	35.77
C-9 TR GG	0.85	Tributary	<0.100 U	<0.250 U	15.76	46.16	7.64	11.09	47.46	NR	52.79
C-8.5 TR	0.89	Tributary	<0.100 U	<0.250 U	4.12	176.47	3.04	3.71	16.83	NR	22.32
C-7.5 TR	1.05	Tributary	<0.100 U	<0.250 U	7.25	250.94	7.70	7.43	42.64	NR	43.15
C-5 TR	1.25	Tributary	1.16	<0.250 U	1.350 J	1516.23	8.63	20.00	30.58	NR	42.21
MSD-B	1.58	Tributary	<0.100 U	<0.250 U	19.86	997.89	6.77	14.67	132.74	NR	39.60

					MIM	MINOR AND TRACE METAI	ACE META	LS LS		
Site Name	Distance	Stream	Ba, TR	Be	Be, TR	Br	Cd	Cd, TR	Ce	Ce, TR
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
			TR	Dissolved	TR	Dissolved	Dissolved	TR	Dissolved	TR
C-12 TR	0.31	Tributary	NR	<0.100 U	NR	113.00	<0.100 U	NR	<0.100 U	NR
C-8.5 TR	0.89	Tributary	NR	<0.100 U	NR	81.00	<0.100 U	NR	<0.100 U	NR
C-8	1.00	Primary	NR	<0.100 U	NR	121.00	<0.100 U	NR	<0.100 U	NR
C-7.5 TR	1.05	Tributary	NR	<0.100 U	NR	112.00	0.130 J	NR	<0.100 U	NR
C-6	1.20	Primary	NR	<0.100 U	NR	114.00	<0.100 U	NR	<0.100 U	NR
C-7.5 POND	1.01	Pond	76.96	<0.100 U	<0.250 U	81.00	<0.100 U	0.760 J	<0.100 U	3.39
I-0	0.00	Primary	49.05	<0.100 U	<0.250 U	87.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-12 US	0.24	Primary	48.40	<0.100 U	<0.250 U	3070.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-12 DS	0.39	Primary	49.69	<0.100 U	<0.250 U	3030.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-11 US	0.48	Primary	50.24	<0.100 U	<0.250 U	2910.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-11 DS	0.59	Primary	50.63	<0.100 U	<0.250 U	2850.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-9 US	0.83	Primary	52.96	<0.100 U	<0.250 U	2730.00	<0.100 U	<0.250 U	<0.100 U	0.290 J
C-9 DS	0.86	Primary	50.16	<0.100 U	<0.250 U	2740.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-8	1.00	Primary	50.13	<0.100 U	<0.250 U	2950.00	<0.100 U	<0.250 U	<0.100 U	0.270 J
C-7	1.13	Primary	52.66	<0.100 U	<0.250 U	2710.00	<0.100 U	<0.250 U	<0.100 U	0.290 J
C-6	1.20	Primary	49.87	<0.100 U	<0.250 U	2690.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-5	1.31	Primary	50.60	<0.100 U	<0.250 U	2580.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-4.5	1.47	Primary	48.34	<0.100 U	<0.250 U	2550.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
SS-04.5	1.56	Primary	50.35	<0.100 U	<0.250 U	2590.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
SS-04.5	1.65	Primary	50.44	<0.100 U	<0.250 U	2600.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
SS-05	1.82	Primary	49.43	<0.100 U	<0.250 U	2610.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
SS-05A	2.66	Primary	50.42	<0.100 U	<0.250 U	2700.00	<0.100 U	<0.250 U	<0.100 U	0.250 J
SS-06A	3.00	Primary	52.04	<0.100 U	<0.250 U	2610.00	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-12 TR	0.31	Tributary	63.49	<0.100 U	<0.250 U	4.18E+02	<0.100 U	<0.250 U	<0.100 U	<0.250 U
SAND CREEK	0.41	Tributary	65.58	<0.100 U	<0.250 U	1.14E+03	<0.100 U	<0.250 U	<0.100 U	0.640 J
C-11 TR	0.51	Tributary	40.37	<0.100 U	<0.250 U	1.77E+02	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-9 TR GG	0.85	Tributary	56.95	<0.100 U	<0.250 U	2.10E+03	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-8.5 TR	0.89	Tributary	26.50	<0.100 U	<0.250 U	8.10E+01	0.200 J	0.610 J	<0.100 U	0.370 J
C-7.5 TR	1.05	Tributary	47.07	<0.100 U	<0.250 U	8.00E+01	<0.100 U	<0.250 U	<0.100 U	0.520 J
C-5 TR	1.25	Tributary	86.80	<0.100 U	<0.250 U	1.21E+02	<0.100 U	0.550 J	<0.100 U	3.00
MSD-B	1.58	Tributary	54.21	<0.100 U	<0.250 U	1.49E+02	<0.100 U	L 077.0	<0.100 U	1.93

					MINOF	MINOR AND TRACE METALS	METALS			
Site Name	Distance	Stream	Co	Co, TR	Cr	Cr, TR	Cs	Cs, TR	Cu	Cu, TR
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
			Dissolved	TR	Dissolved	TR	Dissolved	TR	Dissolved	TR
C-12 TR	0.31	Tributary	<0.100 U	NR	0.210 J	NR	<0.100 U	NR	0.51	NR
C-8.5 TR	0.89	Tributary	<0.100 U	NR	0.160 J	NR	<0.100 U	NR	0.55	NR
C-8	1.00	Primary	0.100 J	NR	0.180 J	NR	<0.100 U	NR	0.360 J	NR
C-7.5 TR	1.05	Tributary	<0.100 U	NR	0.480 J	NR	<0.100 U	NR	0.50	NR
C-6	1.20	Primary	<0.100 U	NR	0.170 J	NR	<0.100 U	NR	0.190 J	NR
C-7.5 POND	1.01	Pond	0.210 J	0.960 J	0.150 J	1.030 J	<0.100 U	0.710 J	0.79	39.44
0-1	0.00	Primary	0.210 J	<0.250 U	0.180 J	0.300 J	<0.100 U	<0.250 U	1.40	2.48
C-12 US	0.24	Primary	0.340 J	<0.250 U	0.180 J	0.290 J	<0.100 U	<0.250 U	1.43	2.30
C-12 DS	0.39	Primary	0.340 J	<0.250 U	0.220 J	0.500 J	<0.100 U	<0.250 U	1.40	2.38
C-11 US	0.48	Primary	0.170 J	<0.250 U	0.250 J	0.390 J	<0.100 U	<0.250 U	1.39	2.91
C-11 DS	0.59	Primary	0.340 J	<0.250 U	0.220 J	0.330 J	<0.100 U	<0.250 U	1.37	4.10
C-9 US	0.83	Primary	0.260 J	<0.250 U	0.250 J	0.360 J	<0.100 U	<0.250 U	1.82	22.58
C-9 DS	0.86	Primary	0.130 J	<0.250 U	0.240 J	0.350 J	<0.100 U	<0.250 U	1.45	6.20
C-8	1.00	Primary	0.110 J	<0.250 U	0.210 J	0.340 J	<0.100 U	<0.250 U	1.33	4.60
C-7	1.13	Primary	0.250 J	<0.250 U	0.210 J	0.490 J	<0.100 U	<0.250 U	1.31	8.92
C-6	1.20	Primary	0.120 J	<0.250 U	0.210 J	0.330 J	<0.100 U	<0.250 U	1.41	3.65
C-5	1.31	Primary	0.120 J	<0.250 U	0.180 J	0.320 J	<0.100 U	<0.250 U	1.34	4.54
C-4.5	1.47	Primary	0.140 J	<0.250 U	0.180 J	0.310 J	<0.100 U	<0.250 U	1.16	3.30
SS-04.5	1.56	Primary	0.140 J	<0.250 U	0.180 J	0.310 J	<0.100 U	<0.250 U	1.29	4.10
SS-04.5	1.65	Primary	0.130 J	<0.250 U	0.270 J	0.310 J	<0.100 U	<0.250 U	1.32	3.20
SS-05	1.82	Primary	0.240 J	<0.250 U	0.230 J	0.340 J	<0.100 U	<0.250 U	2.57	4.09
SS-05A	2.66	Primary	0.100 J	<0.250 U	0.220 J	0.350 J	<0.100 U	<0.250 U	2.84	7.52
SS-06A	3.00	Primary	<0.100 U	<0.250 U	0.230 J	0.400 J	<0.100 U	<0.250 U	3.61	7.94
C-12 TR	0.31	Tributary	0.380 J	<0.250 U	0.150 J	0.300 J	<0.100 U	<0.250 U	0.94	3.44
SAND CREEK	0.41	Tributary	0.390 J	0.270 J	0.170 J	0.420 J	<0.100 U	<0.250 U	0.88	5.23
C-11 TR	0.51	Tributary	0.230 J	<0.250 U	0.160 J	0.280 J	<0.100 U	<0.250 U	0.79	3.78
C-9 TR GG	0.85	Tributary	0.250 J	<0.250 U	0.170 J	0.320 J	<0.100 U	<0.250 U	1.38	9.42
C-8.5 TR	0.89	Tributary	0.180 J	<0.250 U	0.220 J	0.380 J	<0.100 U	<0.250 U	0.65	7.44
C-7.5 TR	1.05	Tributary	0.120 J	<0.250 U	0.150 J	0.320 J	<0.100 U	<0.250 U	1.00	5.07
C-5 TR	1.25	Tributary	0.110 J	0.860 J	0.150 J	1.110 J	<0.100 U	0.400 J	0.49	62.48
MSD-B	1.58	Tributary	0.320 J	0.600 J	0.210 J	0.690 J	<0.100 U	<0.250 U	10.23	42.27

						MINOR	MINOR AND TRACE METALS	E METALS				
Site Name	Distance	Stream		Ga,TR	La	La, TR	Li	Li, TR	Mo	Mo, TR	dN	Nb, TR
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
			Dissolved	TR	Dissolved	TR	Dissolved	TR	Dissolved	TR	Dissolved	TR
C-12 TR	0.31	Tributary	<0.100 U	NR	<0.100 U	NR	1.460 J	NR	5.31	NR	<0.100 U	NR
C-8.5 TR	0.89	Tributary	<0.100 U	NR	<0.100 U	NR	3.96	NR	10.95	NR	<0.100 U	NR
C-8	1.00	Primary	<0.100 U	NR	<0.100 U	NR	3.24	NR	5.52	NR	<0.100 U	NR
C-7.5 TR	1.05	Tributary	<0.100 U	NR	<0.100 U	NR	7.11	NR	15.10	NR	<0.100 U	NR
C-6	1.20	Primary	<0.100 U	NR	<0.100 U	NR	8.14	NR	3.12	NR	<0.100 U	NR
C-7.5 POND	1.01	Pond	<0.100 U	0.680 J	<0.100 U	2.00	13.42	14.00	19.80	21.24	<0.100 U	0.320 J
0-1	0.00	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	3.06	6.11	4.82	4.79	<0.100 U	<0.250 U
C-12 US	0.24	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	3.38	5.59	5.62	5.45	<0.100 U	<0.250 U
C-12 DS	0.39	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	3.33	4.160 J	5.78	5.92	<0.100 U	<0.250 U
C-11 US	0.48	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	7.23	3.190 J	5.67	5.92	<0.100 U	<0.250 U
C-11 DS	0.59	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	6.70	3.730 J	5.88	6.14	<0.100 U	<0.250 U
C-9 US	0.83	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	6.85	3.580 J	5.92	6.31	<0.100 U	<0.250 U
C-9 DS	0.86	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	6.86	3.520 J	5.93	6.14	<0.100 U	<0.250 U
C-8	1.00	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	6.59	3.530 J	6.15	6.28	<0.100 U	<0.250 U
C-7	1.13	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	6.27	3.200 J	6.11	6.38	<0.100 U	<0.250 U
C-6	1.20	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	6.11	5.23	6.13	6.27	<0.100 U	<0.250 U
C-5	1.31	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	6.11	5.83	6.09	6.32	<0.100 U	<0.250 U
C-4.5	1.47	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	3.56	7.25	5.92	6.25	<0.100 U	<0.250 U
SS-04.5	1.56	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	3.20	5.95	5.88	6.38	<0.100 U	<0.250 U
SS-04.5	1.65	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	6.90	5.37	5.90	6.38	<0.100 U	<0.250 U
SS-05	1.82	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	6.49	5.11	5.81	6.22	<0.100 U	<0.250 U
SS-05A	2.66	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	7.59	7.00	6.00	6.29	<0.100 U	<0.250 U
SS-06A	3.00	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	7.77	5.89	5.89	6.30	<0.100 U	<0.250 U
C-12 TR	0.31	Tributary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	2.50	6.09	20.03	20.39	<0.100 U	<0.250 U
SAND CREEK	0.41	Tributary	<0.100 U	<0.250 U	<0.100 U	0.470 J	6.98	2.870 J	5.41	5.60	<0.100 U	<0.250 U
C-11 TR	0.51	Tributary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	7.30	6.77	9.89	10.62	<0.100 U	<0.250 U
C-9 TR GG	0.85	Tributary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	3.84	6.79	5.78	5.65	<0.100 U	<0.250 U
C-8.5 TR	0.89	Tributary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	8.82	8.45	11.27	11.76	<0.100 U	<0.250 U
C-7.5 TR	1.05	Tributary	<0.100 U	<0.250 U	<0.100 U	0.300 J	12.72	13.29	19.13	18.92	<0.100 U	<0.250 U
C-5 TR	1.25	Tributary	<0.100 U	0.560 J	<0.100 U	1.79	11.17	10.96	6.05	7.00	<0.100 U	0.300 J
MSD-B	1.58	Tributary	<0.100 U	0.330 J	<0.100 U	1.220 J	44.28	50.44	10.48	11.61	<0.100 U	<0.250 U

							MINO	R AND T	MINOR AND TRACE METALS	ETALS				
Site Name	Distance	Stream	Nd	Nd, TR	Ni	Ni, TR	Pb	Pb, TR	Pd	Pd, TR	Pr	Pr, TR	Rb	Rb, TR
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
			Dissolved	TR	Dissolved	TR	Dissolved	TR	Dissolved	TR	Dissolved	TR	Dissolved	TR
C-12 TR	0.31	Tributary	<0.100 U	NR	0.230 J	NR	<0.040 U	NR	<0.100 U	NR	<0.100 U	NR	<0.100 U	NR
C-8.5 TR	0.89	Tributary	<0.100 U	NR	0.63	NR	0.150 J	NR	<0.100 U	NR	<0.100 U	NR	0.62	NR
C-8	1.00	Primary	<0.100 U	NR	0.240 J	NR	0.23	NR	<0.100 U	NR	<0.100 U	NR	0.79	NR
C-7.5 TR	1.05	Tributary	<0.100 U	NR	0.260 J	NR	<0.040 U	NR	<0.100 U	NR	<0.100 U	NR	0.470 J	NR
C-6	1.20	Primary	<0.100 U	NR	0.240 J	NR	<0.040 U	NR	<0.100 U	NR	<0.100 U	NR	0.470 J	NR
C-7.5 POND	1.01	Pond	<0.100 U	1.47	0.62	2.38	0.49	15.85	<0.100 U	<0.250 U	<0.100 U	0.350 J	1.20	6.95
1-0	0.00	Primary	<0.100 U	<0.250 U	0.340 J	0.300 J	<0.040 U	0.310 J	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.450 J	0.660 J
C-12 US	0.24	Primary	<0.100 U	<0.250 U	0.360 J	0.300 J	<0.040 U	0.270 J	<0.100 U	<0.250 U	<0.100 U		0.450 J	0.600 J
C-12 DS	0.39	Primary	<0.100 U	<0.250 U	0.350 J	0.370 J	<0.040 U	0.290 J	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.450 J	0.620 J
C-11 US	0.48	Primary	<0.100 U	<0.250 U	0.370 J	0.420 J	<0.040 U	0.55	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.440 J	0.780 J
C-11 DS	0.59	Primary	<0.100 U	<0.250 U	0.360 J	0.390 J	<0.040 U	0.480 J	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.460 J	0.650 J
C-9 US	0.83	Primary	<0.100 U	<0.250 U	0.390 J	0.510 J	<0.040 U	0.81	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.450 J	0.870 J
C-9 DS	0.86	Primary	<0.100 U	<0.250 U	0.340 J	0.390 J	<0.040 U	0.57	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.460 J	0.700 J
C-8	1.00	Primary	<0.100 U	<0.250 U	0.380 J	0.470 J	<0.040 U	0.95	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.480 J	0.820 J
C-7	1.13	Primary	<0.100 U	<0.250 U	0.390 J	0.480 J	<0.040 U	1.05	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.470 J	0.890 J
C-6	1.20	Primary	<0.100 U	<0.250 U	0.410 J	0.410 J	0.050 J	0.69	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.490 J	0.670 J
C-5	1.31	Primary	<0.100 U	<0.250 U	0.380 J	0.410 J	<0.040 U	0.79	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.480 J	0.760 J
C-4.5	1.47	Primary	<0.100 U	<0.250 U	0.120 J	0.360 J	<0.040 U	0.53	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.420 J	0.610 J
SS-04.5	1.56	Primary	<0.100 U	<0.250 U	0.340 J	0.440 J	0.040 J	0.55	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.430 J	0.640 J
SS-04.5	1.65	Primary	<0.100 U	<0.250 U	0.330 J	0.410 J	<0.040 U	0.68	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.440 J	0.670 J
SS-05	1.82	Primary	<0.100 U	<0.250 U	0.350 J	0.500 J	0.060 J	0.83	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.450 J	0.680 J
SS-05A	2.66	Primary	<0.100 U	<0.250 U	0.370 J	0.480 J	0.040 J	2.07	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.470 J	0.830 J
SS-06A	3.00	Primary	<0.100 U	<0.250 U	0.370 J	0.490 J	0.050 J	1.43	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.480 J	0.740 J
C-12 TR	0.31	Tributary	<0.100 U	<0.250 U	0.51	0.540 J	<0.040 U	1.61	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.380 J	0.670 J
SAND CREEK	0.41	Tributary	<0.100 U	0.320 J	0.370 J	0.550 J	<0.040 U	1.83	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.360 J	1.32
C-11 TR	0.51	Tributary	<0.100 U	<0.250 U	0.55	0.610 J	<0.040 U	1.32	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.290 J	0.640 J
C-9 TR GG	0.85	Tributary	<0.100 U	<0.250 U	0.410 J	0.340 J	<0.040 U	1.52	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.52	0.630 J
C-8.5 TR	0.89	Tributary	<0.100 U	<0.250 U	0.75	1.090 J	0.160 J	2.24	<0.100 U	<0.250 U	<0.100 U	<0.250 U	0.57	1.130 J
C-7.5 TR	1.05	Tributary	<0.100 U	<0.250 U	0.68	L 000.0	0.38	2.93	<0.100 U	<0.250 U	<0.100 U	<0.250 U	1.19	1.83
C-5 TR	1.25	Tributary	<0.100 U	1.39	0.240 J	1.220 J	0.170 J	59.28	<0.100 U	<0.250 U	<0.100 U	0.330 J	0.63	4.90
MSD-B	1.58	Tributary	<0.100 U	0.950 J	1.38	2.00	0.180 J	8.36	<0.100 U	<0.250 U	<0.100 U	<0.250 U	2.56	5.29

							Σ	INOR AN	MINOR AND TRACE METALS	E METAL	S			
Site Name	Distance	Stream	Se	Se, TR	Sn	Sn, TR	Sr	Sr, TR	Тһ	Th, TR	Ti	Ti, TR	П	TI, TR
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
			Dissolved	TR	Dissolved	TR	Dissolved	TR	Dissolved	TR	Dissolved	TR	Dissolved	TR
C-12 TR	0.31	Tributary	1.75	NR	<0.100 U	NR	175.35	NR	<0.100 U	NR	<0.100 U	NR	<0.100 U	NR
C-8.5 TR	0.89	Tributary	5.44	NR	<0.100 U	NR	186.14	NR	<0.100 U	NR	<0.100 U	NR	<0.100 U	NR
C-8	1.00	Primary	18.97	NR	<0.100 U	NR	196.78	NR	<0.100 U	NR	<0.100 U	NR	<0.100 U	NR
C-7.5 TR	1.05	Tributary	1.45	NR	<0.100 U	NR	177.94	NR	<0.100 U	NR	<0.100 U	NR	<0.100 U	NR
C-6	1.20	Primary	<0.100 U	NR	<0.100 U	NR	276.91	NR	<0.100 U	NR	<0.100 U	NR	<0.100 U	NR
C-7.5 POND	1.01	Pond	0.400 J	0.680 J	<0.100 U	0.270 J	246.64	276.68	<0.100 U	6.95	<0.100 U	148.98	<0.100 U	<0.250 U
1-0	0.00	Primary	0.77	<0.250 U	<0.100 U	<0.250 U	209.02	216.09	<0.100 U	0.660 J	<0.100 U	4.93	<0.100 U	<0.250 U
C-12 US	0.24	Primary	13.62	<0.250 U	<0.100 U	<0.250 U	205.72	213.74	<0.100 U	0.600 J	<0.100 U	3.58	<0.100 U	<0.250 U
C-12 DS	0.39	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	207.70	220.80	<0.100 U	0.620 J	<0.100 U	3.77	<0.100 U	<0.250 U
C-11 US	0.48	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	207.34	216.53	<0.100 U	0.780 J	<0.100 U	8.21	<0.100 U	<0.250 U
C-11 DS	0.59	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	209.12	223.93	<0.100 U	0.650 J	<0.100 U	5.22	<0.100 U	<0.250 U
C-9 US	0.83	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	209.05	227.47	<0.100 U	0.870 J	<0.100 U	10.58	<0.100 U	<0.250 U
C-9 DS	0.86	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	210.99	223.29	<0.100 U	0.700 J	<0.100 U	6.75	<0.100 U	<0.250 U
C-8	1.00	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	211.09	221.39	<0.100 U	0.820 J	<0.100 U	9.94	<0.100 U	<0.250 U
C-7	1.13	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	209.37	224.63	<0.100 U	0.890 J	<0.100 U	11.67	<0.100 U	<0.250 U
C-6	1.20	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	210.63	223.09	<0.100 U	0.670 J	<0.100 U	5.35	<0.100 U	<0.250 U
C-5	1.31	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	209.58	223.21	<0.100 U	0.760 J	<0.100 U	7.90	<0.100 U	<0.250 U
C-4.5	1.47	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	212.91	218.50	<0.100 U	0.610 J	<0.100 U	3.60	<0.100 U	<0.250 U
SS-04.5	1.56	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	214.43	225.28	<0.100 U	0.640 J	<0.100 U	3.66	<0.100 U	<0.250 U
SS-04.5	1.65	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	214.32	225.87	<0.100 U	0.670 J	<0.100 U	4.34	<0.100 U	<0.250 U
SS-05	1.82	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	215.21	220.01	<0.100 U	0.680 J	<0.100 U	4.51	<0.100 U	<0.250 U
SS-05A	2.66	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	219.58	224.38	<0.100 U	0.830 J	<0.100 U	8.67	<0.100 U	<0.250 U
SS-06A	3.00	Primary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	221.46	230.21	<0.100 U	0.740 J	<0.100 U	5.04	<0.100 U	<0.250 U
C-12 TR	0.31	Tributary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	279.69	299.30	<0.100 U	0.670 J	<0.100 U	6.66	<0.100 U	<0.250 U
SAND CREEK	0.41	Tributary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	241.38	250.62	<0.100 U	1.32	<0.100 U	25.44	<0.100 U	<0.250 U
C-11 TR	0.51	Tributary	1.62	0.910 J	<0.100 U	<0.250 U	250.75	269.74	<0.100 U	0.640 J	<0.100 U	9.01	<0.100 U	<0.250 U
C-9 TR GG	0.85	Tributary	<0.100 U	<0.250 U	<0.100 U	<0.250 U	252.40	256.32	<0.100 U	0.630 J	<0.100 U	2.97	<0.100 U	<0.250 U
C-8.5 TR	0.89	Tributary	0.59	0.540 J	<0.100 U	<0.250 U	193.62	206.00	<0.100 U	1.130 J	<0.100 U	15.48	<0.100 U	<0.250 U
C-7.5 TR	1.05	Tributary	1.63	0.750 J	<0.100 U	<0.250 U	254.39	260.97	<0.100 U	1.83	<0.100 U	18.27	<0.100 U	<0.250 U
C-5 TR	1.25	Tributary	0.75	1.120 J	<0.100 U	0.850 J	233.19	267.64	<0.100 U	4.90	<0.100 U	119.39	<0.100 U	<0.250 U
MSD-B	1.58	Tributary	<0.100 U	1.150 J	<0.100 U	<0.250 U	368.88	382.50	<0.100 U	5.29	<0.100 U	53.78	<0.100 U	<0.250 U

				MINO	MINOR AND TRACE METALS	RACE ME	TALS	
Site Name	Distance	Stream	D	U, TR	M	W, TR	Zn	Zn, TR
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
			Dissolved	TR	Dissolved	TR	Dissolved	TR
C-12 TR	0.31	Tributary	3.22	NR	0.360 J	NR	8.67	NR
C-8.5 TR	0.89	Tributary	2.06	NR	1.66	NR	67.03	NR
C-8	1.00	Primary	0.190 J	NR	1.64	NR	1.74	NR
C-7.5 TR	1.05	Tributary	4.44	NR	<0.100 U	NR	19.04	NR
C-6	1.20	Primary	<0.100 U	NR	2.08	NR	0.410 J	NR
C-7.5 POND	1.01	Pond	4.02	4.51	0.57	1.160 J	2.85	142.46
I-0	0.00	Primary	3.80	3.90	0.150 J	<0.250 U	1.50	2.30
C-12 US	0.24	Primary	4.02	4.02	0.150 J	<0.250 U	1.16	2.49
C-12 DS	0.39	Primary	4.12	4.34	0.160 J	<0.250 U	1.08	2.31
C-11 US	0.48	Primary	4.14	4.28	0.190 J	<0.250 U	1.38	3.12
C-11 DS	0.59	Primary	4.17	4.32	0.210 J	<0.250 U	2.72	4.64
C-9 US	0.83	Primary	4.18	4.39	0.180 J	<0.250 U	2.12	6.01
C-9 DS	0.86	Primary	4.24	4.27	0.180 J	<0.250 U	2.48	4.78
C-8	1.00	Primary	4.20	4.22	0.200 J	<0.250 U	4.06	18.17
C-7	1.13	Primary	4.17	4.24	0.200 J	0.270 J	3.84	13.03
C-6	1.20	Primary	4.16	4.25	0.210 J	<0.250 U	4.16	8.23
C-5	1.31	Primary	4.13	4.19	0.290 J	0.290 J	4.01	10.17
C-4.5	1.47	Primary	4.24	4.13	0.270 J	0.290 J	3.43	7.60
SS-04.5	1.56	Primary	4.19	4.29	0.270 J	0.300 J	4.04	7.85
SS-04.5	1.65	Primary	4.17	4.19	0.360 J	0.310 J	4.46	8.80
SS-05	1.82	Primary	4.20	4.09	0.290 J	0.320 J	4.96	9.27
SS-05A	2.66	Primary	4.39	4.24	0.320 J	0.360 J	6.98	17.15
SS-06A	3.00	Primary	4.38	4.32	0.310 J	0.320 J	12.87	18.78
C-12 TR	0.31	Tributary	7.77	8.16	0.380 J	0.490 J	2.19	9.13
SAND CREEK	0.41	Tributary	6.70	6.89	0.340 J	0.410 J	18.12	31.83
C-11 TR	0.51	Tributary	3.87	4.16	0.370 J	0.390 J	47.96	58.21
C-9 TR GG	0.85	Tributary	4.24	4.17	0.260 J	0.320 J	11.27	16.21
C-8.5 TR	0.89	Tributary	2.28	2.46	0.58	0.630 J	65.70	160.48
C-7.5 TR	1.05	Tributary	3.81	3.74	0.410 J	0.430 J	2.29	22.21
C-5 TR	1.25	Tributary	3.91	4.91	2.32	3.12	0.66	115.04
MSD-B	1.58	Tributary	3.67	3.78	0.360 J	0.800 J	89.79	177.88

						NAV-GPS	NAV-GPS Coordinates			FLOW	
Site Name	Distance Stream		Type	Sample	GWIC	Lat	Long	DATE	Measui	Measured Flow	Calculated Flow
	(km)			D	D	Decima	Decimal Degrees		(cfs)	notes	(cfs)
BR TRACER SOLN 0.00	0.00	Tributary Surface	Surface	200831	999030			9/21/11 9:00 1.15E-04 Very Good	1.15E-04	Very Good	1.15E-04
C-11 TR @ Culvert 0.31	0.31	Tributary	Surface	200825	262795	45.9909222	-112.5231056 9/21/11 13:15	9/21/11 13:15			
DI BLANK	QAQC	QAQC	QAQC	200830	999030			9/21/11 8:40	na		
C-5 TR Duplicate 1.25	1.25	Tributary Surface	Surface	200840	262799			9/21/11 9:50 3.57E-01	3.57E-01		3.57E-01

					ш	HYSICAL	PHYSICAL PARAMETERS	ERS				MAJOR	MAJOR CATIOS	
Site Name	Distance	Stream	Hd	sc	TEMP		DO	Ηd	SC	Hardness	Са	Ca, TR	Mg	Mg, TR
	(km)			(NMHOS)	(C)	(mv)	(mg/L)		(SOHMU)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
BR TRACER SOLN 0.00	0.00	Tributary	NR	NR	NR	NR	NR	7.19	133,600		17.52	17.67	3.410 J	3.720 J
C-11 TR @ Culvert 0.31	0.31	Tributary	6.97	402.10	14.29	399.00	6.06	7.23	500.90	154.66	45.70	48.16	9.85	10.31
DI BLANK	QAQC	QAQC	5.50	10.00	10.00	NR	NR	5.86	9.10		<0.010 U	<0.010 U 0.010 J <0.020 U		<0.020 U
C-5 TR Duplicate 1.25	1.25	Tributary	NR	NR	NR	NR	NR	7.95	430.80	126.93	31.68	34.10	11.62	12.71

						MAJOR CATIONS	ATIONS				4	ANIONS	
Site Name Distance Stream	Distance	Stream	Na	Na, TR	Х	K, TR	Fe	Fe, TR	Mn	Mn, TR	HCO3	CO3	Br
	(km)		(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(ng/L)
BR TRACER SOLN 0.00	00.00	Tributary	81170.00 79966.67	79966.67	443.00	490.85	<5.000 U	<5.000 U	490.85 <5.000 U <5.000 U <1.000 U <5.000 U	<5.000 U	71.37		3.12E+08
C-11 TR @ Culvert 0.31	0.31	Tributary	19.02	18.98	4.28	4.58	0.11	0.50	0.03	0.03	147.60		110
DI BLANK	QAQC	QAQC	<0.020 U	0.100 J	<0.050 U	<0.050 U	<2.000 U	<5.000 U	<1.000 U	<2.500 U	7.34		<10.000 U
C-5 TR Duplicate 1.25	1.25	Tributary	23.68	24.73	5.01	6.58	0.13	4.75	0.08	0.32	149.18		124

			ANIA	ANIONS			NON-METALS		
Site Name	Distance Stream	Stream	C	S04	SiO2	NO3-N	PO4	Carbon	Carbon
	(km)		(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
BR TRACER SOLN 0.00		Tributary	26,019	359,087	9.98	<1000 U	<2000 U	1.52	1.52
C-11 TR @ Culvert 0.31		Tributary	24.17	31.84	25.33	4.15	0.19	2.82	2.82
DI BLANK	QAQC	QAQC	<0.100 U	<0.500 U	<0.020 U	<0.010 U	<0.020 U	0.36	0.36
C-5 TR Duplicate	1.25	Tributary	17.42	34.79	4.53	<0.010 U	<0.020 U	5.40	5.15

						MINOR	MINOR AND TRACEMETALS	EMETALS			
Site Name	Distance	Stream	Ag	Ag, TR	AI	AI, TR	As	As, TR	В	B, TR	Ba
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
BR TRACER SOLN 0.00	0.00	Tributary	<5000 U	<5000 U	<5000 U	<5000 U	<5000 U	<5000 U	<5000 U	NR	<5000 U
C-11 TR @ Culvert 0.31		Tributary	<0.100 U	<0.250 U	20.96	207.60	5.81	9.24	51.89	NR	42.29
DI BLANK	QAQC	QAQC	<0.100 U	<0.250 U	1.320 J	6.84	0.470 J	<0.250 U	<0.500 U	NR	<0.100 U
C-5 TR Duplicate	1.25	Tributary	<0.100 U	<0.250 U	1.110 J	1550.52	8.86	17.76	32.06	NR	42.47

					MIN	MINOR AND TRACE METALS	ACE META	LS		
Site Name Dist	Distance	Stream	Ba, TR	Be	Be, TR	Br	Cd	Cd, TR	Ce	Ce, TR
(km)	(۲		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
BR TRACER SOLN 0.00		Tributary	<5000 U	<5000 U	<5000 U	3.12E+08	<5000 U	<5000 U	<5000 U	<5000 U
C-11 TR @ Culvert 0.31		Tributary	48.60	<0.100 U	<0.250 U	1.10E+02	<0.100 U	<0.250 U	<0.100 U	0.400 J
DI BLANK	QAQC	QAQC	<0.250 U	<0.100 U	<0.250 U	<10.000 U	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-5 TR Duplicate 1.25		Tributary	45.46	<0.100 U	<0.250 U	1.24E+02	<0.100 U	0.330 J	<0.100 U	1.97

					MINO	<i>AINOR AND TRACE METALS</i>	METALS			
Site Name	Distance Stream	Stream	Co	Co, TR	Cr	Cr, TR	Cs	Cs, TR	Cu	Cu, TR
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
BR TRACER SOLN 0.00	0.00	Tributary	<5000 U	<5000 U	<5000 U	<5000 U	<5000 U	<5000 U	<5000 U	<5000 U
C-11 TR @ Culvert 0.31	0.31	Tributary	0.130 J	<0.250 U	0.160 J	0.390 J	<0.100 U	<0.250 U	3.48	10.86
DI BLANK	QAQC	QAQC	<0.100 U	<0.250 U	0.150 J	<0.250 U	<0.100 U	<0.250 U	<0.100 U	<0.250 U
C-5 TR Duplicate 1.25	1.25	Tributary	<0.100 U	0.940 J	0.160 J	1.130 J	<0.100 U	0.610 J	0.44	60.03

						MINOR	MINOR AND TRACE METALS	E METALS				
Site Name	Distance Stream	Stream		Ga,TR	La	La, TR	Li	Li, TR	Mo	Mo, TR	dN	Nb, TR
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
BR TRACER SOLN 0.00	0.00	Tributary	<5000 U	<5000 U	<1000 U	<5000 U	<5000 U	<5000 U				
C-11 TR @ Culvert 0.31	0.31	Tributary	<0.100 U	<0.250 U	<0.100 U	0.400 J	4.49	8.64	5.36	5.49	<0.100 U <0.250 U	<0.250 U
DI BLANK	QAQC	QAQC	<0.100 U	<0.250 U	<0.100 U	<0.250 U	<0.400 U	2.050 J	<0.100 U <0.250 U	<0.250 U	<0.100 U <0.250 U	<0.250 U
C-5 TR Duplicate 1.25	1.25	Tributary	<0.100 U	0.610 J	<0.100 U	86.14	9.69	11.97	5.85	0.320 J	<0.100 U	0.370 J

							MINC	R AND T	WINOR AND TRACE METALS	ETALS				
Site Name	Distance	Stream	Nd	Nd, TR	Ni	Ni, TR	Pb	Pb, TR	Pd	Pd, TR	Pr	Pr, TR	Rb	Rb, TR
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
BR TRACER SOLN 0.00	0.00	Tributary	<5000 U <5000)	<5000 U	<5000 U	<5000 U <5000 U <5000 U <5000 U <5000 U <5000 U	<5000 U	<5000 U	<5000 U	<5000 U	<5000 U	<5000 U	<5000 U
C-11 TR @ Culvert 0.31	0.31	Tributary	<0.100 U 0.280	0.280 J	0.500 J	0.640 J	0.640 J <0.040 U	2.47	<0.100 U	<0.250 U	<0.100 U <0.250 U <0.100 U <0.250 U 0.350 J	<0.250 U	0.350 J	0.950 J
DI BLANK	QAQC	QAQC	<0.100 U <0.250	Γ	<0.100 U	<0.250 U	<0.040 U	<0.100 U	<0.100 U	<0.250 U	<0.100 U <0.250 U <0.040 U <0.100 U <0.100 U <0.250 U <0.100 U <0.250 U <0.250 U	<0.250 U	<0.100 U	<0.250 U
C-5 TR Duplicate 1.25	1.25	Tributary	<0.100 U 1.49	1.49	0.200 J	0.200 J 1.240 J	0.140 J	60.42	<0.100 U <0.250 U	<0.250 U	<0.100 U	0.368 J	0.57	0.920 J
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							N	1INOR AN	MINOR AND TRACE METALS	E METALS	S			
Site Name	Distance Stream	Stream	Se	Se, TR	Sn	Sn, TR	Sr	Sr, TR	Th	Th, TR	Ті	TI, TR	ΤI	TI, TR
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
BR TRACER SOLN 0.00	0.00	Tributary	<5000 U	<5000 U	<5000 U <5000 U <5000 U	<5000 U	<5000 U	<5000 U	<5000 U <5000 U <5000 U <5000 U <5000 U <5000 U	<5000 U	<5000 U	<5000 U	<5000 U	<5000 U
C-11 TR @ Culvert 0.31	0.31	Tributary	0.80	<0.250 U	<0.250 U <0.100 U <0.250 U 256.89	<0.250 U	256.89		267.99 <0.100 U 0.950 J <0.100 U 75.27 <0.100 U <0.250 U	0.950 J	<0.100 U	15.27	<0.100 U	<0.250 U
DI BLANK	QAQC	QAQC	1.30 <0	<0.250 U	<0.100 U	<0.250 U	<0.100 U	<0.250 U	.250 U <0.100 U <0.250 U <0.100 U <0.100 U <0.250 U <0.100 U <0.250 U <0.250 U	<0.250 U	<0.100 U	1.70	<0.100 U	<0.250 U
C-5 TR Duplicate 1.25	1.25	Tributary	<0.100 U	<0.250 U	<0.100 U <0.250 U <0.100 U	3.96	239.02		272.36 <0.100 U 0.920 J <0.100 U 26.95 <0.100 U <0.250 U	0.920 J	<0.100 U	126.95	<0.100 U	<0.250 U

				MINO	WINOR AND TRACE METALS	RACE ME	TALS	
Site Name	Distance	Stream	n	U, TR	M	W, TR	Zn	Zn, TR
	(km)		(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)	(ng/L)
BR TRACER SOLN 0.00	0.00	Tributary	<5000 U	<5000 U	<5000 U	<5000 U	<2000 U <5000 U <5000 U <5000 U <5000 U <5000 U	<5000 U
C-11 TR @ Culvert 0.31	0.31	Tributary	3.53	3.73	3.73 <0.100 U <0.250 U	<0.250 U	40.24	54.23
DI BLANK	QAQC	QAQC	<0.100 U	<0.250 U	<0.100 U	<0.250 U	<0.100 U <0.250 U <0.100 U <0.250 U <0.200 U <0.500 U	<0.500 U
C-5 TR Duplicate 1.25	1.25	Tributary	3.86	4.81	2.21	3.22	0:50	124.70

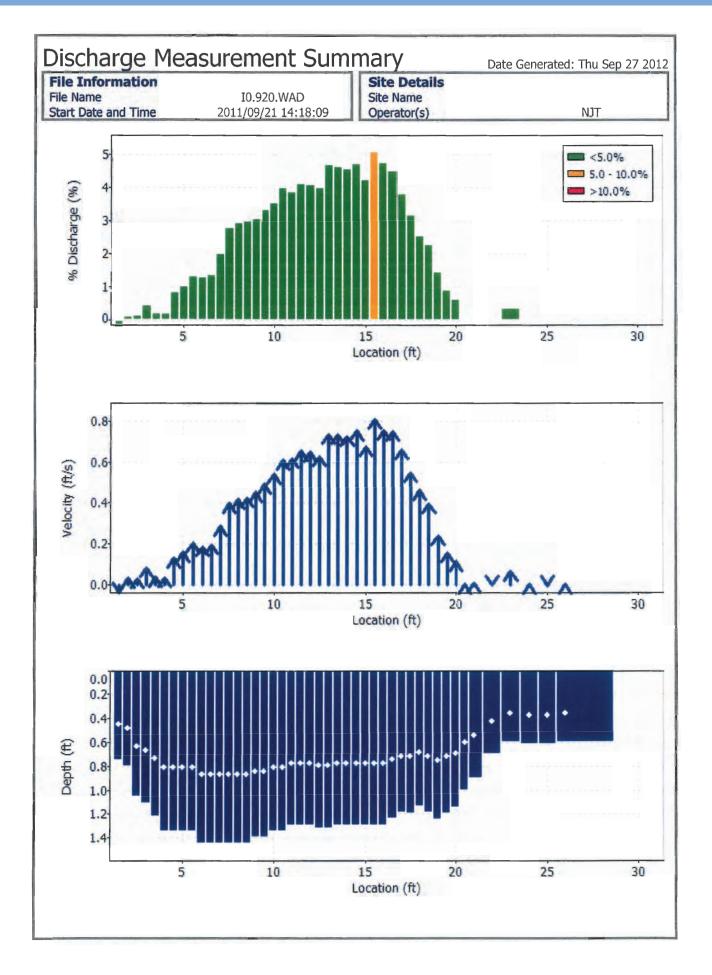
APPENDIX D

DISCHARGE MEASUREMENT SUMMARY

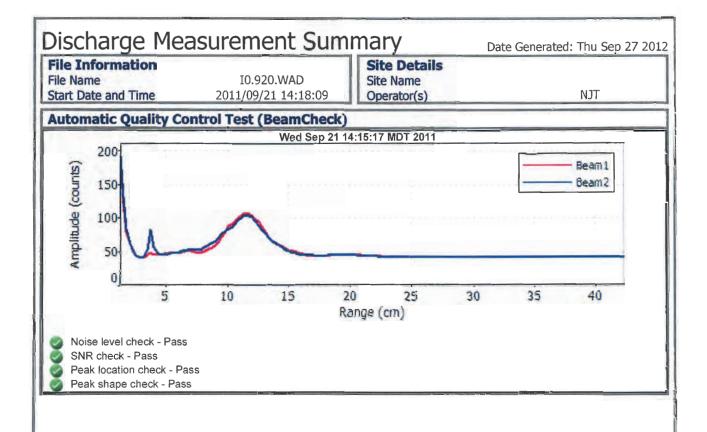
File Information File Name Start Date and Time		0.920.W /09/21 1⁄		Site Details Site Name Operator(s)		TCN	
System Informatio	on		Units	(English Units)	Discharge Un	certainty	
Sensor Type		racker	Distance	ft	Category	ISO	Stats
Serial #		012	Velocity	ft/s	Accuracy	1.0%	1.0%
CPU Firmware Version		.7	Area	ft^2	Depth	0.1%	0.4%
Software Ver	2.	30	Discharge	cfs	Velocity	0.6%	1.4%
Mounting Correction	0.	0%			Width	0.1%	0.1%
	an man and a Mark				Method	1.4%	-
Summary	20	4 Chati		47	# Stations	1.1%	
Averaging Int. Start Edge	30 REW	# Stati Total V		47 30.400	Overall	2.2%	1.8%
Mean SNR	29.3 dB	Total A		29.850			
Mean Temp	51.82 °F	Mean I		0.982			
Disch. Equation	Mid-Section		/elocity	0.3475			
			Discharge	10.3721			

File	e Infor	-	Meas			1	Site De		Date Gene	-		
	Name				920.WAD	- 11	Site Nam	e				
Sta	rt Date a	nd Time	9	2011/09	/21 14:1	8:09	Operator	(s)		-	TLV	
Me	asuren	nent R	esults									
St	Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrFact	MeanV	Area	Flow	%Q
0	14:18	1.00	None	0.000	0.0	0.0	0.0000	1.00	0.0000	0.000	0.0000	0.
1	14:18	1.50	0.6	0.750	0.6	0.300	-0.0400	1.00	-0.0400	0.375	-0.0150	-0.
2	14:19	2.00	0.6	0.800	0.6	0.320	0.0305	1.00	0.0305	0.400	0.0122	0.
3	14:20	2.50	0.6	1.050	0.6	0.420	0.0292	1.00	0.0292	0.525	0.0153	0.
4	14:21	3.00	0.6	1.110	0.6	the later of the l	0.0837	1.00	0.0837	0.555	0.0464	0.
5	14:22	3.50	0.6	1.220	0.6	0.488	0.0348	1.00	0.0348	0.610	0.0212	0.
6	14:24	4.00	0.6	1.350	0.6		0.0341	1.00	0.0341	0.675	0.0230	
7	14:25	4.50	0.6	1.350	0.6		0.1302	1.00	0.1302	0.675	0.0879	
8	14:26	5.00	0.6	1.350	0.6		0.1588	1.00	0.1588	0.675	0.1072	the state of the s
9	14:27	5.50	0.6	1.350	0.6		0.2044	1.00	0.2044	0.675	0.1380	
10	14:28	6.00	0.6	1.450	0.6		0.1870	1.00	0.1870	0.725	0.1356	
11	14:29	6.50	0.6	1.450	0.6	the second se	0.1959	1.00	0.1959	0.725	0.1330	
12	14:30	7.00	0.6	1.450	0.6	the second day of the	0.1955	1.00	0.1959	0.725	0.2079	
13	14:31	7.50	0.6	1.450	the second se	and some of the local division in which the local division in which the local division in which the local division is not the local division in the local	0.4006	And in case of the local division in which the local division in which the local division is not the local division in the local div	the second se	0.725	0.2905	
_			section of the local division of the local d		0.6			1.00	0.4006			
14	14:32	8.00	0.6	1.450	0.6	0.580	0.4199	1.00	0.4199	0.725	0.3045	
15	14:33	8.50	0.6	1.450	0.6		0.4285	1.00	0.4285	0.725	0.3107	3.
16	14:34	9.00	0.6	1.400	0.6		0.4551	1.00	0.4551	0.700	0.3185	
17	14:35	9.50	0.6	1.400	0.6		0.4938	1.00	0.4938	0.700	0.3456	
18	14:36	10.00	0.6	1.350	0.6		0.5443	1.00	0.5443	0.675	0.3674	
19	14:37	10.50	0.6	1.350	0.6		0.6129	1.00	0.6129	0.675	0.4137	4.
20	14:38	11.00	0.6	1.300	0.6		0.6198	1.00	0.6198	0.650	0.4028	
21	14:39	11.50	0.6	1.300	0.6	0.520	0.6552	1.00	0.6552	0.650	0.4258	
22	14:40	12.00	0.6	1.300	0.6		0.6516	1.00	0.6516	0.650	0.4235	
23	14:41	12.50	0.6	1.320	0.6		0.6289	1.00	0.6289	0.660	0.4151	4.
24	14:42	13.00	0.6	1.320	0.6		0.7365	1.00	0.7365	0.660	0.4861	4.
25	14:43	13.50	0.6	1.300	0.6		0.7385	1.00	0.7385	0.650	0.4800	4.
26	14:44	14.00	0.6	1.300	0.6		0.7277	1.00	0.7277	0.650	0.4730	and the second division of the second divisio
27	14:44	14.50	0.6	1.300	0.6		0.7536	1.00	0.7536	0.650	0.4898	
28	14:46	15.00	0.6	1.300	0.6		0.6781	1.00	0.6781	0.650	0.4408	
29	14:47	15.50	0.6	1.300	0.6	0.520	0.8104	1.00	0.8104	0.650	0.5267	5.
30	14:48	16.00	0.6	1.300	0.6	0.520	0.7566	1.00	0.7566	0.650	0.4917	4.
31	14:50	16.50	0.6	1.240	0.6		0.7523	1.00	0.7523	0.620	0.4665	4.
32	14:51	17.00	0.6	1.190	0.6	0.476	0.6634	1.00	0.6634	0.595	0.3947	
33	14:52	17.50	0.6	1.200	0.6	0.480	0.5495	1.00	0.5495	0.600	0.3298	3.
34	14:54	18.00	0.6	1.140	0.6	0.456	0.4639	1.00	0.4639	0.570	0.2645	2.
35	14:55	18.50	0.6	1.190	0.6	0.476	0.3990	1.00	0.3990	0.595	0.2374	2
36	14:56	19.00	0.6	1.250	0.6		0.2408	1.00	0.2408	0.625	0.1505	_
37	14:57	19.50	0.6	1.200	0.6	0.480	0.1558	1.00	0.1558	0.600	0.0935	
38	14:59	20.00	0.6	1.150	0.6	0.460	0.1138	1.00	0.1138	0.575	0.0655	
39	15:00	20.50	0.6	1.000	0.6	0.400	0.0013	1.00	0.0013	0.500	0.0007	
40	15:01	21.00	0.6	0.900	0.6	0.360	0.0089	1.00	0.0089	0.675	0.0060	_
41	15:02	22.00	0.6	0.700	0.6	0.280	-0.0023	1.00	-0.0023	0.700	-0.0016	
42	15:04	23.00	0.6	0.600	0.6	0.240	0.0646	1.00	0.0646	0.600	0.0388	
43	15:05	24.00	0.6	0.620	0.6		0.0010	1.00	0.0010	0.620	0.0006	
44	15:07	25.00	0.6	0.620	0.6		-0.0049	1.00	-0.0049	0.620	-0.0031	
_	the second division in which the second division is not the second division of the second d	26.00	0.6		0.6		0.0003		0.0003		0.0006	_
45	15:08 15:08	31.40	None	0.600	0.0		0.0000	1.00	0.0003	1.920 0.000	0.0000	

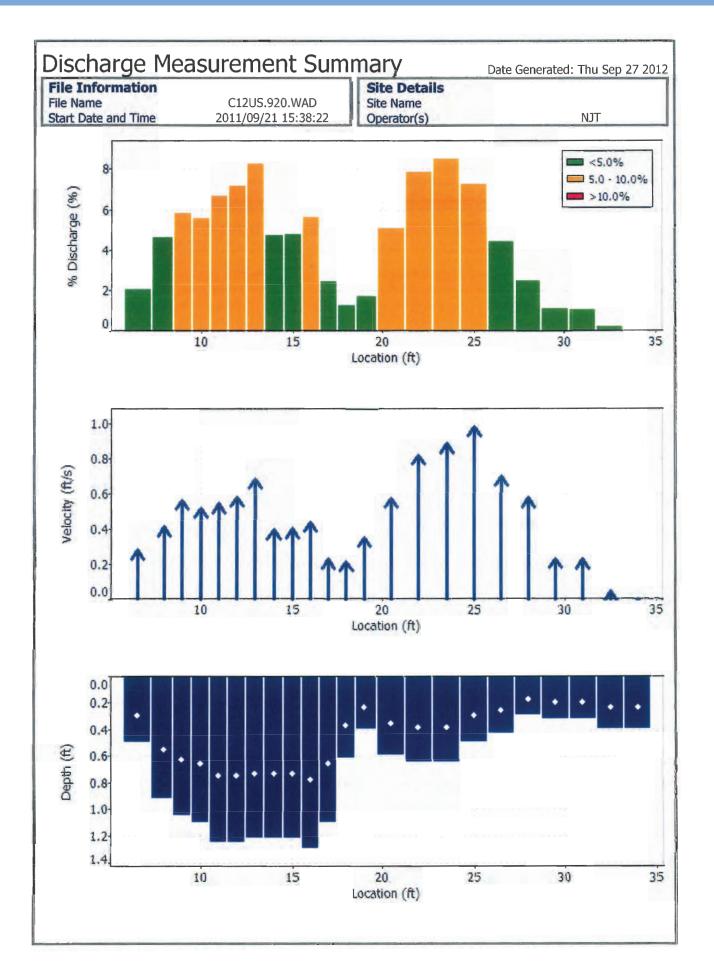
Rows in italics indicate a QC warning. See the Quality Control page of this report for more information.



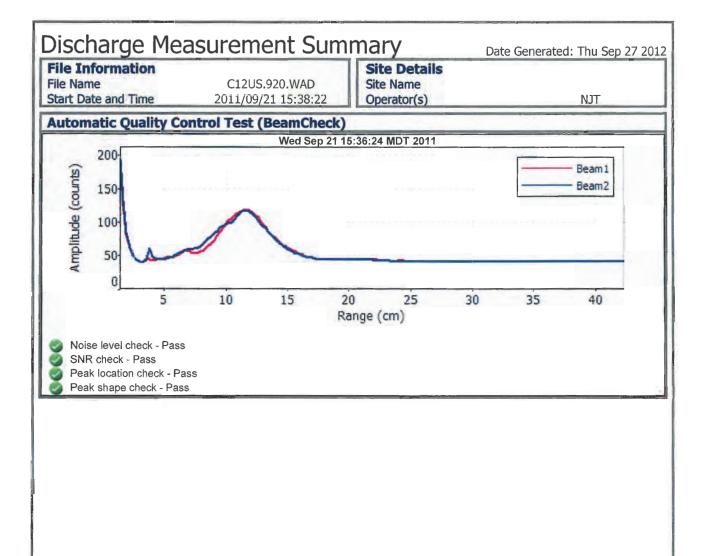
			asurement Sum	The second se	Date Generated: Thu Sep 27 2012
File N	Inform: Name		10.920.WAD	Site Details Site Name	
Start	Date and	Time	2011/09/21 14:18:09	Operator(s)	TEN
Qua	lity Con	trol			
St	Loc	%Dep		Message	
1	1.50	0.6	High angle: 167 SNR (44.1) is different from typic	al SNR (29.3)	
2	2.00		High SNR variation during measu		
3	2.50		High angle: 41 High SNR variation during measu	rement: 6.5,6.0	
5	3.50		High angle: 33		
37	19.50	0.6 0.6	High SNR variation during measu Boundary QC is Good; possible bo	rement: 9.0,10.3 oundary interference	
38	20.00		High SNR variation during measu		
39	20.50	0.6	SNR (47.5) is different from typic	al SNR (29.3)	
40	21.00		SNR (40.6) is different from typic High SNR variation during measu		
41	22.00		SNR (56.5) is different from typic High SNR variation during measu		
42	23.00	0.6	High angle: 42 High SNR variation during measu		
43	24.00		Boundary QC is Fair; possible bou		
44	25.00	0.6	SNR (61.3) is different from typic High SNR variation during measured	al SNR (29.3)	
45	26.00	0.6 0.6	Low SNR: 1.7,48.1 High differences in beam SNR: 1. Boundary QC is Fair; possible bou	7,48.1	



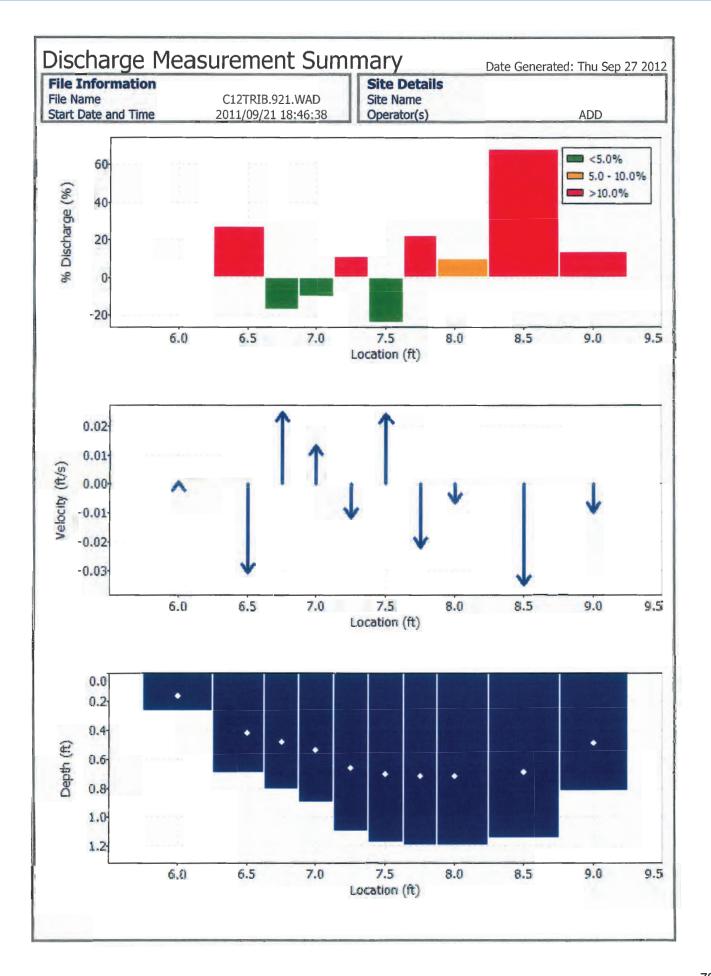
File Inform File Name Start Date and		-		.920.WAD 2 <u>1 15:38</u> :		Site Det Site Name Operator(2			Ν	ΤÜ	
System Inf	ormat	ion		U	nits	(English U	nits)	Dis	charge l	Uncerta	ainty	
Sensor Type		1	-lowTrack	ker Di	stance	ft			Category	I	SO	Stats
Serial #			P3012	Ve	locity	ft/s		Accu	Iracy		1.0%	1.09
CPU Firmware	Version	1	3.7	Ar	ea	ft^2		Dep	th		0.3%	2.39
Software Ver			2.30	Di	scharge	cfs		Velo	city		0.9%	3.79
Mounting Corr	rection		0.0%					Widt	th		0.1%	0.19
Summer Surger						And and a second second	-	Met			1.8%	
Summary		20		Chations		25		and the same of	ations		2.0%	
Averaging Int.		30 DEW		Stations		25		Ove		1	3.1%	4.49
Start Edge Mean SNR		REW		tal Width		30.400		In the second second				
Mean Temp		31.3 c 52.20		tal Area		20.595						
Disch. Equation	n	52.20 Mid-Sec		ean Depthean Veloci		0.677 0.4916						
Disch, Equatio		mu-sec		tal Discl		10.123						
0 15:38	5.00	None	Depth 0.000	%Dep 0.0	MeasD 0.0	Vel 0.0000	CorrF		MeanV 0.0000	Area 0.000	Flow 0.00	%
	5.00	None	0.000	0.0	0.0							
	6 50	statement of the local division in which the local division in which the local division is not the local division of the local division in the local division in the local division is not the local division of the local division in the local division is not the local division of the local division in the local division is not the local division of the local division is not the local division of the local dintedivisi						1.00				
NAME OF TAXABLE PARTY AND ADDRESS OF TAXABLE PARTY.	6.50	0.6	0.500	0.6	0.200	0.2822		1.00	0.2822	0.750	0.21	16 2.
2 15:39	8.00	0.6	0.500	0.6	0.200	0.2822		1.00 1.00	0.2822	0.750	0.21	16 2 61 4
2 15:39 3 15:41	8.00 9.00	0.6 0.6 0.6	0.500 0.920 1.050	0.6 0.6 0.6	0.200 0.368 0.420	0.2822 0.4140 0.5663		1.00	0.2822	0.750 1.150 1.050	0.21	16 2 61 4 45 5
2 15:39 3 15:41 4 15:42	8.00 9.00 10.00	0.6	0.500 0.920 1.050 1.100	0.6	0.200 0.368 0.420 0.440	0.2822 0.4140 0.5663 0.5203		1.00 1.00 1.00	0.2822 0.4140 0.5663	0.750	0.21 0.470 0.594	16 2. 61 4. 45 5. 24 5.
2 15:39 3 15:41 4 15:42	8.00 9.00	0.6 0.6 0.6 0.6	0.500 0.920 1.050	0.6 0.6 0.6 0.6	0.200 0.368 0.420	0.2822 0.4140 0.5663 0.5203 0.5463		1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203	0.750 1.150 1.050 1.100	0.21 0.47 0.59 0.57	16 2. 61 4. 45 5. 24 5. 28 6. 00 7.
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45	8.00 9.00 10.00 11.00 12.00 13.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.100 1.250 1.250 1.220	0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.440 0.500 0.500 0.488	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877		1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877	0.750 1.150 1.050 1.100 1.250 1.250 1.220	0.21 0.47 0.59 0.57 0.68 0.73 0.83	16 2. 61 4. 45 5. 24 5. 28 6. 00 7. 90 8.
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46	8.00 9.00 10.00 11.00 12.00 13.00 14.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.100 1.250 1.250 1.220 1.220	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.440 0.500 0.500 0.488 0.488	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957	0.750 1.150 1.050 1.100 1.250 1.250 1.220 1.220	0.21 0.47 0.59 0.57 0.68 0.73 0.83 0.83	16 2 61 4 45 5 24 5 28 6 00 7 90 8 28 4
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46 9 15:47	8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.250 1.250 1.220 1.220 1.220	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.440 0.500 0.500 0.488 0.488 0.488	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016	0.750 1.150 1.050 1.250 1.250 1.220 1.220 1.220	0.21 0.470 0.59 0.57 0.68 0.730 0.83 0.83 0.48 0.49	16 2 61 4 45 5 24 5 28 6 00 7 90 8 28 4 00 4
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46 9 15:47 10 15:48	8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.300	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.500 0.500 0.488 0.488 0.488 0.488 0.520	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409	0.750 1.150 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.300	0.21 0.47 0.59 0.57 0.68 0.73 0.83 0.48 0.48 0.49 0.57	16 2 61 4 45 5 24 5 28 6 00 7 90 8 28 4 00 4 32 5
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46 9 15:47 10 15:48 11 15:49	8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 <i>17.00</i>	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.220 1.300 <i>1.100</i>	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.500 0.500 0.488 0.488 0.488 0.488 0.488 0.520 0.440	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293	0.750 1.150 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.300 1.100	0.21 0.47 0.59 0.57 0.68 0.73 0.83 0.48 0.49 0.57 0.252	16 2 61 4 45 5 24 5 28 6 00 7 90 8 28 4 00 4 32 5 23 2
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46 9 15:47 10 15:48 11 15:49 12 15:50	8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 <i>17.00</i> <i>18.00</i>	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> 0.620	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.500 0.500 0.488 0.488 0.488 0.488 0.520 0.440 0.248	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175	0.750 1.150 1.050 1.250 1.250 1.220 1.220 1.220 1.300 1.100 0.620	0.21 0.47 0.59 0.57 0.68 0.73 0.83 0.48 0.49 0.57 0.25 2 0.13	16 2 61 4 45 5 24 5 28 6 00 7 90 8 28 4 00 4 32 5 23 2 49 1
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46 9 15:47 10 15:48 11 15:49 12 15:50 13 15:52	8.00 9.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.250 1.220 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> 0.620 0.400	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.500 0.500 0.488 0.488 0.488 0.488 0.520 0.440 0.248 0.160	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553	0.750 1.150 1.050 1.250 1.250 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.500	0.21 0.47 0.59 0.57 0.68 0.73 0.83 0.48 0.49 0.57 0.25 2 0.13 0.17	16 2 51 4 45 5 24 5 28 6 00 7 90 8 28 4 00 4 32 5 23 2 19 1 76 1
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46 9 15:47 10 15:48 11 15:49 12 15:50 13 15:52 14 15:53	8.00 9.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 20.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.400 0.600	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.500 0.500 0.488 0.488 0.488 0.488 0.520 0.440 0.248 0.160 0.240	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761	0.750 1.150 1.050 1.250 1.250 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.500 0.900	0.21 0.47(0.59) 0.57 0.68 0.73(0.83) 0.48 0.49(0.57) 0.252 0.134 0.17 0.51(16 2 51 4 45 5 24 5 28 6 00 7 90 8 28 4 00 4 32 5 23 2 19 1 76 1 86 5
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46 9 15:47 10 15:48 11 15:49 12 15:50 13 15:52 14 15:53 15 15:54	8.00 9.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 20.50 22.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.400 0.600 0.650	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.500 0.500 0.488 0.488 0.488 0.488 0.520 0.440 0.248 0.160 0.240 0.260	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238	0.750 1.150 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.500 0.900 0.975	0.21 0.47(0.59) 0.57 0.68 0.73(0.83) 0.48 0.49(0.57) 0.252 0.134 0.17 0.51(0.80)	16 2 51 4 45 5 24 5 28 6 00 7 90 8 228 4 00 4 32 5 23 2 79 1. 76 1 86 5 31 7
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46 9 15:47 10 15:48 11 15:49 12 15:50 13 15:52 14 15:53 15 15:54 16 15:55	8.00 9.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 20.50 22.00 23.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.400 0.650 0.650	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.500 0.500 0.488 0.488 0.488 0.488 0.520 0.440 0.240 0.240 0.240 0.260	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901	0.750 1.150 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.500 0.900 0.975 0.975	0.21 0.47(0.59) 0.57 0.68 0.73 0.83 0.48 0.49 0.57 0.25 2 0.13 0.13 0.17 0.51 0.80 0.80 0.86	16 2 51 4 45 5 24 5 28 6 00 7 90 8 28 4 00 4 32 5 23 2 49 1 76 1 86 5 31 7 78 8
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46 9 15:47 10 15:48 11 15:49 12 15:50 13 15:52 14 15:53 15 15:54 16 15:55 17 15:56	8.00 9.00 11.00 12.00 13.00 14.00 15.00 15.00 16.00 17.00 18.00 19.00 20.50 22.00 23.50 25.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.400 0.650 0.650 0.650	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.500 0.500 0.488 0.488 0.488 0.488 0.488 0.520 0.440 0.240 0.240 0.260 0.260 0.200	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8201 0.9902	0.750 1.150 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.220 1.220 0.500 0.500 0.900 0.975 0.975 0.750	0.21 0.474 0.599 0.577 0.683 0.730 0.833 0.483 0.499 0.577 0.252 0.134 0.177 0.511 0.800 0.866 0.748	16 2 61 4 45 5 24 5 28 6 00 7 90 8 228 4 00 4 32 5 23 2 49 1 76 1 86 5 31 7 78 8 26 7
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46 9 15:47 10 15:48 11 15:49 12 15:50 13 15:52 14 15:53 15 15:54 16 15:55 17 15:56 18 15:57	8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 20.50 22.00 23.50 25.00 26.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.400 0.650 0.650 0.650 0.500 <i>0.430</i>	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.500 0.500 0.488 0.488 0.488 0.488 0.488 0.520 0.440 0.240 0.240 0.240 0.260 0.260 0.200 0.172	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047	0.750 1.150 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.500 0.900 0.975 0.975	0.21 0.47(0.59) 0.57 0.68 0.73 0.83 0.48 0.49 0.57 0.25 2 0.13 0.13 0.17 0.51 0.80 0.80 0.86	16 2 51 4 45 5 24 5 28 6 00 7 90 8 28 4 00 4 32 5 23 2 49 1 76 1 86 5 31 7 78 8 26 7 47 4
2 15:39 3 15:41 4 15:42 5 15:43 6 15:44 7 15:45 8 15:46 9 15:47 10 15:48 11 15:49 12 15:50 13 15:52 14 15:53 15 15:54 16 15:55 17 15:56 18 15:57 19 15:58	8.00 9.00 11.00 12.00 13.00 14.00 15.00 15.00 16.00 17.00 18.00 19.00 20.50 22.00 23.50 25.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.500 0.920 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.400 0.650 0.650 0.650 0.500 <i>0.430</i> 0.300	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.200 0.368 0.420 0.500 0.500 0.488 0.488 0.488 0.488 0.488 0.488 0.488 0.520 0.440 0.240 0.240 0.240 0.260 0.260 0.200 0.2172 0.120	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047 0.5791		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.2822 0.4140 0.5663 0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8201 0.9902	0.750 1.150 1.050 1.250 1.250 1.220 1.220 1.220 1.220 1.220 1.220 0.500 0.620 0.900 0.975 0.975 0.750 0.645	0.21 0.47(0.59) 0.57 0.683 0.483 0.483 0.483 0.490 0.57 0.252 0.134 0.17 0.515 0.800 0.860 0.745	16 2 61 4 45 5 24 5 28 6 00 7 90 8 228 4 00 4 32 5 23 2.2 49 1. 76 1 86 5 31 7 78 8 26 7 47 4. 005 2
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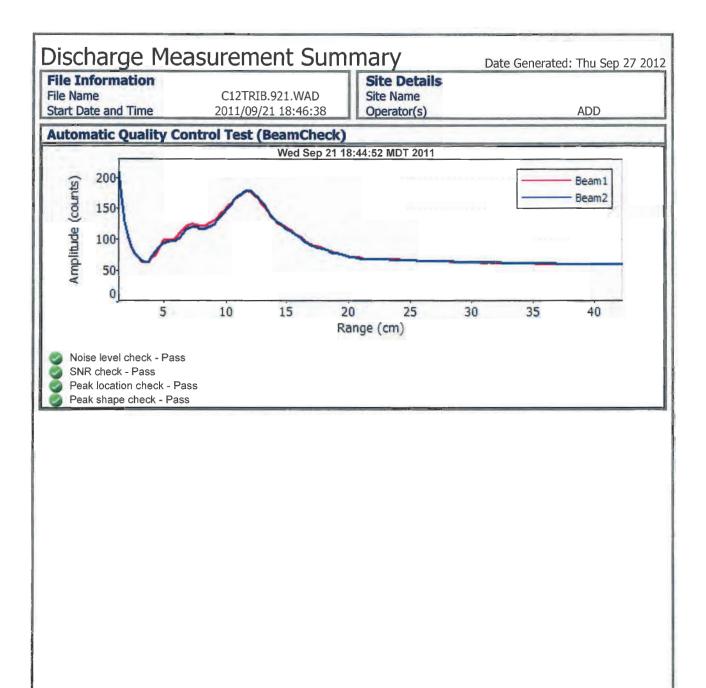
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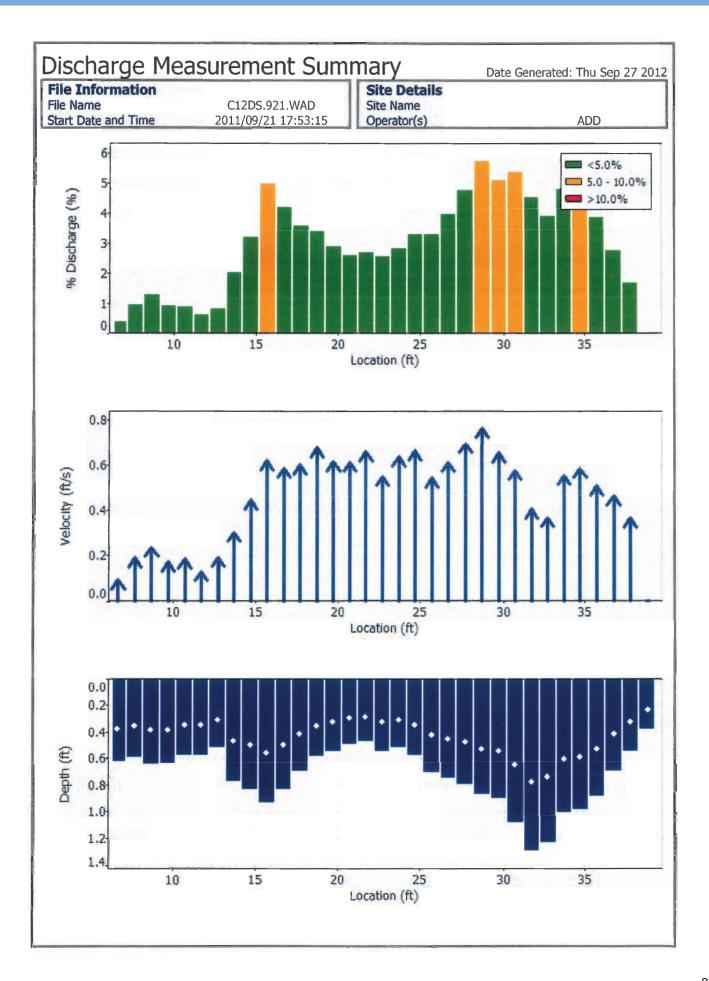
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Sof	ware Ve	er		2.3		Discharge		fs	Velocity		316.7%	93.39
Mou	inting C	orrection		0.0					Width		0.4%	0.49
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	mmary								# Station	ne l	4.2%	
	raging I t Edge	int.		30 EW	# Station Total Wi		12 4.00		Overall	and the second sec	316.8%	93.4%
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Mea Disc Mea	an Temp ch. Equa asurei Clock 18:46	ment Ro Loc M 5.50	57. Mid-s esuits lethod None	Section Depth 0.000	Mean Ve Total D %Dep 0.0	MeasD 0.0	0.73 -0.00 -0.02 Vel 0.0000	83 095 297 CorrFact	00 0.00	00 0.000	0.0000	0.
Mea Disc Mea	an Temp ch. Equa asurei Clock 18:46 18:46	ment Ro Loc M 5.50 6.00	57. Mid-s esuits lethod None 0.6	Depth 0.000 0.270	Mean Ve Total Di %Dep 0.0 0.6	MeasD 0.0 0.108	0.73 -0.00 -0.02 Vel 0.0000 0.0010	83 095 297 CorrFact 1. 1.	00 0.00 00 0.00	00 0.000 10 0.135	0.000	0 0.
Mea Disc Mea t 1 2	asurei Clock 18:46 18:46 18:48	ment Ro Loc M 5.50 6.00 6.50	57. Mid-S esuits lethod None 0.6 0.6	Depth 0.000 0.270 0.700	Mean Ve Total D %Dep 0.0 0.6 0.6	MeasD 0.0 0.108 0.280	0.73 -0.00 -0.02 Vel 0.0000 0.0010 -0.0308	83 095 297 CorrFact 1. 1.	00 0.00 00 0.00 00 -0.03	00 0.000 10 0.135 08 0.263	0.0000 0.0000 -0.0081	0 0. -0. 27.
Mea Disc Me t 0 1 2 3	an Temp ch. Equa asurei Clock 18:46 18:46 18:48 19:00	ment Ro Loc M 5.50 6.00 6.50 6.75	57. Mid-3 esuits lethod None 0.6 0.6 0.6	Depth 0.000 0.270 0.700 0.810	Mean Ve Total Di %Dep 0.0 0.6 0.6 0.6	MeasD 0.0 0.108 0.280 0.324	0.72 -0.00 -0.02 Vel 0.0000 0.0010 -0.0308 0.0249	83 095 297 CorrFact 1. 1. 1. 1.	00 0.00 00 0.00 00 -0.03 00 0.02	00 0.000 10 0.135 08 0.263 49 0.203	0.0000 0.0001 -0.0081 0.0050	0 -0. 27. -17.
Mea Disc Me 1 2 3 4	an Temph. Equa asurer Clock 18:46 18:46 18:48 19:00 18:49	ment R Loc M 5.50 6.00 6.50 6.75 7.00	57. Mid-3 esuits lethod None 0.6 0.6 0.6 0.6	Depth 0.000 0.270 0.700 0.810 0.900	Mean Ve Total D %Dep 0.0 0.6 0.6 0.6 0.6	MeasD 0.0 0.108 0.280 0.324 0.360	0.72 -0.00 -0.02 Vel 0.0000 0.0010 -0.0308 0.0249 0.0135	83 095 297 CorrFact 1. 1. 1. <i>1.</i> <i>1.</i> <i>1.</i> <i>1.</i> <i>1.</i> <i>1.</i>	00 0.00 00 0.00 20 -0.03 20 0.02 00 0.01	00 0.000 10 0.135 08 0.263 49 0.203 35 0.225	0.0000 0.0001 -0.0081 0.0050 0.0030	0 -0. 27. -17. 0 -10.
Mea Disc Me 1 2 3 4 5	an Temph. Equa asurer Clock 18:46 18:46 18:48 19:00 18:49 19:02	ment R Loc M 5.50 6.00 6.75 7.00 7.25	57. Mid-3 esuits lethod None 0.6 0.6 0.6 0.6 0.6	Depth 0.000 0.270 0.700 0.810 0.900 1.100	Mean Ve Total D %Dep 0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6	MeasD 0.0 0.108 0.280 0.324 0.360 0.440	0.72 -0.00 -0.02 Vel 0.0000 0.0010 -0.0308 0.0249 0.0135 -0.0118	83 095 297 CorrFact 1. 1. 1. 1. 1. 1.	00 0.00 00 0.00 00 -0.03 00 0.02 00 0.01 00 -0.01	00 0.000 10 0.135 08 0.263 49 0.203 35 0.225 18 0.275	0.0000 0.0001 -0.0081 0.0050 0.0030 -0.0032	0 -0 27. -17. 0 -10. 2 10.
Mea Disc Me 1 2 3 4 5 6	an Temph. Equa asurer Clock 18:46 18:46 18:48 19:00 18:49 19:02 18:51	ment R Loc M 5.50 6.00 6.50 6.75 7.00 7.25 7.50	57. Mid-3 esuits lethod 0.6 0.6 0.6 0.6 0.6 0.6 0.6	Depth 0.000 0.270 0.700 0.810 0.900 1.100 1.180	Mean Ve Total D %Dep 0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6	MeasD 0.0 0.108 0.280 0.324 0.360 0.440 0.472	0.72 -0.00 -0.02 Vel 0.0000 0.0010 -0.0308 0.0249 0.0135 -0.0118 0.0243	83 095 297 CorrFact 1. 1. 1. 1. 1. 1. 1. 1.	00 0.00 00 0.00 00 -0.03 00 0.02 00 0.01 00 -0.01 00 -0.02	00 0.000 10 0.135 08 0.263 49 0.203 35 0.225 18 0.275 43 0.295	0.0000 0.0001 -0.0081 0.0050 0.0030 -0.0032 0.0072	0. -0. 27. -17. 010. 2. 10. 224.
Mea Disc Me t 0 1 2 3 4 5 6 7	an Temph. Equa asurer Clock 18:46 18:46 18:48 19:00 18:49 19:02 18:51 19:03	ment R Loc M 5.50 6.00 <i>6.50</i> <i>6.75</i> 7.00 7.25 7.50 <i>7.75</i>	57. Mid-3 esuits lethod 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	Depth 0.000 0.270 0.810 0.900 1.100 1.180 1.200	Mean Ve Total Di %Dep 0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6	MeasD 0.0 0.108 0.280 0.324 0.360 0.440 0.472 0.480	0.72 -0.00 -0.02 0.0000 0.0010 -0.0308 0.0249 0.0135 -0.0118 0.0243 -0.0220	83 095 297 CorrFact 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	00 0.00 00 0.00 00 -0.03 00 0.02 00 0.01 00 -0.01 00 -0.02 00 -0.02 00 -0.02	00 0.000 10 0.135 08 0.263 49 0.203 35 0.225 18 0.275 43 0.295 20 0.300	0.0000 0.0001 0.0050 0.0030 -0.0030 0.0077 -0.0066	0 -0 27. -17. -10. 2 10. 2 -24. 22.
Mea Disc Me 0 1 2 3 4 5 6 7 8	an Temph. Equa asurer Clock 18:46 18:46 18:48 19:00 18:49 19:02 18:51 19:03 18:52	ment R Loc M 5.50 6.00 <i>6.50</i> <i>6.75</i> 7.00 7.25 7.50 <i>7.75</i> 8.00	57. Mid-3 esuits lethod 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	Depth 0.000 0.270 0.700 0.810 0.900 1.100 1.180 1.200	Mean Ve Total D %Dep 0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6	MeasD 0.0 0.108 0.280 0.324 0.360 0.440 0.472 0.480	0.72 -0.00 -0.02 0.0000 0.0010 -0.0308 0.0249 0.0135 -0.0118 0.0243 -0.0220 -0.0066	83 095 297 CorrFact 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	00 0.00 00 0.00 00 -0.03 00 0.02 00 0.01 00 -0.01 00 -0.02 00 -0.02 00 -0.02	00 0.000 10 0.135 08 0.263 49 0.203 35 0.225 18 0.275 43 0.295 20 0.300 66 0.450	0.0000 0.0001 -0.0081 0.0050 0.0030 -0.0032 0.0077 -0.0066 -0.0030	0 -0. 27. -17. -10. -10. -10. 2 -24. 22. 9
Mea Disc Mea St 0 1 2 3 4 5 6 7	an Temph. Equa asurer Clock 18:46 18:46 18:48 19:00 18:49 19:02 18:51 19:03	ment R Loc M 5.50 6.00 <i>6.50</i> <i>6.75</i> 7.00 7.25 7.50 <i>7.75</i>	57. Mid-3 esuits lethod 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	Depth 0.000 0.270 0.810 0.900 1.100 1.180 1.200	Mean Ve Total Di %Dep 0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6	MeasD 0.0 0.108 0.280 0.324 0.360 0.440 0.472 0.480	0.72 -0.00 -0.02 0.0000 0.0010 -0.0308 0.0249 0.0135 -0.0118 0.0243 -0.0220	83 095 297 CorrFact 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	00 0.00 00 0.00 00 -0.03 00 0.02 00 0.01 00 -0.01 00 -0.02 00 -0.02 00 -0.02	00 0.000 10 0.135 08 0.263 49 0.203 35 0.225 18 0.275 43 0.295 20 0.300 66 0.450 51 0.575	0.0000 0.0001 0.0050 0.0030 -0.0030 0.0077 -0.0066	0 -0. 27. -17. 0 -10. 2 -10. 2 -10. 2 -24. 2 -27. 2 -27. 2 -27. 2 -10. 2



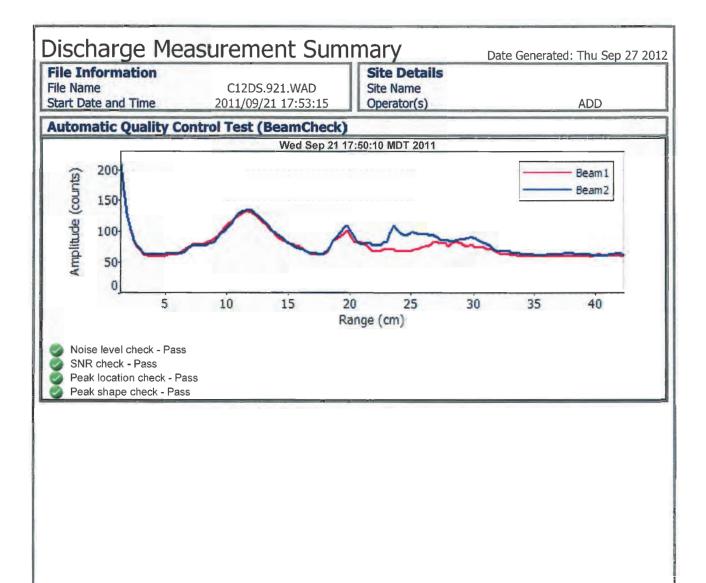
-ile	Inform	ation	surement Sum	Site Details	Date Generated: Thu Sep 27 20
ile I	Name		C12TRIB.921.WAD	Site Name	
Start	Date and	d Time	2011/09/21 18:46:38	Operator(s)	ADD
Qua	lity Cor	ntrol			
St	Loc	%Dep		Message	
2	6.50	0.6	High angle: -102 Low SNR: 4.3,2.5		
		0.6	SNR (3.4) is different from typic High standard error: 0.359	cal SNR (41.6)	
		0.6	High standard error: 0.359		
3	6.75 7.75		High angle: 58 High angle: -170		
9	8.50	0.6	High angle: -180		



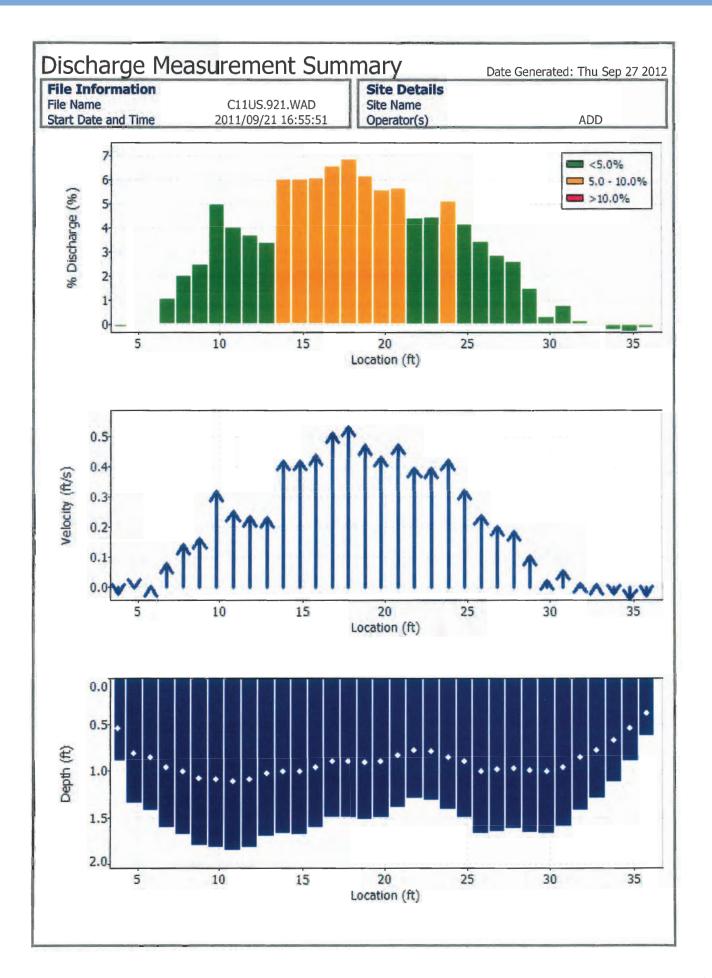
File	e Inform Name t Date a				.921.WAD		Site Det Site Name Operator(1		A	DD	
Svs	stem In	forma	tion		U	nits	(English U	nits) Dis	scharge l	Uncerta	ainty	
	sor Type			FlowTrac		stance	ft		Category	and the second s	the second s	Stats
	al #			P3532		elocity	ft/s	Acc	uracy		1.0%	1.09
CPL	Firmwa	re Versio	on	3.7		ea	ft^2	Dep			0.3%	1.20
Soft	ware Ve	r		2.30	Di	scharge	cfs		ocity		0.5%	1.9
Mou	inting Co	rrection		0.0%		Res and Real 197		Wic			0.1%	0.1
-					and the state of t	Street Street	6 Contraction	Distance in the local	thod		1.5%	0.1
	mmary								Stations		1.5%	_
	raging Ir	nt.	30	90.	Stations		35		erall	-	2.4%	2.59
	t Edge		REV		otal Width		33.500	-	erali		2.770	2.0
	IN SNR		29.1 (otal Area		24.144	1				
	n Temp		51.94		ean Dept		0.721					
DISC	h. Equat	non	Mid-Sec		ean Veloc		0.4838					
_		-		I	otal Disc	narge	11.681	4				
-										and the second		
_	asuren		the local division in which the local division is not the local division of the local division is not the local division of the loca	-								1
_	Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrFact	MeanV	Area	Flow	%
0	17:53 17:57	6.10 6.70	None 0.6	0.000	0.0	0.0	0.0000	1.00 1.00	0.0000	0.000	0.000	
2	17:58	7.70	0.6	0.600	0.6	0.232		1.00	0.1932	0.600	0.116	
3	17:59	8.70	0.6	0.650	0.6	0.240		1.00	0.2388	0.650	0.155	
4	18:01	9.70	0.6	0.640	0.6	0.256		1.00	0.1752	0.640	0.112	
5	18:02	10.70	0.6	0.580	0.6	0.232		1.00		0.580	0.109	
6	18:04	11.70	0.6	0.580	0.6	0.232		1.00	0.1316	0.580	0.076	
7	18:05	12.70	0.6	0.520	0.6	0.208		1.00	0.1939	0.520	0.100	
8	18:06	13.70	0.6	0.780	0.6	0.312		1.00	0.3064	0.780	0.239	
9	18:07	14.70	0.6	0.840	0.6	0.336		1.00	0.4488	0.840	0.377	0 3
10	18:08	15.70	0.6	0.940	0.6	0.376		1.00	0.6220	0.940	0.584	
11	18:09	16.70	0.6	0.840	0.6	0.336		1.00	0.5902	0.840	0.495	
12	18:10	17.70	0.6	0.700	0.6	0.280		1.00	0.6050	0.700	0.423	
13	18:11	18.70	0.6	0.590	0.6	0.236		1.00	0.6808	0.590	0.401	
14	18:12	19.70	0.6	0.550	0.6	0.220		1.00	0.6188	0.550	0.340	
15 16	18:13 18:14	20.70	0.6	0.500	0.6	0.200		<u>1.00</u> 1.00	0.6634	0.500	0.307	
17	18:14	22.70	0.6	0.480	0.6	0.192		1.00		0.480	0.304	
18	18:16	23.70	0.6	0.520	0.6	0.220		1.00		0.520	0.333	
19	18:17	24.70	0.6	0.580	0.6	0.232		1.00	0.6683	0.580	0.387	
20	18:18	25.70	0.6	0.710	0.6	0.284		1.00	0.5469	0.710	0.388	
21	18:19	26.70	0.6	0.760	0.6	0.304		1.00	0.6155	0.760	0.467	7 4
22	18:20	27.70	0.6	0.800	0.6	0.320	0.7008	1.00	0.7008	0.800	0.560	
23	18:21	28.70	0.6	0.880	0.6	0.352		1.00	0.7674	0.880	0.675	
	18:22	29.70	0.6	0.910	0.6	0.364		1.00	0.6578	0.910	0.598	
	18:28	30.70	0.6	1.090	0.6	0.436		1.00	0.5801	1.090	0.632	
25	18:26	31.70	0.6	1.300	0.6	0.520		1.00	0.4091	1.300	0.531	
25 26	10 20	32.70	0.6	1.240	0.6	0.496		1.00	0.3711	1.240	0.460	
25 26 27	18:29		0.6	1.010	0.6	0.404		1.00	0.5581	1.010	0.563	
25 26 27 28	18:30	33.70			0.6	0.396		1.00	0.5902	0.990	0.584	
25 26 27 28 29	18:30 18:31	34.70	0.6		0.0	n area						
25 26 27 28 29 30	18:30 18:31 18:32	34.70 35.70	0.6	0.890	0.6	0.356		1.00				
31	18:30 18:31 18:32 18:33	34.70 35.70 36.70	0.6 0.6	0.890	0.6	0.280	0.4685	1.00	0.4685	0.700	0.328	0 2
25 26 27 28	18:30 18:31 18:32	34.70 35.70	0.6	0.890			0.4685					0 2



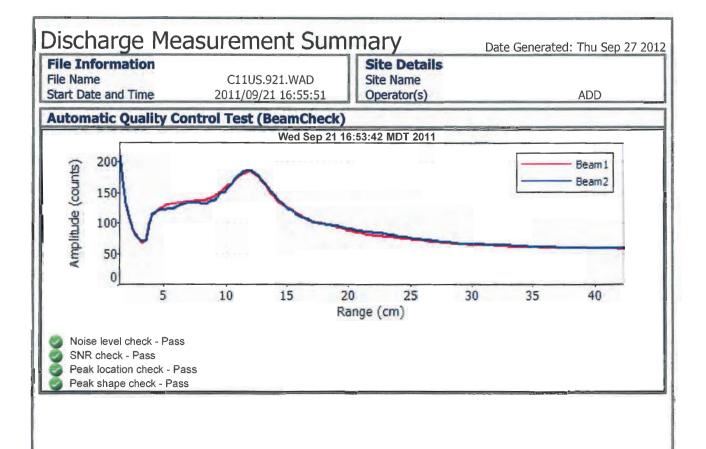
Dis	char	ge Me	asurement Sum	imary	Date Generated: Thu Sep 27 201
File I	Information Name Date and		C12DS.921.WAD 2011/09/21 17:53:15	Site Details Site Name Operator(s)	ADD
Qua	lity Con	trol			
St	Loc	%Dep	The second states to	Message	
1	6.70	0.6	Boundary QC is Fair; possible bo	undary interference	
4	9.70		High angle: 20		
33	38.70	0.6	High differences in beam SNR: 1 Boundary QC is Poor; possible bo	7.6,27.9 oundary interference	



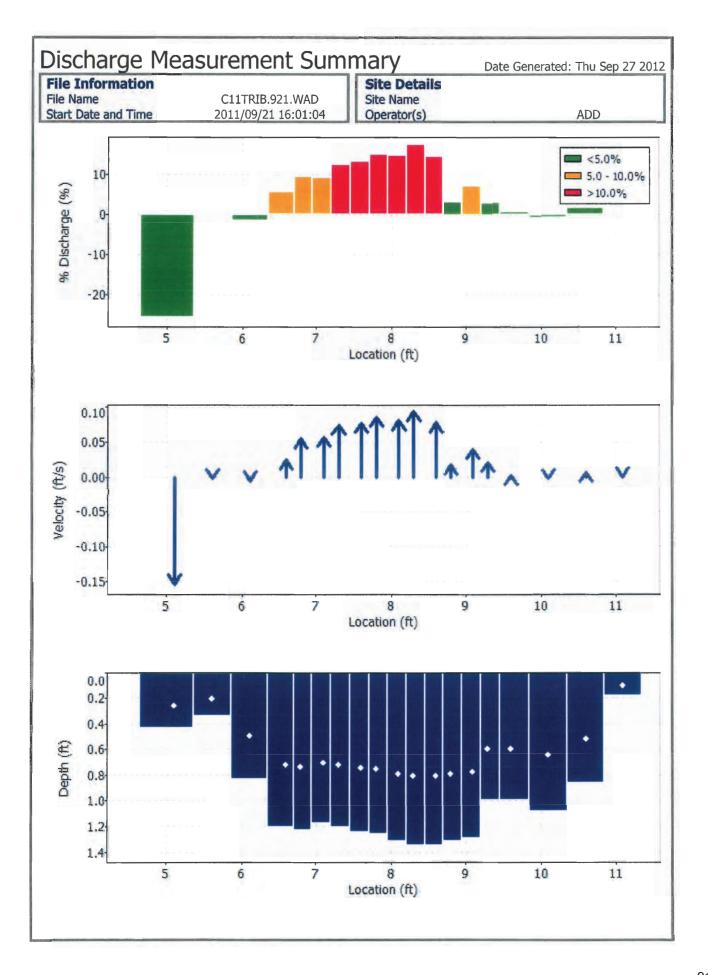
File	Name Name The Date a				S.921.WA 9/21 16:5		Site De Site Name Operator	e			ADD	
Sv	stem In	nforma	ation			Units	(English L	Inits)	ischarge	Uncert	ainty	
	sor Type			FlowTra		Distance	ft		Category	Concession of the local division of the loca		tats
	al #			P353		Velocity	ft/s		ccuracy		1.0%	1.09
	J Firmwa	re Versi	ion	3.7	_	Area	ft^2		epth		0.1%	0.69
	ware Ve			2.30		Discharge	cfs		elocity		0.7%	2.69
	unting Co		1	0.0%		siscilarge	2		Vidth		0.1%	0.10
									The second se			0.1
Su	mmary	0							lethod		1.7%	
	raging In		30)	# Stations	5	35	and a second sec	Stations		1.5%	
	t Edge		RE	W	Total Widt	th	33.500		verall		2.5%	2.9%
	IN SNR		31.2	dB 1	Total Area	1	48.945					
	n Temp		52.77		Mean Dep		1.461					
	h. Equat		Mid-Se		Mean Velo		0.2385					
					Total Dis		11.671					
-				-	1-12							_
Mo	asuren	nont D	oculte		Patronal pre-							
St	Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrFact	MeanV	Area	Flow	%0
0	16:55	3.30	None	and the local division of the local division			0.0000	1.00	and in case of the local division of the loc	0.000	0.0000	
1	16:55	3.80	0.6	0.900	0.6	0.360	-0.0210	1.00		0.675	-0.0142	the summer of the local division of the loca
2	16:57	4.80	0.6	1.350		0.540	-0.0036	1.00	successive of successive statements	1.350	-0.0049	_
3	16:58	5.80	0.6	1.430			0.0036	1.00		1.430	0.0052	
4	17:00	6.80	0.6			and the second se	0.0804	1.00		1.610	0.1294	
5	17:02	7.80	0.6	1.680		the second day of the	0.1424	1.00		1.680	0.2392	
6	17:03	8.80	0.6	Contraction of the local division of the loc			0.1634	1.00	No. of Concession, Name of	1.800	0.2941	
7	17:04	9.80	0.6	1.830			0.3182	1.00		1.830	0.5824	
8	17:06	10.80	0.6	1.860	0.6		0.2523	1.00		1.860	0.4692	
9	17:07	11.80	0.6	1.830	0.6	the other designs and the second division in which the second division is not the second division of the second di	0.2359	1.00		1.830	0.4317	
10	17:08	12.80	0.6	1.710	0.6	0.684	0.2323	1.00	0.2323	1.710	0.3972	3
11	17:09	13.80	0.6	1.670	0.6		0.4206	1.00		1.670	0.7024	
12	17:10	14.80	0.6	1.680	0.6		0.4196	1.00		1.680	0.7050	
13	17:11	15.80	0.6	1.610	0.6		0.4393	1.00		1.610	0.7072	
14	17:13	16.80	0.6	1.500	0.6		0.5121	1.00		1.500	0.7682	
15	17:16	17.80	0.6	1.500	0.6		0.5338	1.00		1.500	0.8007	
16	17:17	18.80	0.6	1.520	0.6	And in case of the local division in which the local division is not the local division in the local division is not the local division in the local division in the local division is not the local division in the local din the local division in the local division in the local din the l	0.4715	1.00		1.520	0.7166	
17	17:18	19.80	0.6	1.500			0.4341	1.00		1.500	0.6511	
18	17:19	20.80	0.6		0.6		0.4734	1.00	and the second data was not seen as a second data was a second data was a second data was a second data was a s	1.390	0.6581	
19	17:20	21.80	0.6	1.300	0.6		0.3963	1.00		1.300	0.5152	
20	17:21 17:23	22.80	0.6	1.320		the second se	0.3957	1.00		1.320	0.5222	
21 22	17:23	23.80	0.6	1.420	0.6	0.568	0.4213	1.00	Statement and a statement of the stateme	1.420	0.5982	
22	17:20	25.80	0.6	1.500	0.6		0.3245	1.00		1.500	0.486/	
24	17:28	26.80	0.6	1.650	0.6		0.2408	1.00	the subscription of the local division of th	1.650	0.4021	
25	17:20	27.80	0.6	1.620	0.6	the star party of the local division of the	0.1880	1.00		1.620	0.3046	Concession of the local division of the loca
26	17:31	28.80	0.6	1.660	0.6		0.1066	1.00		1.660	0.1770	
	17:32	29.80	0.6	1.670	0.6	0.668	0.0246	1.00		1.670	0.0411	
	17:33	30.80	0.6	1.600	0.6		0.0587	1.00		1.600	0.0940	-
27	17:34	31.80	0.6	1.430			0.0148	1.00	The rest of the local division of the local	1.430	0.0211	
27 28		32.80	0.6	1.300	0.6	0.520	0.0098	1.00		1.300	0.0128	
27 28 29						0.452	-0.0226	1.00		1.130	-0.0256	
27 28 29 30 31	17:35 17:36	33.80	0.6	1.130	0.6	0.7521	0,02201	1.00				
27 28 29 30	17:35		0.6	1.130 0.900	0.6	0.360	-0.0400	1.00		0.900	-0.0360	
27 28 29 30 31	17:35 17:36	33.80	the state of the s		the second s	0.360			-0.0400			-0



	and the second second		asurement Sum	Site Details	Date Generated: Thu Sep 27 201
File Information File Name Start Date and Time			C11US.921.WAD 2011/09/21 16:55:51	ADD	
Qua	lity Con	trol			
St	Loc	%Dep		Message	
1	3.80		High angle: 180 SNR (48.5) is different from typic	al SNR (31.2)	
2	4.80	0.6			
3	5.80	0.6	SNR (42.4) is different from typic	al SNR (31.2)	
27	29.80		High angle: 26 High SNR variation during measu	rement: 5.2,5.2	
30	32.80		SNR (44.2) is different from typic High SNR variation during measu		
31	33.80	0.6	High angle: 139 SNR (43.4) is different from typic		
32	34.80	0.6	High angle: 158 SNR (45.5) is different from typic		Barry and the second
33	35.80	0.6 0.6	High angle: -148 SNR (43.0) is different from typic Boundary QC is Good; possible bo	al SNR (31.2)	

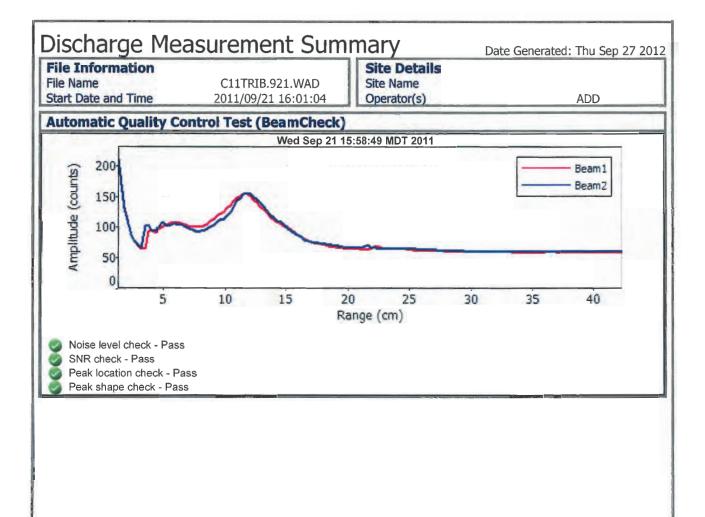


File	e Infor Name				IB.921.W		Site Nan	ne			Thu Sep	
-	rt Date a			2011/09/21 16:01:04			Operato	r(s)			ADD	_
System Informati			tion				(English	Units)	Discharge Uncertainty			
	sor Type	9		FlowTra		Distance	ft		Category	I		Stats
	ial #	and Manual				Velocity	ft/		Accuracy		1.0%	1.00
	J Firmwa		on	3.7		Area	ft^		Depth		0.4%	6.4
	tware Ve			2.30		Discharge	cf	Contraction of the local division of the loc	Velocity	-	144.5%	17.0
MO	unting Co	orrection		0.0%					Width		0.2%	0.2
Su	mmary	0						in the second	Method		3.5%	
	raging I		30)	# Station	S	21	a line	# Stations		2.4%	
	rt Edge		RE		Total Wid		7.40		Overall	1	44.6%	18.2
	an SNR		34.0		Total Area		6.21					
	an Temp	E.	58.66		Mean Dep	oth	0.83					
	ch. Equa		Mid-Se		Mean Velo		0.029					
				Total Discharge			0.180	08				
St	asuren Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrFact	MeanV	Area	Flow	
_	the second se	and the second se		Depth	%Dep	MeasD	Vel	CorrFact	MeanV	Area	Flow	%0
St 0	Clock 16:01	Loc 4.20	Method None	0.000	0.0	0.0	0.0000	1.00	0.0000	0.000	0.0000	0 0
5t 0 1	Clock 16:01 16:02	Loc 4.20 5.10	Method None 0.6	0.000	0.0	0.0	0.0000 -0.1539	1.00	0.0000	0.000 0.301	0.0000	-25
0 1 2	Clock 16:01 16:02 16:04	Loc 4.20 5.10 5.60	Method None 0.6 0.6	0.000 0.430 0.340	0.0 0.6 0.6	0.0 0.172 0.136	0.0000 -0.1539 -0.0020	1.00 1.00 1.00	0.0000 -0.1539 -0.0020	0.000 0.301 0.170	0.0000 -0.0463 -0.0003	-25
5t 0 1 2 3	Clock 16:01 16:02 16:04 16:06	Loc 4.20 5.10 5.60 6.10	Method None 0.6 0.6 0.6	0.000 0.430 0.340 0.830	0.0 0.6 0.6 0.6	0.0 0.172 0.136 0.332	0.0000 -0.1539 -0.0020 -0.0062	1.00 1.00 1.00 1.00	0.0000 -0.1539 -0.0020 -0.0062	0.000 0.301 0.170 0.415	0.0000 -0.0463 -0.0003 -0.0026	-25 -0 -1
0 1 2 3 4	Clock 16:01 16:02 16:04 16:06 16:07	Loc 4.20 5.10 5.60 6.10 6.60	Method None 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210	0.0 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484	0.0000 -0.1539 -0.0020 -0.0062 0.0246	1.00 1.00 1.00 1.00 1.00	0.0000 -0.1539 -0.0020 -0.0062 0.0246	0.000 0.301 0.170 0.415 0.423	0.0000 -0.0463 -0.0003 -0.0026 0.0104	-25 -0 -1
St 0 1 2 3 4 5	Clock 16:01 16:02 16:04 16:06 16:07 16:27	Loc 4.20 5.10 5.60 6.10 6.60 6.80	Method None 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230	0.0 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554	1.00 1.00 1.00 1.00 1.00 1.00	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554	0.000 0.301 0.170 0.415 0.423 0.307	0.0000 -0.0463 -0.0003 -0.0026 0.0104 0.0170	-25 -0 -1 5
0 1 2 3 4 5 6	Clock 16:01 16:02 16:04 16:07 16:27 16:27 16:09	Loc 4.20 5.10 5.60 6.10 6.60 6.80 7.10	Method None 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230 1.180	0.0 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492 0.472	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0571	1.00 1,00 1.00 1.00 1.00 1.00 1.00	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0551	0.000 0.301 0.170 0.415 0.423 0.307 0.295	0.0000 -0.0463 -0.0003 -0.0026 0.0104 0.0170 0.0168	-25 -0 -1 5 9
0 1 2 3 4 5	Clock 16:01 16:02 16:04 16:06 16:07 16:27	Loc 4.20 5.10 5.60 6.10 6.60 6.80	Method None 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230	0.0 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554	1.00 1.00 1.00 1.00 1.00 1.00	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748	0.000 0.301 0.170 0.415 0.423 0.307 0.295 0.302	0.0000 -0.0463 -0.0003 -0.0026 0.0104 0.0170 0.0168 0.0226	-25 -0 -1 5 9 9 9
St 0 1 2 3 4 5 6 7 8 9	Clock 16:01 16:02 16:04 16:06 16:07 16:27 16:29 16:29 16:11 16:33	Loc 4.20 5.10 5.60 6.10 6.60 6.80 7.10 7.30 7.60 7.80	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.830 1.210 1.230 1.210 1.210 1.250 1.260	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492 0.472 0.484 0.500 0.504	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.00860	0.000 0.301 0.170 0.415 0.423 0.307 0.295 0.302 0.302 0.313 0.315	0.0000 -0.0463 -0.0003 -0.0026 0.0104 0.0170 0.0168 0.0226 0.0241 0.0271	0 00 -25 -00 -11 55 99 99 12 -12 -12 -12 -12 -12 -12 -12 -12 -12
St 0 1 2 3 4 5 6 7 8 9 10	Clock 16:01 16:02 16:04 16:06 16:07 16:27 16:09 16:29 16:11 16:33 16:13	Loc 4.20 5.10 5.60 6.10 6.60 6.80 7.10 7.30 7.60 7.80 8.10	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230 1.210 1.250 1.250 1.260 1.320	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492 0.472 0.484 0.500 0.504 0.528	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810	0.000 0.301 0.170 0.415 0.423 0.307 0.295 0.302 0.313 0.315 0.330	0.0000 -0.0463 -0.0026 0.0104 0.0170 0.0168 0.0226 0.0241 0.0271 0.0267	0 0 -25 -0 -1 5 9 9 9 9 9 12 12 12 12 12 14
St 0 1 2 3 4 5 6 7 8 9 10 11	Clock 16:01 16:02 16:04 16:06 16:07 16:27 16:09 16:29 16:11 16:33 16:13 16:35	Loc 4.20 5.10 5.60 6.10 6.60 6.80 7.10 7.30 7.60 7.80 8.10 8.30	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230 1.210 1.250 1.250 1.260 1.320 1.350	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492 0.472 0.484 0.500 0.500 0.504 0.528 0.540	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0942	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0942	0.000 0.301 0.170 0.415 0.423 0.307 0.295 0.302 0.313 0.315 0.330 0.338	0.0000 -0.0463 -0.0003 -0.0026 0.0104 0.0170 0.0168 0.0226 0.0241 0.0271 0.0267 0.0318	0 -25 -0 -1 -1 5 -1 5 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1
0 1 2 3 4 5 6 7 8 9 10 11 12	Clock 16:01 16:02 16:04 16:06 16:07 16:27 16:29 16:11 16:33 16:13 16:35 16:15	Loc 4.20 5.10 5.60 6.10 6.60 6.80 7.10 7.30 7.60 7.80 8.10 8.30 8.60	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230 1.210 1.250 1.250 1.260 1.320 1.350	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492 0.472 0.484 0.500 0.500 0.504 0.528 0.540 0.540	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0810 0.0942 0.0778	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 -0.1539 -0.0020 -0.00246 0.0254 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0810 0.0942 0.0778	0.000 0.301 0.170 0.415 0.423 0.307 0.295 0.302 0.313 0.315 0.330 0.338 0.338	0.0000 -0.0463 -0.0003 -0.0026 0.0104 0.0170 0.0168 0.0226 0.0241 0.0271 0.0267 0.0318 0.0262	0 -25 -0 -1 -1 5 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1
0 1 2 3 4 5 6 7 8 9 10 11 12 13	Clock 16:01 16:02 16:04 16:06 16:07 16:27 16:09 16:29 16:11 16:33 16:13 16:13 16:35 16:15 16:36	Loc 4.20 5.10 5.60 6.10 6.60 6.80 7.10 7.30 7.60 7.80 8.10 8.30 8.60 8.80	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230 1.210 1.250 1.250 1.260 1.320 1.350 1.350 1.320	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492 0.472 0.484 0.500 0.500 0.504 0.528 0.540 0.540 0.528	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0810 0.0942 0.0778 0.0180	$\begin{array}{c} 1.00\\$	0.0000 -0.1539 -0.0020 -0.0026 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0810 0.0942 0.0778 0.0180	0.000 0.301 0.170 0.415 0.423 0.307 0.295 0.302 0.313 0.315 0.330 0.338 0.338 0.338	0.0000 -0.0463 -0.0003 -0.0026 0.0104 0.0170 0.0168 0.0226 0.0241 0.0271 0.0267 0.0318 0.0262 0.0060	0 -25 -00 -11 55 99 99 99 12 13 15 14 14 17 14 17 14 14 17 14 14 15 15 15 15 15 15 15 15 15 15
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14	Clock 16:01 16:02 16:04 16:06 16:07 16:27 16:29 16:11 16:33 16:13 16:13 16:15 16:36 16:16	Loc 4.20 5.10 5.60 6.10 6.60 6.80 7.10 7.30 7.60 7.80 8.10 8.30 8.60 8.80 9.10	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230 1.230 1.250 1.250 1.260 1.320 1.350 1.350 1.320 1.320	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492 0.472 0.484 0.500 0.500 0.504 0.528 0.540 0.540 0.528 0.540	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0810 0.0942 0.0778 0.0180 0.0400	$\begin{array}{c} 1.00\\$	0.0000 -0.1539 -0.0020 -0.00246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0810 0.0942 0.0778 0.0180 0.0400	0.000 0.301 0.170 0.415 0.423 0.307 0.295 0.302 0.313 0.315 0.330 0.338 0.338 0.338 0.330 0.323	0.0000 -0.0463 -0.0026 0.0104 0.0170 0.0168 0.0226 0.0241 0.0271 0.0267 0.0318 0.0262 0.0318 0.0262 0.0060	0 -25 -00 -11 55 99 99 99 122 13 13 15 14 14 17 2 14 0 33 7
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14	Clock 16:01 16:02 16:04 16:06 16:07 16:27 16:29 16:29 16:11 16:33 16:13 16:13 16:15 16:36 16:16 16:37	Loc 4.20 5.10 5.60 6.10 6.60 6.80 7.10 7.30 7.60 7.80 8.10 8.30 8.30 8.60 8.80 9.10 9.30	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230 1.230 1.250 1.250 1.260 1.320 1.350 1.350 1.320 1.320 1.320 1.320 1.290	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492 0.472 0.484 0.500 0.504 0.504 0.528 0.540 0.540 0.528 0.540 0.528 0.516 0.400	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0942 0.0778 0.0180 0.0400 0.0213	$\begin{array}{c} 1.00\\$	0.0000 -0.1539 -0.0020 -0.00246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0810 0.0942 0.0778 0.0180 0.0400 0.0213	0.000 0.301 0.170 0.415 0.423 0.307 0.295 0.302 0.313 0.315 0.330 0.338 0.338 0.338 0.330 0.323 0.250	0.0000 -0.0463 -0.0026 0.0104 0.0170 0.0168 0.0226 0.0241 0.0271 0.0267 0.0318 0.0262 0.0318 0.0262 0.0060 0.0129 0.0053	0 0 -25: -00 -11 5: 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	Clock 16:01 16:02 16:04 16:06 16:07 16:27 16:29 16:11 16:33 16:13 16:13 16:15 16:35 16:15 16:36 16:37 16:18	Loc 4.20 5.10 5.60 6.10 6.60 7.10 7.30 7.60 7.80 8.10 8.30 8.30 8.60 8.80 9.10 9.60	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230 1.230 1.250 1.250 1.350 1.350 1.350 1.350 1.320 1.320 1.320 1.320 1.320 1.290 1.000	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492 0.472 0.484 0.500 0.504 0.504 0.528 0.540 0.540 0.528 0.540 0.528 0.516 0.400 0.400	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0942 0.0778 0.0180 0.0400 0.0213 0.0030	$\begin{array}{c} 1.00\\$	0.0000 -0.1539 -0.0020 -0.0020 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0810 0.0942 0.0778 0.0180 0.0180 0.0400 0.0213 0.0030	0.000 0.301 0.170 0.415 0.423 0.307 0.295 0.302 0.313 0.315 0.330 0.338 0.338 0.338 0.338 0.330 0.323 0.250 0.400	0.0000 -0.0463 -0.0026 0.0104 0.0170 0.0168 0.0226 0.0241 0.0271 0.0267 0.0318 0.0267 0.0318 0.0267 0.0318 0.0267 0.0318 0.0267 0.00129	$\begin{array}{c c} & 0 \\ & 0 \\ -25 \\ -0 \\ -1 \\ 5 \\ -25 \\ -$
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	Clock 16:01 16:02 16:04 16:06 16:07 16:27 16:29 16:19 16:13 16:13 16:13 16:15 16:35 16:15 16:36 16:16 16:37 16:18 16:20	Loc 4.20 5.10 5.60 6.10 6.60 6.80 7.10 7.30 7.60 7.80 8.10 8.30 8.10 8.30 8.60 8.80 9.10 9.60 10.10	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230 1.230 1.250 1.250 1.260 1.320 1.350 1.350 1.350 1.320 1.320 1.390 1.000 1.000 1.000	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492 0.472 0.484 0.500 0.504 0.504 0.528 0.540 0.540 0.528 0.540 0.528 0.540 0.528 0.516 0.400 0.432	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0942 0.0778 0.0180 0.0400 0.0213 0.0030 -0.0023	$\begin{array}{c} 1.00\\$	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0571 0.0771 0.0860 0.0810 0.0942 0.0778 0.0180 0.0180 0.0180 0.0213 0.0030 -0.0023	0.000 0.301 0.170 0.415 0.423 0.307 0.295 0.302 0.313 0.315 0.330 0.338 0.338 0.338 0.338 0.338 0.330 0.323 0.250 0.400 0.540	0.0000 -0.0463 -0.0026 0.0104 0.0170 0.0168 0.0226 0.0241 0.0271 0.0267 0.0318 0.0267 0.0318 0.0262 0.0060 0.0129 0.0053 0.0012 -0.0012	$\begin{array}{c c} & 0 \\ & 0 \\ \hline & -25 \\ -0 \\ -0 \\ -11 \\ \hline & 5 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 12 \\ 13 \\ 13 \\ 13 \\ 12 \\ 14 \\ 14 \\ 17 \\ 2 \\ 14 \\ 17 \\ 2 \\ 14 \\ 17 \\ 2 \\ 14 \\ 17 \\ 2 \\ 14 \\ 17 \\ 2 \\ 14 \\ 17 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 14 \\ 2 \\ 2 \\ 2 \\ 0 \\ 2 \\ -0 \\ 2 \\ -0 \\ 2 \\ -0 \\ 2 \\ -0 \\ 2 \\ -0 \\ 2 \\ -0 \\ 2 \\ -0 \\ 2 \\ -0 \\ 2 \\ -0 \\ -0$
St 0 1 2 3 4 5 6 7 7 8 9 9 10 11 12 13 14 15 16	Clock 16:01 16:02 16:04 16:06 16:07 16:27 16:29 16:11 16:33 16:13 16:13 16:15 16:35 16:15 16:36 16:37 16:18	Loc 4.20 5.10 5.60 6.10 6.60 7.10 7.30 7.60 7.80 8.10 8.30 8.30 8.60 8.80 9.10 9.60	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.430 0.340 0.830 1.210 1.230 1.230 1.250 1.250 1.350 1.350 1.350 1.350 1.320 1.320 1.320 1.320 1.320 1.290 1.000	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.172 0.136 0.332 0.484 0.492 0.472 0.484 0.500 0.504 0.504 0.528 0.540 0.540 0.528 0.540 0.528 0.516 0.400 0.400	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0942 0.0778 0.0180 0.0400 0.0213 0.0030	$\begin{array}{c} 1.00\\$	0.0000 -0.1539 -0.0020 -0.0062 0.0246 0.0554 0.0554 0.0571 0.0748 0.0771 0.0860 0.0810 0.0942 0.0778 0.0180 0.0180 0.0213 0.0030 -0.0023 0.0072	0.000 0.301 0.170 0.415 0.423 0.307 0.295 0.302 0.313 0.315 0.330 0.338 0.338 0.338 0.338 0.330 0.323 0.250 0.400	0.0000 -0.0463 -0.0026 0.0104 0.0170 0.0168 0.0226 0.0241 0.0271 0.0267 0.0318 0.0267 0.0318 0.0267 0.0318 0.0267 0.0318 0.0267 0.00129	-25. -0. -1. 5. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 12. 13. 155 144 177 144 177 2. 0. 2. 0. 2. 0. 2. 0. 12. 13. 15. 14. 17. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.

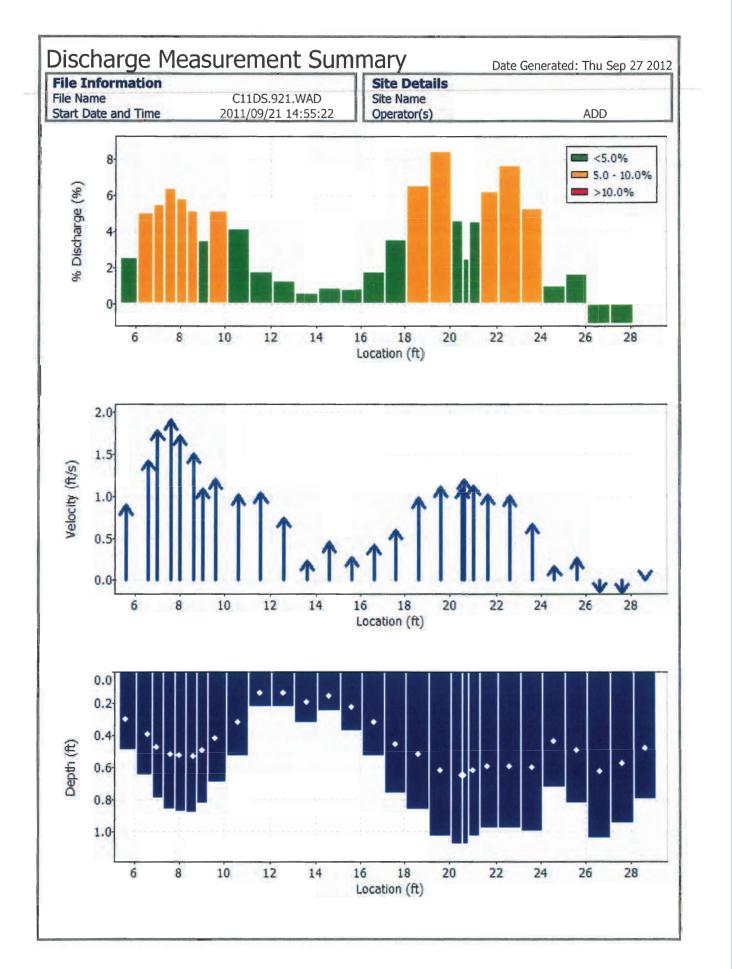


-			asurement Sum		Date Generated: Thu Sep 27 201
File I	Informa Name Date and		C11TRIB.921.WAD 2011/09/21 16:01:04	Site Details Site Name Operator(s)	ADD
Qua	lity Con	trol			
St	Loc	%Dep		Message	
1	5.10	0.6 0.6 0.6	High angle: -179 Low SNR: 9.8,0.0 SNR (4.9) is different from typica High SNR variation during measu High standard error: 0.868		
2	5.60	0.6	High number of spikes: 4		
3	6.10	0.6	SNR (46.2) is different from typic	al SNR (34.0)	
4	6.60	0.6	High angle: -27		
5	6.80	0.6	High angle: -29		
6	7.10	0.6	High angle: -33		
14	9.10	0.6	High angle: -23		
15	9.30	0.6	High angle: 25		
19	11.10		High SNR variation during measu Boundary QC is Fair; possible bo		

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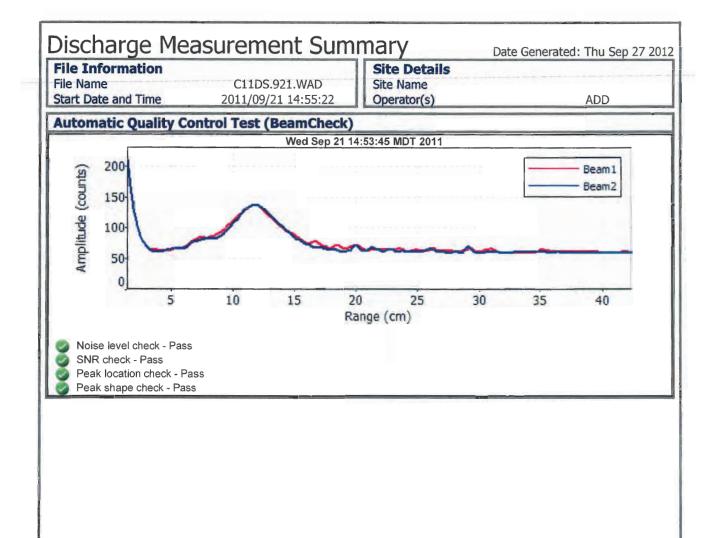
File	e Infor Name rt Date a				S.921.WA 9/21 14:5	0.0	Site Details Site Name Operator(s) ADD							
Sy	stem In	nforma	ation			Units	(English U	Inits)	Di	scharge	Uncert	ainty		
	sor Type			FlowTra	cker 🚺	Distance	ft			Category		ISO Stats		
Ser	ial #			P353	2	Velocity	ft/s		Ac	curacy		1.0%	1.0%	
CPL	J Firmwa	re Versi	on	3.7		Area	ft^2	2		pth		0.3%	1.8%	
Sof	tware Ve	r		2.30		Discharge	cfs			locity		0.9%	3.6%	
Mo	unting Co	orrection	1	0.0%	0					dth		0.1%	0.1%	
				and the second second						thod		1.7%		
	mmary									Stations		1.7%		
	eraging In	nt.	30		# Stations		31			rall		2.7%	4.1%	
	rt Edge		RE		otal Widt		24.500		0	ciali		217 70	4.2.7	
	an SNR		32.4		otal Area		16.942							
	an Temp		53.04		lean Dep		0.691							
Dis	ch. Equat	tion	Mid-Se		lean Velo		0.7633							
_				1	otal Dis	charge	12.930	18						
-	-	-				- M				5700 B	~ 23			
	asuren	the second se											1	
St		Loc	Method	Depth	%Dep	MeasD	Vel	CorrFa		MeanV	Area	Flow	%Q	
0	14:55	5.10	None		0.0		0.0000		1.00	0.0000	0.000	0.0000	and the second s	
1	14:57	5.60	0.6		0.6		0.8976		1.00	0.8976	0.368	0.3300		
23	14:59 15:43	6.60 7.00	0.6		0.6		1.4350 1.7930		1.00	1.4350	0.455	0.6528		
3	15:43	7.60	0.6		0.6	0.310	1.9150		1.00	1.9150	0.395	0.8234		
5	15:05	8.00	0.6		0.6		1.7303		1.00	1.7303	0.435	0.7528		
6	15:04	8.60	0.6	0.880	0.6	Statement Street Street, or other	1.5177		1.00	1.5177	0.440	0.6677		
7	15:46	9.00	0.6		0.6		1.0991		1.00	1.0991	0.410	0.4506		
8	15:05	9.60	0.6	0.690	0.6		1.2087		1.00	1.2087	0.552	0.6672		
9	15:06	10.60	0.6		0.6	the second se	1.0197		1.00	1.0197	0.530	0.5403		
10	15:14	11.60	0.6	0.220	0.6	successive sector successive sector and the sector of the	1.0423		1.00	1.0423	0.220	0.2295		
11	15:15	12.60	0.6		0.6		0.7503		1.00	0.7503	0.220	0.1652		
12	15:18	13.60	0.6	0.320	0.6	0.128	0.2365		1.00	0.2365	0.320	0.0757		
13	15:20	14.60	0.6		0.6	No. of Concession, Name	0.4587		1.00	0.4587	0.250	0.1147		
14	15:23	15.60	0.6	0.370	0.6	A DESCRIPTION OF TAXABLE PARTY OF TAXABLE PARTY.	0.2838	and the second se	1.00	0.2838	0.370	0.1050	0 0.	
15	15:25	16.60	0.6		0.6		0.4249		1.00	0.4249	0.530	0.2251	1	
16	15:27	17.60	0.6		0.6		0.6070		1.00	0.6070	0.760	0.4612		
17	15:28	18.60	0.6		0.6		0.9846		1.00	0.9846	0.860	0.8466		
18	15:29	19.60	0.6		0.6		1.1148	strength of the local division in which the	1.00	1.1148	0.978	1.0907		
19	15:49	20.50	0.6		0.6	summer of the local division in which the local division is not determined in which the local division is not determined in th	1.0994		1.00	1.0994	0.540	0.593		
20	15:31	20.60	0.6		0.6		1.2044		1.00	1.2044	0.270	0.3257		
21	15:50	21.00	0.6		0.6	strength and a diversity of the second state.	1.1335	second se	1.00	1.1335	0.515	0.583		
22	15:32	21.60	0.6	successive successive states where	0.6		1.0262		1.00	1.0262	0.784	0.8040		
23	15:33	22.60	0.6	the second se	0.6	spont statement of the local division in which the local division in which the local division is not the local division of the local division in the local division in the local division is not the local division of the local division in the local division in the local division in the local division in the local division of the local division in the local division in the local division in the local division in the local division of the local division in the l	1.0098		1.00	1.0098	0.980	0.9890		
24	15:34	23.60	0.6	and the second se	0.6	Concession of the local division of the loca	0.6791		1.00	0.6791	1.000	Contraction of the local division of the loc	_	
25	15:36	24.60	0.6	0.720	0.6		0.1736		1.00	0.1736	0.720	0.125		
26	15:37 15:38	25.60	0.6	1.040	0.6	the second se	-0.141.7	and the second division of the second divisio	.00	-0,1417	1.040,	-0.1434	_	
27 28	15.39	27:60	0.6	0.950	0.6		-0.1539		.00	-0.1539	0.950	-0.1462		
201		28:60	0.6		0.6	the summer of the summer of the summer of the summer summer summer summer summer summer summer summer summer su	-0.2003		.00	-0.1559	0.800	-0.0003		
29	15:40													



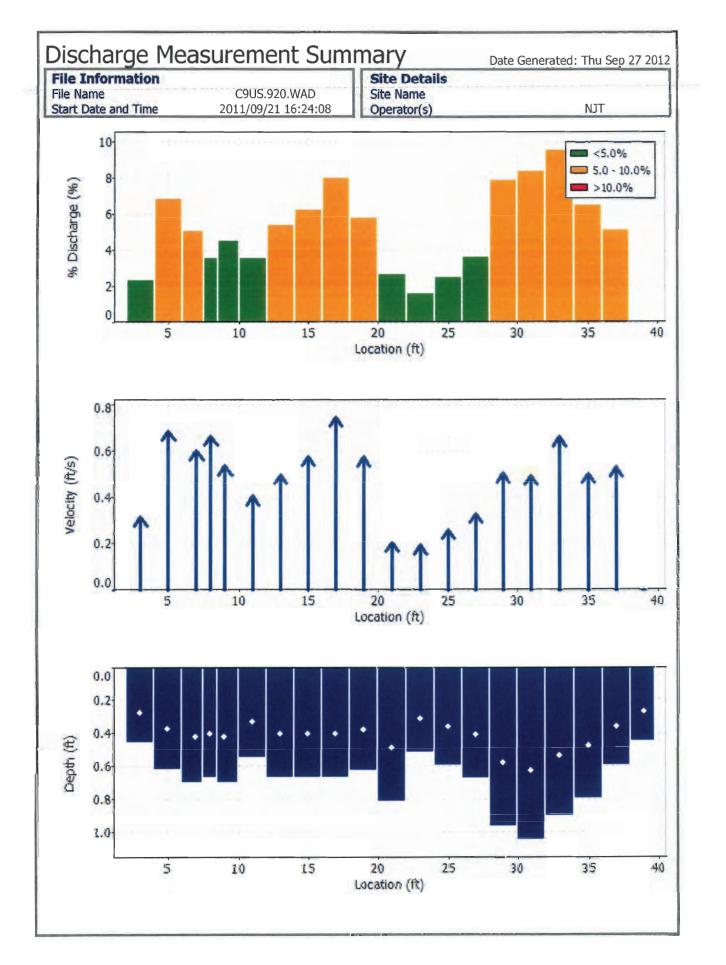
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File N	Informa lame Date and		C11DS.921.WAD 2011/09/21 14:55:22	Site Details Site Name Operator(s)	ADD
Qua	lity Cont	rol			
St	Loc	%Dep		Message	
12	13.60	0.6	High angle: -27		
26	25.60	0.6	High SNR variation during measured	surement: 7.3,7.3	
27	26.60		High angle: -149		
28	27.60	0.6	High angle: -155		
29	28.60		High differences in beam SNR: SNR (57.4) is different from typ		

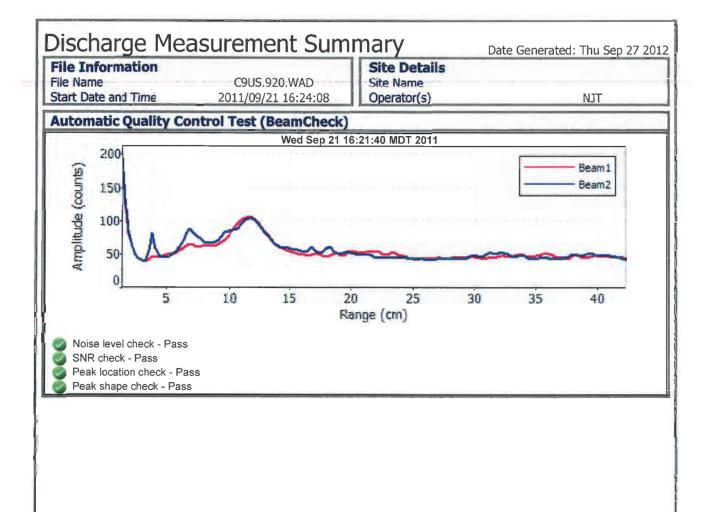
1



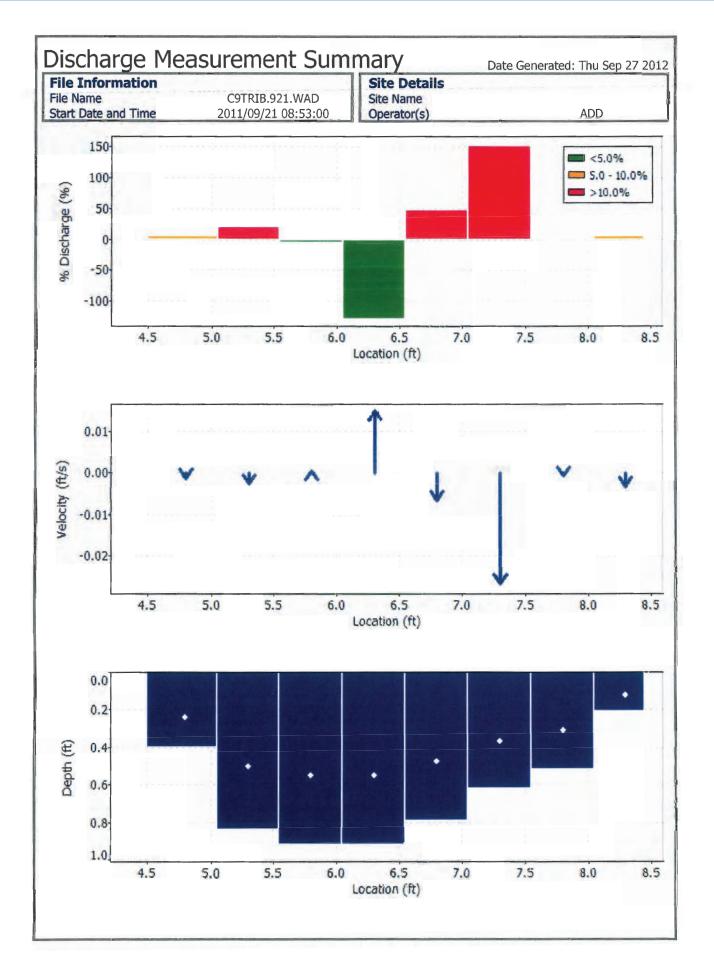
File	Name Name rt Date ar				920.WAD 21_16:24:		Site Det Site Name Operator(s	•			N	IJŢ		
System Information Units							English U	nits)	Discharge Uncertainty					
	sor Type			FlowTrack	ker Di	stance	ce ft		Category				tats	
Ser	ial #			P3012	Ve	locity	ft/s	1		uracy		1.0%	1.0%	
CPL	J Firmwar	re Versio	on	3.7	Ar	Area ft^2			Dep			0.4%	2.8%	
_	tware Ver			2.30	Di	scharge	cfs			ocity		0.8%	5.0%	
Mo	unting Co	rrection		0.0%				-	Wid			0.1%	0.1%	
-									Met			1.9%		
	mmary	-	~~~		•		22		and a second second	tations		2.3%		
	raging In	τ.	30		Stations		22		The Party Name	erali		3.2%	5.8%	
	t Edge		REW		tal Width		39.600				-			
1.00	an SNR		27.4 (otal Area	5	26.000							
	n Temp		53.91		ean Depth		0.657							
DIS	ch. Equat	ION	Mid-Sec		ean Veloci		0.4776 12.417							
-					Aut Disci	large	221127	-	_				-	
-	1.0.2.1.7.3.4		and the second s			n. Iti un	5 -					-		
Me	asurem	ent Re	PSUITS											
_	Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrF	act	MeanV	Area	Flow	%Q	
_				Depth 0.000	%Dep 0.0	MeasD 0.0	Vel 0.0000	CorrF	act 1.00		Area 0.000	Flow 0.000		
St	Clock	Loc	Method		the second division of	I HAR DO NOT THE OWNER OF TAXABLE PARTY.		CorrF		MeanV 0.0000 0.3173			0 0.	
0 1 2	Clock 16:24	Loc 1.00	Method None	0.000	0.0	0.0	0.0000 0.3173 0.6873	CorrF	1.00	0.0000	0.000	0.000	0 0.0 9 2.4 4 6.9	
0 1 2 3	Clock 16:24 16:24 16:25 16:26	Loc 1.00 3.00 5.00 7.00	Method None 0.6 0.6 0.6	0.000 0.460 0.620 0.700	0.0 <i>0.6</i>	0.0 0.184 0.248 0.280	0.0000 0.3173 0.6873 0.6030	CorrF	1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030	0.000 0.920 1.240 1.050	0.000 0.291 0.852 0.633	0 0. 9 2.4 4 6. 3 5.	
0 1 2 3 4	Clock 16:24 16:24 16:25 16:26 16:27	Loc 1.00 <i>3.00</i> 5.00 7.00 8.00	Method None 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670	0.0 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268	0.0000 0.3173 0.6873 0.6030 0.6667	CorrF	1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667	0.000 0.920 1.240 1.050 0.670	0.000 0.291 0.852 0.633 0.446	0 0. 9 2.4 4 6. 3 5. 6 3.	
0 1 2 3 4 5	Clock 16:24 16:25 16:26 16:27 16:28	Loc 1.00 3.00 5.00 7.00 8.00 9.00	Method None 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.700	0.0 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387	CorrF	1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030	0.000 0.920 1.240 1.050 0.670 1.050	0.000 0.2919 0.852 0.633 0.446 0.565	0 0. 9 2.4 4 6.9 3 5. 6 3.0 8 4.	
St 0 1 2 3 4 5 6	Clock 16:24 16:25 16:26 16:27 16:28 16:30	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.670 0.700 0.550	0.0 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091	0.000 0.920 1.240 1.050 0.670 1.050 1.100	0.000 0.291 0.852 0.633 0.446 0.565 0.449	0 0.0 9 2.4 4 6.1 3 5. 6 3.1 8 4.1 9 3.1	
St 0 1 2 3 4 5 6 7	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.700 0.550 0.670	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.220 0.268	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340	0.000 0.291 0.852 0.633 0.446 0.565 0.449 0.673	0 0. 9 2.4 4 6.9 3 5. 6 3. 8 4. 9 3. 9 5.	
St 0 1 2 3 4 5 6 7 8	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.700 0.550 0.670 0.670	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.220 0.268 0.268	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340 1.340	0.000 0.291 0.852 0.633 0.446 0.565 0.449 0.673 0.777	0 0.1 9 2.4 4 6.9 3 5. 6 3.1 8 4.1 9 3.1 9 5.1 2 6.1	
St 0 1 2 3 4 5 6 7 8 9	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.700 0.550 0.670 0.670 0.670	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268 0.268 0.268	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340 1.340 1.340	0.000 0.291 0.852 0.633 0.446 0.565 0.449 0.673 0.777 1.003	0 0.1 9 2.4 4 6.5 3 5. 6 3.1 6 3.1 8 4.1 9 3.1 9 5.2 2 6.2 6 8.	
St 0 1 2 3 4 5 6 7 8 9 10	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:33	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.550 0.670 0.670 0.670 0.630	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268 0.268 0.268 0.268 0.252	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768	0.000 0.920 1.240 1.050 1.050 1.050 1.100 1.340 1.340 1.340 1.260	0.000 0.291 0.852 0.633 0.446 0.565 0.449 0.673 0.777 1.003 0.726	9 2.4 4 6.1 3 5. 6 3.4 9 3.4 9 3.4 9 3.4 9 3.4 9 3.4 9 3.4 9 3.4 9 5.4 6 8.4 6 8.4 6 5.5	
St 0 1 2 3 4 5 6 7 8 9 10 11	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.670 0.630 0.630	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268 0.268 0.268 0.268 0.268 0.252 0.328	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340 1.340 1.340 1.260 1.640	0.000 0.291 0.852 0.633 0.446 0.565 0.449 0.673 0.777 1.003 0.726 0.338	0 0. 9 2.4 4 6.9 3 5. 6 3.6 8 4. 9 3. 9 5. 2 6. 6 8. 6 8. 6 5. 4 2.	
St 0 1 2 3 4 5 6 7 8 9 10 11 12	Clock 16:24 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:33 16:36 16:37 16:38	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.670 0.630 0.820 0.520	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.220 0.268 0.268 0.268 0.268 0.268 0.268 0.252 0.328 0.208	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340 1.340 1.340 1.340 1.260 1.640 1.040	0.000 0.291 0.852 0.633 0.446 0.565 0.449 0.673 0.777 1.003 0.776 0.338 0.203	0 0. 9 2.4 4 6. 3 5. 6 3. 6 3. 8 4. 9 3. 9 5. 2 6. 6 8. 6 8. 6 5. 4 2. 0 1.	
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.670 0.630 0.820 0.820 0.520 0.600	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.220 0.268 0.268 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.208 0.208 0.208	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628	CorrF	$\begin{array}{c} 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ \end{array}$	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628	0.000 0.920 1.240 1.050 1.050 1.050 1.100 1.340 1.340 1.340 1.340 1.260 1.640 1.040 1.200	0.000 0.291 0.852 0.633 0.446 0.565 0.449 0.673 0.777 1.003 0.776 0.338 0.726 0.338 0.203 0.315	0 0.0 9 2.4 4 6.1 3 5. 6 3.1 8 4. 9 3. 9 5. 2 6. 6 8. 6 8. 6 5. 4 2. 0 1. 4 2.1	
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40 16:41	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.670 0.630 0.820 0.520 0.6600 0.680	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.268 0.220 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.208 0.220 0.222	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337	0.000 0.920 1.240 1.050 1.050 1.050 1.100 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360	0.000 0.291: 0.852 0.633 0.446 0.565 0.449 0.673 0.777 1.003 0.776 0.338 0.203 0.315 0.453	0 0.0 9 2.4 4 6.1 3 5. 6 3.1 8 4. 9 3. 9 5. 2 6. 6 8. 6 8. 6 5. 4 2. 0 1. 4 2.1 9 3.1	
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 15 15 15 15 15 15 15 15 15	Clock 16:24 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40 16:41 16:42	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00 29.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.630 0.820 0.820 0.520 0.660 0.520 0.660 0.520	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.268 0.268 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.220 0.328 0.208 0.222 0.328 0.208 0.240 0.227 0.388	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092	0.000 0.920 1.240 1.050 1.050 1.050 1.100 1.340 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360 1.940	0.000 0.291: 0.852 0.633 0.446 0.565 0.449 0.673 0.777 1.003 0.776 0.338 0.203 0.315 0.453 0.988	0 0.0 9 2.4 4 6.3 3 5. 6 3.6 8 4.1 9 3.1 9 5. 2 6. 6 8. 4 2. 0 1. 4 2. 9 3.2 9 5.2 9 3.2 9 3.2 9 5.2 9 3.2 9 3.2 9 5.2 9 3.2 9 5.2 9 5.5 9 5.5 9 5.5 9 5.5 9 5.5 9 5.5 9 5.5 9 5.5 9 5.5 9	
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40 16:41 16:42 16:43	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00 29.00 31.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.630 0.820 0.820 0.520 0.660 0.520 0.660 0.520 0.660 0.520	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.268 0.220 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.220 0.222 0.328 0.208 0.222 0.328 0.208 0.222 0.328 0.208 0.240 0.222 0.328 0.208 0.240 0.252 0.328 0.208 0.252 0.328 0.208 0.252 0.328 0.208 0.252 0.328 0.268 0.252 0.258 0.258 0.258 0.268 0.252 0.328 0.258 0.258 0.252 0.328 0.258 0.258 0.258 0.252 0.328 0.2572 0.388 0.420	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984	0.000 0.920 1.240 1.050 1.050 1.050 1.100 1.340 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360 1.940 2.100	0.000 0.291: 0.852 0.633 0.446 0.565 0.449 0.673 0.777 1.003 0.776 0.338 0.203 0.315 0.453 0.988 1.046	0 0.0 9 2.4 4 6.5 3 5. 6 3.6 8 4.6 9 3.5 9 5.5 2 6. 8 4.9 9 3.5 2 6. 6 8. 6 5.5 4 2. 0 1. 4 2. 9 3.5 9 3.5 9 5.5 9	
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	Clock 16:24 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40 16:41 16:42 16:44	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00 29.00 31.00 33.00	Method None 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.670 0.630 0.820 0.520 0.660 0.520 0.660 0.520 0.660 0.520 0.520 0.600 0.520 0.520 0.520 0.520 0.520 0.520 0.520 0.670 0.620 0.670 0.620 0.620 0.620 0.620 0.620 0.620 0.520 0.620 0.520 0.620 0.520 0.620 0.520 0.620 0.520 0.620 0.520 0.690 0.520 0.690 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.90000 0.90000 0.90000 0.90000 0.90000 0.90000 0.90000000000	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.268 0.268 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.220 0.328 0.208 0.222 0.328 0.208 0.240 0.222 0.388 0.208 0.240 0.268 0.252 0.355 0.268 0.255 0.268 0.255 0.255 0.268 0.255 0.255 0.255 0.258 0.255 0.258 0.252 0.328 0.258 0.258 0.258 0.252 0.328 0.2588 0.2588 0.2588 0.2588 0.2588 0.2588 0.2588 0.2588 0.2	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984 0.6644	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984 0.6644	0.000 0.920 1.240 1.050 1.050 1.050 1.100 1.340 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360 1.940 2.100 1.800	0.000 0.291: 0.852 0.633 0.446 0.565 0.449 0.673 0.777 1.003 0.776 0.338 0.203 0.315 0.453 0.988 1.046 1.195	0 0.0 9 2.4 4 6.3 3 5. 6 3.6 8 4. 9 3.5 9 5. 2 6. 6 8. 6 5. 2 6. 6 8. 6 5. 4 2. 0 1. 4 2. 9 3. 9 3. 9 5. 2 6. 8 4. 8 4. 8 9. 8 9. 8 9. 8 9. 8 9. 8 9. 8 1. 9 2.4 9 3.5 1. 9 5. 1. 9 5. 2. 6. 8 4. 9 5. 1. 9 5. 1. 9 5. 1. 9 5. 1. 9 5. 1. 9 5. 1. 9 5. 1. 9 5. 2. 6. 8. 8. 9 5. 1. 9 5. 1. 9 5. 2. 6. 8. 8. 9 5. 1. 9 5. 2. 6. 8. 8. 9 5. 1. 9 5. 2. 6. 8. 8. 9 5. 1. 9 5. 2. 6. 8. 8. 9 5. 1. 9 5. 2. 6. 8. 8. 9 5. 2. 9 5. 2. 8. 9 5. 2. 9 5. 2. 8. 8. 8. 9 5. 9 5. 9 5. 9 5. 9 5. 9 5. 9 5. 9 5	
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	Clock 16:24 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:33 16:36 16:37 16:38 16:40 16:41 16:42 16:43 16:44 16:45	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00 29.00 31.00 33.00 35.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.670 0.630 0.820 0.620 0.680 0.520 0.660 0.520 0.660 0.970 1.050 0.900 0.800	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.268 0.268 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.220 0.328 0.208 0.222 0.328 0.208 0.240 0.222 0.328 0.208 0.240 0.238 0.208 0.252 0.328 0.268 0.252 0.328 0.328 0.420 0.328 0.420 0.328 0.420 0.320 0.320 0.328 0.420 0.32	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984 0.6644 0.5066	CorrF	1.00 <i>1.00</i> 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984 0.6644 0.5066	0.000 0.920 1.240 1.050 1.050 1.050 1.000 1.340 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360 1.940 2.100 1.800 1.600	0.000 0.291: 0.852 0.633 0.446 0.565 0.449 0.673 0.777 1.003 0.776 0.338 0.203 0.315 0.453 0.988 1.046 1.195 0.810	0 0.0 9 2.4 4 6.5 3 5. 6 3.6 8 4.1 9 3.5 9 5.5 2 6.8 8 4.1 9 3.2 6 8. 6 5.5 4 2. 0 1.1 4 2.1 9 3.2 9 3	
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	Clock 16:24 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40 16:41 16:42 16:44	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00 29.00 31.00 33.00	Method None 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.670 0.630 0.820 0.520 0.660 0.520 0.660 0.520 0.660 0.520 0.520 0.600 0.520 0.520 0.520 0.520 0.520 0.520 0.520 0.670 0.620 0.670 0.620 0.620 0.620 0.620 0.620 0.620 0.520 0.620 0.520 0.620 0.520 0.620 0.520 0.620 0.520 0.620 0.520 0.690 0.520 0.690 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.9000 0.90000 0.90000 0.90000 0.90000 0.90000 0.90000 0.90000000000	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.268 0.268 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.220 0.328 0.208 0.222 0.328 0.208 0.240 0.222 0.388 0.208 0.240 0.268 0.252 0.355 0.268 0.255 0.268 0.255 0.255 0.268 0.255 0.255 0.255 0.258 0.255 0.258 0.252 0.328 0.258 0.258 0.258 0.252 0.328 0.2588 0.2588 0.2588 0.2588 0.2588 0.2588 0.2588 0.2588 0.2	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984 0.6644	CorrF	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984 0.6644	0.000 0.920 1.240 1.050 1.050 1.050 1.100 1.340 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360 1.940 2.100 1.800	0.000 0.291: 0.852 0.633 0.446 0.565 0.449 0.673 0.777 1.003 0.776 0.338 0.203 0.315 0.453 0.988 1.046 1.195	0 0.0 9 2.4 4 6.3 3 5. 6 3.6 8 4.1 9 3.5 9 5.5 2 6. 8 4.9 9 3.1 9 5.5 2 6. 6 8. 6 5.5 4 2. 0 1.1 4 2.1 9 3.2 9 5.5 9 3.5 9 5.5 9 3.5 9 5.5 9 3.5 9 5.5 9 3.5 9 5.5 9 5.5	



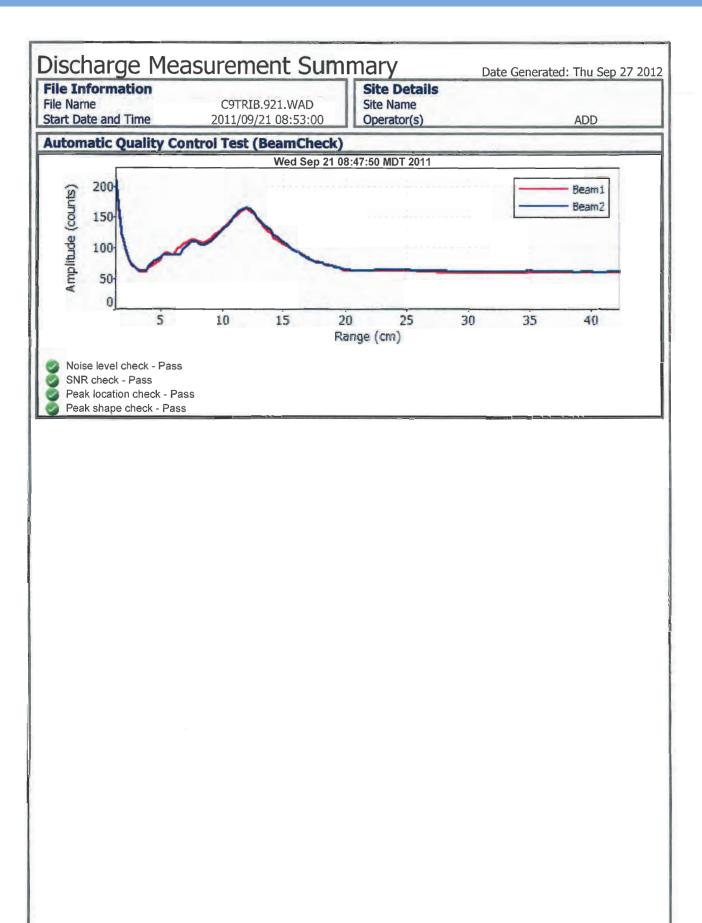
File Information		Mary Site Details	Date Generated: Thu Sep 27 20
File Name	C9US.920.WAD	Site Name	
Start Date and Time	2011/09/21 16:24:08	Operator(s)	TCN
Quality Control			
St Loc %Dep		Message	
1 3.00	0.6 High standard error: 0.031	ricourge	
13 25.00	0.6 High angle: -26		
14 27.00 20 39.00	0.6 High angle: -23 0.6 SNR (57.0) is different from ty	nicol CND (27.4)	
20 39.00	0.0 SNR (57.0) is different from ty	pical SNR (27.4)	



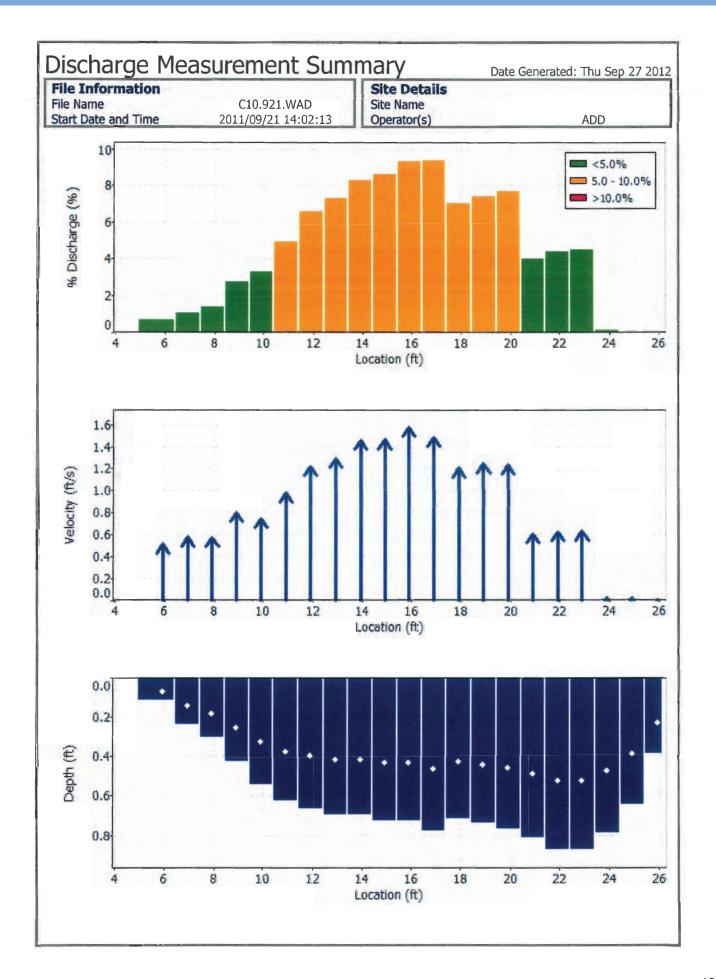
File	e Name art Date				RIB.921.\ 09/21 08		Site I Site Na Operat				ADD			
S	stem 1	nform	nation			Units (English Units)			Discharge Uncertainty					
	nsor Typ			FlowT	racker	Distance		ft	Categor	the sub-	ISO	Stats		
	rial #			P35		Velocity		t/s	Accuracy		1.0%	1.0%		
CPU Firmware Version		rsion			Area		^2	Depth		3.1%	21.8%			
Software Ver				2.3	30	Discharge	(fs	Velocity	-	14.0%	200.6%		
Mounting Correction			ion	0.0)%	Section 2 and a section of the			Width		1.0%	1.0%		
-		1 1 1 1 1 1 1 1							Method		15.4%			
	Immar								# Stations		5.1%			
	eraging	Int.		30	# Statio		10	-	Overall		21.7%	201.8%		
	art Edge			REW	Total W		4.4		Overall		21.7 70	201.07		
Mean SNR			20	38.3 dB Total A			2.609							
	Mean Temp													
Me	an Tem		37	02 °F	Mean De	epth	0.5	93						
Me			37		Mean De Mean Ve	epth		93 021						
Me Dis	an Temp sch. Equa	ation ment	37 Mid- Results	.02 °F Section	Mean Do Mean Ve Total D	epth elocity Pischarge	0.5 -0.0 -0.0	93 021 054	Monut	Area	Flow	1 %0		
Me Dis Me	an Temp sch. Equa easure Clock	ment Loc	37. Mid- Results Method	.02 °F Section Depth	Mean Do Mean Ve Total D	epth elocity Discharge MeasD	0.5 -0.0 -0.0	93 021 054 CorrFact	MeanV	Area	Flow	%Q		
Me Dis Me St	easure Clock 08:52	ment Loc 4.20	37. Mid- Results Method None	02 °F Section Depth 0 0.000	Mean Do Mean Ve Total D %Dep 0.0	epth elocity Discharge MeasD 0.0	0.5 -0.0 -0.0	93 021 054 CorrFact 1.0	0.0000	0.000	0.000	0 0.		
Me Dis Me St 0 1	easure Clock 08:52 08:56	ment Loc 4.20 4.80	37 Mid- Results Method None 0.6	02 °F Section Depth 0.000 0.400	Mean Do Mean Ve Total D %Dep 0.0 0.0 0.6	epth elocity bischarge MeasD 0.0 0.160	0.5 -0.00 -0.0 Vel 0.0000 -0.0013	93 021 054 CorrFact 1.0 1.0	0 0.0000 7 -0.0013	0.000	0.000	00 0. 13 5.		
Me Dis Me St	easure Clock 08:52	ment Loc 4.20 4.80 5.30	37. Mid- Results Method None	02 °F Section Depth 0.000 0.400 0.840	Mean Do Mean Vo Total D %Dep 0.0 0.6 0.6	MeasD 0.0 0.160 0.336	0.5 -0.00 -0.00 Vel 0.0000 -0.0013 -0.0026	93 021 054 CorrFact 1.0 1.0 1.0	0 0.0000 7 -0.0013 7 -0.0026	0.000 0.220 0.420	0.000	00 0. 3 5. 1 20.		
Me Dis Me St 0 1 2	easure Clock 08:52 08:56 08:59	ment Loc 4.20 4.80	37 Mid- Results Method None 0.6 0.6	02 °F Section Depth 0.000 0.400	Mean Do Mean Ve Total D %Dep 0.0 0.0 0.6	epth elocity bischarge MeasD 0.0 0.160	0.5 -0.00 -0.0 Vel 0.0000 -0.0013	93 021 054 CorrFact 1.0 1.0	0 0.0000 7 -0.0013 7 -0.0026 0 0.0007	0.000	0.000 -0.000 -0.001	0000. 35. 120. 3-5.		
Me Dis Me St 0 1 2 3	easure Clock 08:52 08:56 08:59 09:04	ment Loc 4.20 4.80 5.30 5.80	37 Mid- Results Method 0.6 0.6 0.6	02 °F Section Depth 0.000 0.400 0.840 0.920	Mean Do Mean Ve Total D %Dep 0.0 0.6 0.6 0.6	epth elocity bischarge 0.0 0.160 0.336 0.368	0.5 -0.0 -0.0 -0.00 -0.0013 -0.0026 0.0007	93 021 054 CorrFact 1.0 1.0 1.0 1.0	0 0.0000 7 -0.0013 7 -0.0026 0 0.0007 0 0.0151	0.000 0.220 0.420 0.460	0.000 -0.000 -0.001 0.000	0 0. 3 5. 1 20. 3 -5. 9 -128.		
Me Dis St 0 1 2 3 4	an Temp sch. Equa easure Clock 08:52 08:56 08:59 09:04 09:02	ment Loc 4.20 5.30 5.80 6.30	37 Mid- Results Method 0.6 0.6 0.6 0.6	02 °F Section Depth 0.000 0.400 0.840 0.920 0.920	Mean Do Mean Ve Total D %Dep 0.0 0.6 0.6 0.6 0.6	epth elocity bischarge 0.0 0.160 0.336 0.368 0.368	0.5 -0.0 -0.0 -0.00 -0.0013 -0.0026 0.0007 0.0151	93 021 054 CorrFact 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 0 -0.0013 0 -0.0026 0 0.0007 0 0.0151 0 -0.0066	0.000 0.220 0.420 0.460 0.460	0.000 -0.000 -0.001 0.000 0.000	0 0. 3 5. 1 20. 3 -5. 9 -128. 6 47.		
Me Dis St 0 1 2 3 4 5	an Temp sch. Equa easure Clock 08:52 08:55 08:59 09:04 09:02 09:06	ation ment Loc 4.20 4.80 5.30 5.80 6.30 6.80	37 Mid- Method 0.6 0.6 0.6 0.6 0.6 0.6	02 °F Section Depth 0.000 0.400 0.920 0.920 0.920 0.790	Mean Do Mean Ve Total D %Dep 0.0 0.6 0.6 0.6 0.6 0.6 0.6	epth elocity bischarge 0.0 0.160 0.336 0.368 0.368 0.316	0.5 -0.0 -0.0 0.0000 -0.0013 -0.0026 0.0007 0.0151 -0.0066	93 021 054 CorrFact 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0.0000 -0.0013 0.0007 0.0007 0.0151 0.00066 0.00266	0.000 0.220 0.420 0.460 0.460 0.395	0.000 -0.000 -0.001 0.000 0.000 -0.002	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
Me Dis St 0 1 2 3 4 5 6	an Temp sch. Equa easure Clock 08:52 08:55 08:59 09:04 09:02 09:06 09:07	ation ment Loc 4.20 4.80 5.30 5.80 6.30 6.80 7.30	37 Mid- Results Method 0.6 0.6 0.6 0.6 0.6 0.6	02 °F Section Depth 0.000 0.400 0.920 0.920 0.920 0.790 0.620	Mean Do Mean Ve Total D %Dep 0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6	epth elocity bischarge 0.0 0.160 0.336 0.368 0.368 0.368 0.316 0.248	0.5 -0.0 -0.0 -0.000 -0.0013 -0.0026 0.0007 0.0151 -0.0066 -0.0266	93 021 054 CorrFact 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0.0000 -0.0013 0.0007 0.0007 0.0151 0.00066 0.0266 0.0007	0.000 0.220 0.420 0.460 0.460 0.395 0.310	0.000 -0.000 -0.001 0.000 -0.002 -0.002 -0.008	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		



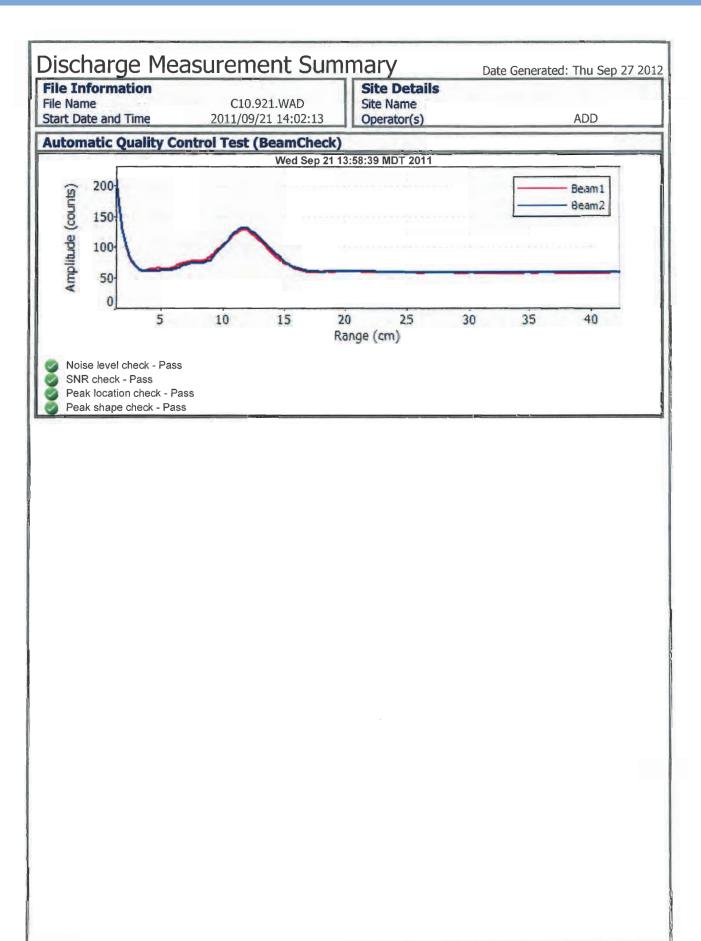
File Information File Name Start Date and Time			C9TRIB.921.WAD 2011/09/21 08:53:00				
Qua	ality Co	ontrol					
St	Loc	%Dep	and the state of the	Message			
1	4.80	0.6	High differences in beam SNR: 25.7	,43.8			
2	5.30	0.6	High differences in beam SNR: 29.6	,42.1			
6	7.30		High angle: -158	1/			
7	7.80	0.6	Boundary QC is Fair; possible boun	dary interference			
8	8.30	0.6	High differences in beam SNR: 33. Boundary QC is Good; possible bou	5,44.7			



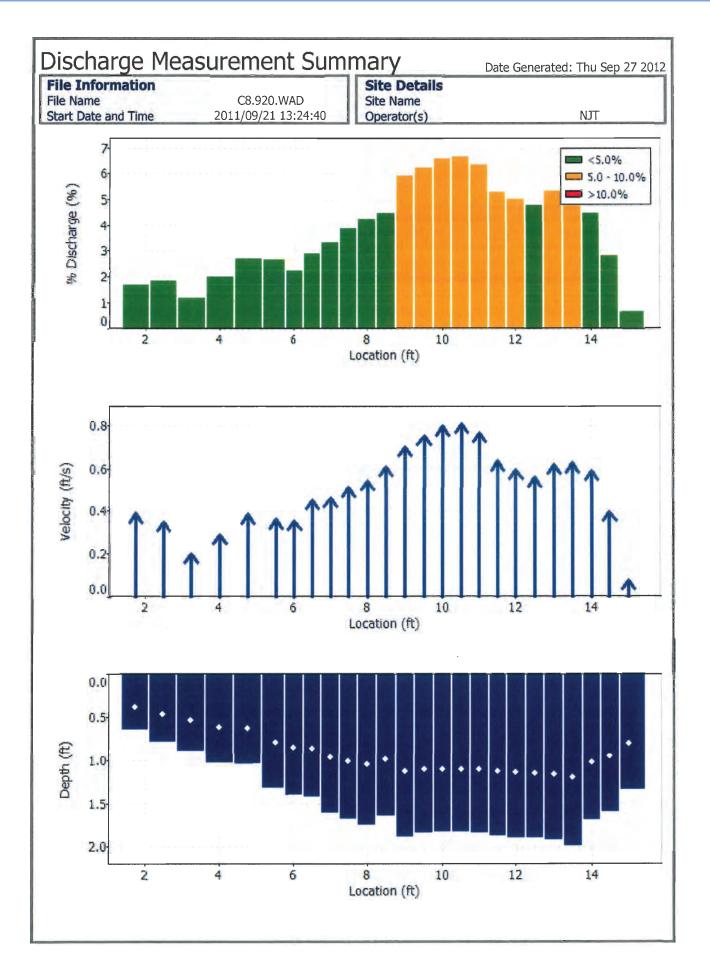
File	Name t Date an	00.0254			21 14:02:	13	Site Deta Site Name Operator(s				A	DD	
Sys	stem In	format	tion		U	nits	(English Ur	nits)	Discharge Uncertainty				
Sen	sor Type			lowTracl	ker Di	stance	ft			Category			Stats
	al #			P3532	Ve	elocity	ft/s			iracy			1.09
CPU	Firmwar	re Versio	n	3.7		ea	ft^2	1	Dept			0.4%	0.99
Soft	ware Ver	r .		2.30	Di	scharge	cfs		Velo			0.7%	3.39
Mou	nting Correction 0.0%					Widt			0.1%	0.10			
-			Service and Service and				-		Meth			2.0%	0.1
	mmary								No. of Concession, Name	ations		2.2%	
	veraging Int. 30 # Stat						23		The second second	and the second se	the second se		
				tal Width		22.400		Ove	rali		3.2%	3.59	
	IN SNR		29.1 c		tal Area		13.173						
	n Temp		52.44		ean Depth		0.588						
Disc	h. Equat	ion	Mid-Sec	tion M	ean Veloc	ity	0.9355						
1.1				Т	tal Disc	harge	12.3241						
	Clock	Loc	Mathad	Douth	04 Den	Monch	Vol	ComEr	-	Mannill	Auon	Elaw	04.0
St 0	14:02	Loc 3.90	Method None	Depth 0.000	%Dep 0.0	MeasD 0.0	Vel 0.0000	CorrFa	1.00	MeanV 0.0000	Area 0.000	Flow 0.00	
0	14:02 14:02	3.90 5.90	None 0.6	0.000	0.0 0.6	0.0	0.0000	CorrFa		0.0000	0.000	0.00	00 0 31 0
0 1 2	14:02 14:02 14:03	3.90 5.90 6.90	None 0.6 0.6	0.000 0.120 0.240	0.0 0.6 0.6	0.0 0.048 0.096	0.0000 0.5167 0.5804	CorrFa	1.00 1.00 1.00	0.0000 0.5167 0.5804	0.000 0.180 0.240	0.00	00 0 31 0 94 1
0 1 2 3	14:02 14:02 14:03 14:04	3.90 5.90 6.90 7.90	None 0.6 0.6 0.6	0.000 0.120 0.240 0.310	0.0 0.6 0.6 0.6	0.0 0.048 0.096 0.124	0.0000 0.5167 0.5804 0.5751	CorrFa	1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751	0.000 0.180 0.240 0.310	0.00 0.09 0.13 0.17	00 0 31 0 94 1 83 1
01234	14:02 14:02 14:03 14:04 14:06	3.90 5.90 6.90 7.90 8.90	None 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.430	0.0 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.172	0.0000 0.5167 0.5804 0.5751 0.8048	CorrFa	1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048	0.000 0.180 0.240 0.310 0.430	0.00 0.09 0.13 0.17 0.34	00 0 31 0 94 1 83 1 62 2
0 1 2 3 4 5	14:02 14:02 14:03 14:04 14:06 14:07	3.90 5.90 6.90 7.90 8.90 9.90	None 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.430 0.550	0.0 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.172 0.220	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490	0.000 0.180 0.240 0.310 0.430 0.550	0.00 0.09 0.13 0.17 0.34 0.41	00 0 31 0 94 1 83 1 62 2 19 3
0 1 2 3 4 5 6	14:02 14:02 14:03 14:04 14:06 14:07 14:08	3.90 5.90 6.90 7.90 8.90 9.90 10.90	None 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.430 0.550 0.630	0.0 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.172 0.220 0.252	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833	0.000 0.180 0.240 0.310 0.430 0.550 0.630	0.00 0.09 0.13 0.17 0.34 0.41 0.61	00 0 31 0 94 1 83 1 62 2 19 3 94 5
01234567	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09	3.90 5.90 6.90 7.90 8.90 9.90 10.90 11.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.430 0.550 0.630 0.670	0.0 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.172 0.220 0.252 0.268	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228	0.000 0.180 0.240 0.310 0.430 0.550 0.630 0.670	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6
012345678	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10	3.90 5.90 6.90 7.90 8.90 9.90 10.90 11.90 12.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.430 0.550 0.630 0.670 0.700	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.172 0.220 0.252 0.268 0.280	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982	0.000 0.180 0.240 0.310 0.430 0.550 0.630 0.670 0.700	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.61 0.81 0.90	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7
0123456789	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11	3.90 5.90 6.90 7.90 8.90 9.90 10.90 11.90 12.90 13.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.430 0.550 0.630 0.670 0.700 0.700	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.220 0.252 0.268 0.280 0.280	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646	0.000 0.180 0.240 0.310 0.430 0.550 0.630 0.670 0.700 0.700	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 8
0 1 2 3 4 5 6 7 8 9 10	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11 14:13	3.90 5.90 6.90 7.90 8.90 9.90 10.90 11.90 12.90 13.90 14.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.430 0.550 0.630 0.670 0.700 0.700 0.700 0.730	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.220 0.252 0.268 0.280 0.280 0.280 0.292	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659	0.000 0.180 0.240 0.310 0.430 0.550 0.630 0.670 0.700 0.700 0.700 0.730	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02 1.07	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 8 01 8
0 1 2 3 4 5 6 7 8 9 10 11	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11 14:13 14:14	3.90 5.90 6.90 7.90 8.90 10.90 11.90 12.90 13.90 14.90 15.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.430 0.550 0.630 0.670 0.700 0.700 0.700 0.730	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.220 0.252 0.268 0.280 0.280 0.280 0.292 0.292	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814	0.000 0.180 0.240 0.310 0.430 0.550 0.630 0.670 0.700 0.700 0.730 0.730	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02 1.07 1.15	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 8 01 8 44 9
0 1 2 3 4 5 6 7 8 9 10 11 12	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11 14:11 14:13 14:14 14:15	3.90 5.90 6.90 7.90 8.90 10.90 11.90 12.90 13.90 14.90 15.90 16.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.550 0.630 0.670 0.700 0.700 0.700 0.730 0.730 0.730	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.220 0.252 0.268 0.280 0.280 0.280 0.292 0.292 0.292	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918	0.000 0.180 0.240 0.310 0.430 0.550 0.630 0.670 0.700 0.700 0.730 0.730 0.730	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02 1.07 1.15 1.16	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 8 01 8 44 9 34 9
0 1 2 3 4 5 6 7 7 8 9 10 11 12 13	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11 14:13 14:14 14:15 14:17	3.90 5.90 6.90 7.90 8.90 9.90 10.90 11.90 12.90 13.90 14.90 15.90 16.90 17.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.550 0.630 0.670 0.700 0.700 0.700 0.730 0.730 0.730 0.730 0.730	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.220 0.252 0.268 0.280 0.280 0.280 0.292 0.292 0.312 0.288	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106	0.000 0.180 0.240 0.310 0.430 0.550 0.630 0.670 0.700 0.700 0.730 0.730 0.780 0.720	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02 1.07 1.15 1.16 0.87	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 8 01 8 44 9 34 9 18 7
0 1 2 3 4 5 6 7 8 9 10 11 11 12 13 14	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11 14:13 14:14 14:15 14:17 14:18	3.90 5.90 6.90 7.90 8.90 9.90 10.90 11.90 12.90 13.90 14.90 15.90 16.90 17.90 18.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.550 0.630 0.670 0.700 0.700 0.730 0.730 0.730 0.730 0.730 0.720 0.740	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.220 0.252 0.268 0.280 0.280 0.292 0.292 0.292 0.312 0.288 0.296	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454	0.000 0.180 0.240 0.310 0.430 0.550 0.630 0.670 0.700 0.700 0.730 0.730 0.780 0.720 0.740	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02 1.07 1.15 1.16 0.87 0.92	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 8 01 8 44 9 34 9 18 7 18 7
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11 14:13 14:14 14:15 14:17 14:18 14:19	3.90 5.90 6.90 7.90 8.90 9.90 10.90 11.90 12.90 13.90 14.90 15.90 16.90 17.90 18.90 19.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.550 0.630 0.670 0.700 0.700 0.730 0.730 0.730 0.730 0.730 0.720 0.740	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.220 0.252 0.268 0.280 0.280 0.292 0.292 0.292 0.312 0.288 0.296 0.308	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385	0.000 0.180 0.240 0.310 0.550 0.630 0.630 0.700 0.700 0.730 0.730 0.780 0.720 0.740 0.770	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02 1.07 1.15 1.16 0.87 0.92 0.95	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 8 01 8 44 9 34 9 18 7 18 7 37 7
0 1 2 3 4 5 5 6 7 7 8 9 10 11 12 13 14 15 16	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11 14:13 14:14 14:15 14:17 14:18 14:19 14:30	3.90 5.90 6.90 7.90 8.90 10.90 11.90 12.90 13.90 14.90 15.90 16.90 17.90 18.90 19.90 20.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.550 0.630 0.670 0.700 0.700 0.730 0.730 0.730 0.730 0.730 0.720 0.740 0.770 0.770	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.220 0.252 0.268 0.280 0.280 0.292 0.292 0.292 0.312 0.288 0.296 0.308 0.328	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385 0.6099	CorrFa	1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385 0.6099	0.000 0.180 0.240 0.310 0.550 0.630 0.630 0.700 0.700 0.700 0.730 0.730 0.730 0.720 0.740 0.770 0.820	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02 1.07 1.15 1.16 0.87 0.92 0.95 0.50	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 8 01 8 44 9 34 9 18 7 7 7 01 4
0 1 2 3 4 5 5 6 7 7 8 9 10 11 12 13 14 15 16 <i>17</i>	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11 14:13 14:14 14:15 14:17 14:18 14:19 14:30 14:33	3.90 5.90 6.90 7.90 8.90 10.90 11.90 12.90 13.90 14.90 15.90 16.90 17.90 18.90 19.90 20.90 21.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.550 0.630 0.670 0.700 0.700 0.730 0.730 0.730 0.730 0.730 0.730 0.740 0.770 0.740 0.770 0.820 0.880	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.220 0.252 0.268 0.280 0.280 0.292 0.292 0.292 0.312 0.288 0.296 0.308	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385 0.6099 0.6273	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.57511 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385 0.6099 0.6273	0.000 0.180 0.240 0.310 0.550 0.630 0.700 0.700 0.700 0.730 0.730 0.730 0.780 0.720 0.740 0.770 0.820 0.880	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02 1.07 1.15 1.16 0.87 0.92 0.95 0.50 0.55	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 8 01 8 44 9 34 9 18 7 18 7 37 7 01 4 20 4
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 <i>17</i> 18	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11 14:13 14:14 14:15 14:17 14:18 14:19 14:30	3.90 5.90 6.90 7.90 8.90 10.90 11.90 12.90 13.90 14.90 15.90 16.90 17.90 18.90 19.90 20.90 21.90 22.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.550 0.630 0.670 0.700 0.700 0.730 0.730 0.730 0.730 0.730 0.730 0.740 0.770 0.820 0.880 0.880	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.220 0.252 0.268 0.280 0.280 0.292 0.292 0.292 0.312 0.288 0.296 0.308 0.328 0.328 0.328	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385 0.6099 0.6273 0.6355	CorrFa	1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385 0.6099 0.6273 0.6355	0.000 0.180 0.240 0.310 0.430 0.550 0.630 0.700 0.700 0.700 0.730 0.730 0.730 0.780 0.720 0.740 0.770 0.820 0.880 0.880	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02 1.07 1.15 1.16 0.87 0.92 0.95 0.55 0.55	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 8 01 8 44 9 34 9 18 7 7 7 01 4 20 4 92 4
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 <i>17</i> 18	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11 14:13 14:14 14:15 14:17 14:18 14:19 14:30 14:33 14:34	3.90 5.90 6.90 7.90 8.90 10.90 11.90 12.90 13.90 14.90 15.90 16.90 17.90 18.90 19.90 20.90 21.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.550 0.630 0.670 0.700 0.700 0.730 0.730 0.730 0.730 0.730 0.730 0.740 0.770 0.740 0.770 0.820 0.880	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.220 0.252 0.268 0.280 0.280 0.292 0.292 0.292 0.312 0.288 0.296 0.308 0.328 0.328	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385 0.6099 0.6273	CorrFa	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.5167 0.5804 0.57511 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385 0.6099 0.6273	0.000 0.180 0.240 0.310 0.550 0.630 0.700 0.700 0.700 0.730 0.730 0.730 0.780 0.720 0.740 0.770 0.820 0.880	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02 1.07 1.15 1.16 0.87 0.92 0.95 0.50 0.55	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 88 01 8 44 9 34 9 18 7 7 7 01 4 20 4 13 0
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	14:02 14:02 14:03 14:04 14:06 14:07 14:08 14:09 14:10 14:11 14:13 14:14 14:15 14:17 14:18 14:19 14:30 14:33 14:34 14:36	3.90 5.90 6.90 7.90 8.90 10.90 11.90 12.90 13.90 14.90 15.90 16.90 17.90 18.90 19.90 20.90 21.90 22.90 23.90	None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.120 0.240 0.310 0.550 0.630 0.670 0.700 0.700 0.730 0.730 0.730 0.730 0.730 0.730 0.740 0.770 0.820 0.880 0.880 0.880 0.880	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.048 0.096 0.124 0.172 0.220 0.252 0.268 0.280 0.280 0.292 0.292 0.312 0.288 0.296 0.308 0.328 0.328 0.328 0.352 0.352	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385 0.6099 0.6273 0.6355 0.0269	CorrFa	1.00 1.00	0.0000 0.5167 0.5804 0.5751 0.8048 0.7490 0.9833 1.2228 1.2982 1.4646 1.4659 1.5814 1.4918 1.2106 1.2454 1.2385 0.6099 0.6273 0.6355 0.0269	0.000 0.180 0.240 0.310 0.550 0.630 0.700 0.700 0.700 0.730 0.730 0.730 0.730 0.730 0.730 0.720 0.740 0.770 0.820 0.880 0.880 0.880 0.790	0.00 0.09 0.13 0.17 0.34 0.41 0.61 0.81 0.90 1.02 1.07 1.15 1.16 0.87 0.92 0.95 0.55 0.55 0.02	00 0 31 0 94 1 83 1 62 2 19 3 94 5 92 6 89 7 54 88 01 8 44 9 34 9 18 7 7 01 4 20 40 41.3 0.334 0.2



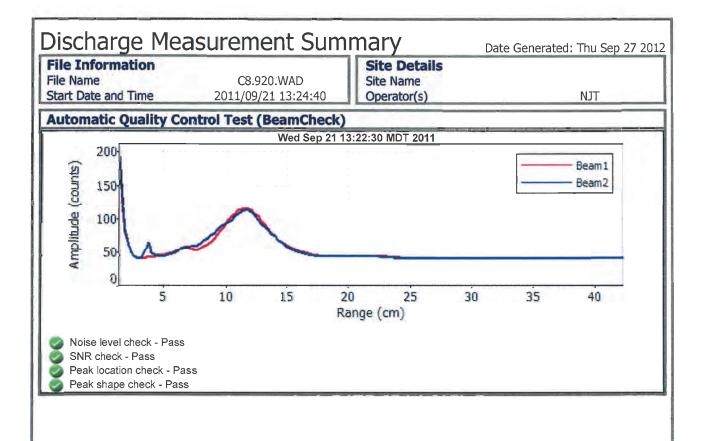
Dis	charg	je Mea	asurement Sum	imary	Date Generated: Thu Sep 27 2012
File N	Informa Name Date and		C10.921.WAD 2011/09/21 14:02:13	Site Details Site Name Operator(s)	ADD
Qua	lity Con	trol			
St	Loc	%Dep		Message	
17	21.90	0.6	High standard error: 0.033		
19	23.90	0.6	High angle: -60		
20	24.90	0.6	High angle: -47		
		0.6	SNR (43.2) is different from typic	cal SNR (29.1)	1
		0.6	High SNR variation during measu	Irement: 7.3,7.7	
21	25.90	0.6	Boundary QC is Fair; possible bo	undary interference	



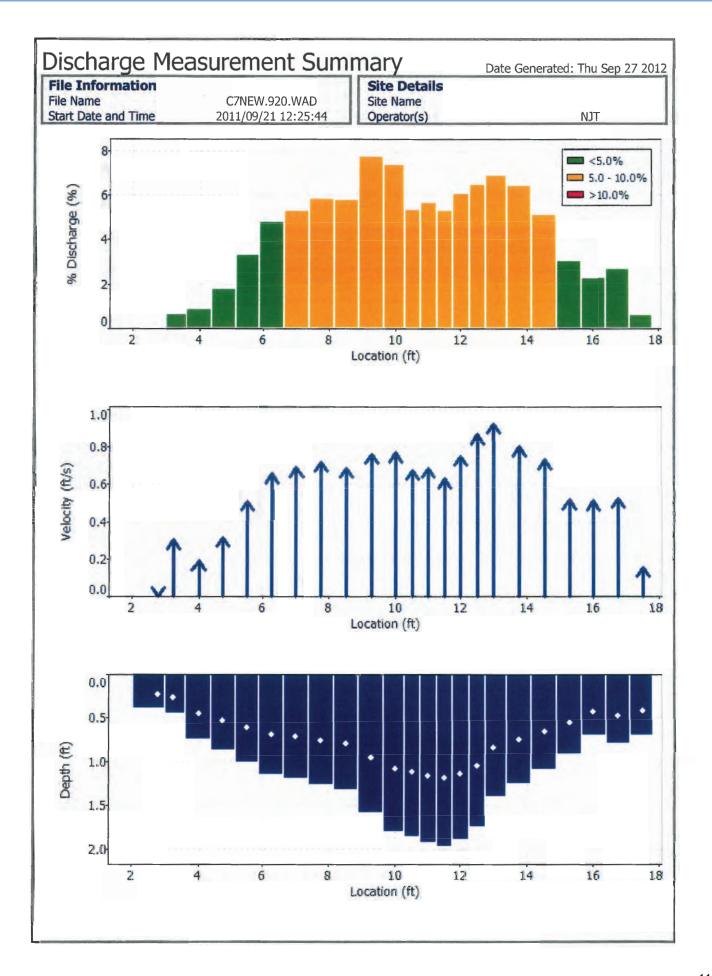
File	Name t Date an				20.WAD 21 13:24:	40	Site Detail Site Name Operator(s)	s		Ν	TCI		
Sys	tem In	formati	ion		U	nits	(English Unit	s) D	Discharge Uncertainty				
	sor Type			lowTrack	ker Di	stance	ft		Category		and the second se	Stats	
	al #			P3012	B	Velocity ft/s		A	ccuracy		1.0%	1.09	
		re Version	1	3.7		Area ft^2			epth	0.1%		0.8	
Soft	ware Ver	r .		2.30			Discharge cfs				0.1%		
	nting Co			0.0%					elocity /idth		0.1%	1.4	
-								-	ethod		1.6%	0.1	
	Summary							Same "	Stations		1.9%		
	veraging Int. 30 # Stat				Stations		27	A DOMESTIC	and the second se			1.00	
Start Edge R			REW		tal Width		14.900		verall		2.8%	1.99	
	n SNR		26.8 d		tal Area		20.964						
	n Temp		52.66		ean Depth		1.407						
Disc	h. Equat	ion	Mid-Sec		ean Veloci		0.5302						
				Тс	tal Discl	harge	11.1156						
-												-	
Mea	asurem	ent Res	sults				-						
St	Clock	Loc	Method	Depth	%Dep	MeasD	Vel C	orrFact	MeanV	Area	Flow	9/00	
0	13:24	1.00	None	0.000	0.0	0.0	0.0000	1.0	0.0000	0.000	0.000	0 0	
1	13:24	1.75	0.6	0.650	0.6	0.260	0.3921	1.0	0 0.3921	0.487	0.191		
2	13:26	2.50	0.6	0.790	0.6	0.316		1.0		0.593	0.208		
3	13:27	3.25	0.6	0.900	0.6	0.360		1.0		0.675	0.136		
4	13:28	4.00	0.6	1.040	0.6	0.416	0.2910	1.0	0 0.2910	0.780	0.227		
5	12.20											0 2	
	13:30	4.75	0.6	1.050	0.6	0.420		1.0		0.787	0.304		
6	13:31	5.50	0.6	1.330	0.6	0.532	0.3622	1.0	0 0.3622	0.831	0.301	1 2	
67	13:31 13:32	5.50	0.6 0.6	1.330 1.410	0.6 0.6	0.532	0.3622	1.0	0 0.3622	0.831	0.301	1 2 2	
6 7 8	13:31 13:32 13:34	5.50 6.00 6.50	0.6 0.6 0.6	1.330 1.410 1.430	0.6 0.6 0.6	0.532 0.564 0.572	0.3622 0.3563 0.4544	1.0 1.0 1.0	0 0.3622 0 0.3563 0 0.4544	0.831 0.705 0.715	0.301 0.251 0.324	1 2 2 2 9 2	
6 7 8 9	13:31 13:32 13:34 13:35	5.50 6.00 6.50 7.00	0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610	0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644	0.3622 0.3563 0.4544 0.4656	1.0 1.0 1.0 1.0	0 0.3622 0 0.3563 0 0.4544 0 0.4656	0.831 0.705 0.715 0.805	0.301 0.251 0.324 0.374	1 2 2 2 9 2 7 3	
6 7 8 9 10	13:31 13:32 13:34 13:35 13:36	5.50 6.00 6.50 7.00 7.50	0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690	0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676	0.3622 0.3563 0.4544 0.4656 0.5144	1.0 1.0 1.0 1.0 1.0	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144	0.831 0.705 0.715 0.805 0.845	0.301 0.251 0.324 0.374 0.374	1 2 2 2 9 2 7 3 7 3	
6 7 8 9 10 11	13:31 13:32 13:34 13:35 13:36 13:37	5.50 6.00 6.50 7.00 7.50 8.00	0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750	0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700	0.3622 0.3563 0.4544 0.4656 0.5144 0.5440	1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440	0.831 0.705 0.715 0.805 0.845 0.875	0.301 0.251 0.324 0.374 0.434 0.434	1 2 2 2 9 2 7 3 7 3 0 4	
6 7 8 9 10 11 12	13:31 13:32 13:34 13:35 13:36 13:37 13:38	5.50 6.00 6.50 7.00 7.50 8.00 8.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750 1.650	0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.660	0.3622 0.3563 0.4544 0.4656 0.5144 0.5440 0.6096	1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096	0.831 0.705 0.715 0.805 0.845 0.875 0.875	0.301 0.251 0.324 0.374 0.434 0.436 0.476	1 2 2 2 9 2 7 3 7 3 7 3 0 4 9 4	
6 7 9 10 11 12 13	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39	5.50 6.00 6.50 7.00 7.50 8.00 8.50 9.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750 1.650 1.890	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.660 0.756	0.3622 0.3563 0.4544 0.4656 0.5144 0.5440 0.6096 0.7044	$ \begin{array}{r} 1.0 \\ $	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044	0.831 0.705 0.715 0.805 0.845 0.875 0.825 0.825 0.945	0.301 0.251 0.324 0.374 0.434 0.434 0.476 0.502 0.665	1 2 2 2 9 2 7 3 7 3 7 3 7 3 0 4 9 4 7 6	
6 7 9 10 11 12 13 14	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39 13:41	5.50 6.00 6.50 7.00 7.50 8.00 8.50 9.00 9.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750 1.650 1.890 1.850	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.660 0.756 0.740	0.3622 0.3563 0.4544 0.4656 0.5144 0.5440 0.6096 0.7044 0.7549	$ \begin{array}{r} 1.0 \\ $	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044 0 0.7549	0.831 0.705 0.719 0.805 0.845 0.875 0.825 0.825 0.945 0.925	0.301 0.251 0.324 0.374 0.434 0.476 0.502 0.665 0.698	1 2 2 2 9 2 7 3 7 3 7 3 7 3 0 4 9 4 7 6 3 6	
6 7 9 10 11 12 13 14 15	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39 13:41 13:42	5.50 6.00 7.00 7.50 8.00 8.50 9.00 9.50 10.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750 1.650 1.890 1.850 1.840	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.660 0.756 0.740 0.736	0.3622 0.3563 0.4544 0.4656 0.5144 0.5440 0.6096 0.7044 0.7549 0.8018	$ \begin{array}{r} 1.0 \\ 1$	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044 0 0.7549 0 0.8018	0.831 0.705 0.715 0.805 0.845 0.875 0.825 0.925 0.945 0.925 0.920	0.301 0.251 0.324 0.374 0.434 0.476 0.502 0.665 0.698 0.737	1 2 2 2 9 2 7 3 7 3 7 3 7 3 7 3 7 3 7 3 7 3 7 3 7 3	
6 7 9 10 11 12 13 14 15 16	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39 13:41 13:42 13:43	5.50 6.00 7.00 7.50 8.00 8.50 9.00 9.50 10.00 10.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750 1.650 1.890 1.850 1.840 1.840	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.660 0.756 0.740 0.736 0.736	0.3622 0.3563 0.4544 0.4656 0.5144 0.5440 0.6096 0.7044 0.7549 0.8018 0.8123	$ \begin{array}{r} 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\$	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044 0 0.7549 0 0.8018 0 0.8123	0.831 0.705 0.715 0.805 0.845 0.875 0.825 0.945 0.925 0.920 0.920	0.301 0.251 0.324 0.374 0.434 0.476 0.502 0.665 0.698 0.737 0.747	1 2 2 2 9 2 7 3 7 3 7 3 7 3 7 3 7 3 7 3 7 3 7 3 7 3	
6 7 9 10 11 12 13 14 15 16 17	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39 13:41 13:42 13:43 13:44	5.50 6.00 6.50 7.00 7.50 8.00 8.50 9.00 9.50 10.00 10.50 11.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750 1.650 1.890 1.850 1.840 1.840 1.840	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.660 0.756 0.740 0.736 0.736 0.736	0.3622 0.3563 0.4544 0.4656 0.5144 0.5440 0.6096 0.7044 0.7549 0.8018 0.8123 0.7707	$ \begin{array}{r} 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\$	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044 0 0.7549 0 0.8018 0 0.8123 0 0.7707	0.831 0.705 0.715 0.805 0.845 0.875 0.825 0.945 0.925 0.920 0.920 0.925	0.301 0.251 0.324 0.434 0.476 0.502 0.665 0.698 0.737 0.747 0.712	1 2 2 2 9 2 7 3 0 4 9 4 7 6 3 6 6 6 9 6	
6 7 8 9 10 11 12 13 14 15 16 17 18	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39 13:41 13:42 13:43 13:44 13:46	5.50 6.00 6.50 7.00 7.50 8.00 8.50 9.00 9.50 10.00 10.50 11.00 11.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750 1.650 1.890 1.850 1.840 1.840 1.840 1.850 1.880	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.660 0.756 0.740 0.736 0.736 0.740 0.752	0.3622 0.3563 0.4544 0.4656 0.5144 0.5440 0.6096 0.7044 0.7549 0.8018 0.8123 0.7707 0.6352	$\begin{array}{r} 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\$	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044 0 0.7549 0 0.8018 0 0.8123 0 0.7707 0 0.6352	0.831 0.705 0.715 0.805 0.845 0.875 0.825 0.945 0.925 0.920 0.920 0.920 0.925 0.940	0.301 0.251 0.324 0.434 0.476 0.502 0.665 0.698 0.737 0.747 0.747 0.712	1 2 2 2 9 2 7 3 0 4 9 4 7 6 3 6 6 6 9 6 3 6 9 6 9 6	
6 7 9 10 11 12 13 14 15 16 17 18 19	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39 13:41 13:42 13:43 13:44 13:46 13:47	5.50 6.00 6.50 7.00 7.50 8.00 8.50 9.00 9.50 10.00 10.50 11.00 11.50 12.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750 1.650 1.890 1.850 1.840 1.840 1.840 1.850 1.880 1.880 1.900	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.660 0.756 0.740 0.736 0.740 0.752 0.760	0.3622 0.3563 0.4544 0.4656 0.5144 0.5440 0.6096 0.7044 0.7549 0.8018 0.8123 0.7707 0.6352 0.5955	$\begin{array}{c} 1.0 \\$	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044 0 0.7549 0 0.8018 0 0.8123 0 0.7707 0 0.6352 0 0.5955	0.831 0.705 0.715 0.805 0.845 0.875 0.825 0.945 0.925 0.920 0.920 0.920 0.925 0.940 0.950	0.301 0.251 0.324 0.434 0.434 0.476 0.502 0.665 0.698 0.737 0.747 0.747 0.712 0.597 0.565	1 2 2 2 9 2 7 3 7 3 6 6 3 6 6 6 3 6 9 6 3 6 6 6 7 5	
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39 13:41 13:42 13:43 13:44 13:46 13:47 13:48	5.50 6.00 6.50 7.00 7.50 8.00 8.50 9.00 9.50 10.00 10.50 11.00 11.50 12.00 12.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750 1.650 1.890 1.850 1.840 1.840 1.840 1.840 1.840 1.840 1.840 1.840 1.900 1.910	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.660 0.756 0.740 0.736 0.736 0.740 0.752 0.760 0.764	0.3622 0.3563 0.4544 0.4656 0.5144 0.5440 0.6096 0.7044 0.7549 0.8018 0.8123 0.7707 0.6352 0.5955 0.5620	$\begin{array}{c} 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\$	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044 0 0.7549 0 0.8018 0 0.8123 0 0.7707 0 0.6352 0 0.5955 0 0.5620	0.831 0.705 0.715 0.805 0.845 0.875 0.825 0.945 0.925 0.920 0.920 0.920 0.925 0.940 0.955	0.301 0.251 0.324 0.434 0.434 0.476 0.502 0.665 0.698 0.737 0.747 0.712 0.597 0.565 0.536	1 2 2 2 9 2 9 2 7 3 0 4 9 4 7 6 6 6 6 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 7	
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39 13:41 13:42 13:43 13:44 13:46 13:47 13:48 13:49	5.50 6.00 6.50 7.00 7.50 8.00 8.50 9.00 9.50 10.00 10.50 11.00 11.50 11.00 11.50 12.00 12.50 13.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750 1.650 1.890 1.850 1.840 1.840 1.840 1.850 1.840 1.850 1.880 1.900 1.910	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.766 0.736 0.736 0.736 0.740 0.752 0.760 0.764 0.772	0.3622 0.3563 0.4544 0.5144 0.5144 0.5440 0.7044 0.7549 0.8018 0.8123 0.7707 0.6352 0.5955 0.5620 0.6204	$\begin{array}{c} 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\$	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044 0 0.7549 0 0.8018 0 0.8123 0 0.7707 0 0.6352 0 0.5955 0 0.5620 0 0.6204	0.831 0.705 0.715 0.805 0.845 0.875 0.825 0.945 0.920 0.920 0.920 0.920 0.920 0.925 0.940 0.955 0.955 0.965	0.301 0.251 0.324 0.434 0.434 0.476 0.502 0.665 0.698 0.737 0.747 0.747 0.712 0.597 0.565 0.536 0.598	1 2 2 2 9 2 9 2 7 3 0 4 9 4 7 6 3 6 6 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 7 10 5	
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39 13:41 13:42 13:43 13:44 13:46 13:47 13:48 13:49 13:50	5.50 6.00 6.50 7.00 7.50 8.00 9.00 9.50 10.00 10.50 11.00 11.50 11.00 11.50 12.00 12.50 13.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.650 1.890 1.850 1.840 1.840 1.840 1.840 1.840 1.840 1.840 1.900 1.910 1.910 2.000	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.766 0.740 0.736 0.740 0.736 0.740 0.752 0.760 0.764 0.772 0.800	0.3622 0.3563 0.4544 0.5144 0.5144 0.5440 0.7044 0.7549 0.8018 0.8123 0.7707 0.6352 0.5955 0.5620 0.6204 0.6263	$\begin{array}{c} 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\$	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044 0 0.7549 0 0.8018 0 0.8123 0 0.7707 0 0.6352 0 0.5955 0 0.5620 0 0.6263	0.831 0.705 0.805 0.845 0.875 0.825 0.945 0.925 0.920 0.920 0.920 0.920 0.920 0.925 0.940 0.955 0.940 0.955 0.965 1.000	0.301 0.251 0.324 0.434 0.434 0.476 0.502 0.665 0.698 0.737 0.747 0.712 0.597 0.565 0.536 0.536 0.598 0.626	1 2 2 2 9 2 7 3 0 4 9 4 9 4 9 4 9 6 6 6 3 6 6 6 9 6 7 5 7 5 3 5	
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39 13:41 13:42 13:42 13:43 13:44 13:46 13:47 13:48 13:49 13:50 <i>13:52</i>	5.50 6.00 6.50 7.00 7.50 8.00 9.00 9.50 10.00 10.50 11.00 11.50 11.00 11.50 12.00 12.50 13.00 13.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.750 1.650 1.890 1.850 1.840 1.840 1.840 1.840 1.840 1.840 1.840 1.900 1.910 1.930 2.000 1.700	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.766 0.740 0.736 0.740 0.736 0.740 0.752 0.760 0.764 0.772 0.800 0.680	0.3622 0.3563 0.4544 0.5144 0.5144 0.5440 0.7044 0.7549 0.8018 0.8123 0.7707 0.6352 0.5955 0.5620 0.6204 0.6263 0.5919	$\begin{array}{c} 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\$	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044 0 0.7549 0 0.8018 0 0.8123 0 0.7707 0 0.6352 0 0.5955 0 0.5620 0 0.6263 0 0.6263 0 0.5919	0.831 0.705 0.715 0.805 0.845 0.875 0.825 0.945 0.925 0.920 0.920 0.920 0.920 0.920 0.925 0.940 0.955 0.940 0.955 0.965 1.000 0.850	0.301 0.251 0.324 0.434 0.434 0.476 0.502 0.665 0.698 0.737 0.747 0.712 0.597 0.565 0.536 0.536 0.598 0.626 0.593	1 2 2 2 2 2 2 9 2 3 7 3 3 7 3 3 7 3 3 7 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 7 5 7 5 7 4 7 5 7 5 7 4 7 5 7 3 3 5 7 4 4 7 7 5 7 5 7 4 7 5 7 7 7 7 7 5 7 7 7 7 7 5 7 7 7 7 7 7 5 7 7 7 7 7 7 7 7 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	13:31 13:32 13:34 13:35 13:36 13:37 13:38 13:39 13:41 13:42 13:43 13:44 13:46 13:47 13:48 13:49 13:50	5.50 6.00 6.50 7.00 7.50 8.00 9.00 9.50 10.00 10.50 11.00 11.50 11.00 11.50 12.00 12.50 13.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.330 1.410 1.430 1.610 1.690 1.650 1.890 1.850 1.840 1.840 1.840 1.840 1.840 1.840 1.840 1.900 1.910 1.910 2.000	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.532 0.564 0.572 0.644 0.676 0.700 0.766 0.740 0.736 0.740 0.736 0.740 0.752 0.760 0.764 0.772 0.800	0.3622 0.3563 0.4544 0.5144 0.5144 0.5440 0.7044 0.7549 0.8018 0.8123 0.7707 0.6352 0.5955 0.5620 0.6204 0.6263 0.5919 0.3980	$\begin{array}{c} 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\$	0 0.3622 0 0.3563 0 0.4544 0 0.4656 0 0.5144 0 0.5440 0 0.6096 0 0.7044 0 0.7549 0 0.8018 0 0.8123 0 0.7707 0 0.6352 0 0.5955 0 0.5620 0 0.6263 0 0.6263 0 0.5919 0 0.3980	0.831 0.705 0.715 0.805 0.845 0.875 0.825 0.945 0.920 0.920 0.920 0.920 0.920 0.920 0.925 0.940 0.955 0.940 0.955 0.965 1.000	0.301 0.251 0.324 0.434 0.434 0.476 0.502 0.665 0.698 0.737 0.747 0.712 0.597 0.565 0.536 0.536 0.598 0.626	1 2 2 2 2 2 9 2 2 9 2 2 7 3 3 7 3 3 6 6 6 6 6 6 6 6 6 6 6 5 7 5 7 7 5 7 7 5 3 7 5 3 7 5 7 7 5 7 7 5 7	



Dis	charg	ge Me	asurement Sum	imary	Date Generated: Thu Sep 27 2012
File N	Information Name Date and		C8.920.WAD 2011/09/21 13:24:40	Site Details Site Name Operator(s)	NJT
Qua	lity Con	trol			
St	Loc	%Dep		Message	
23	14.00		High angle: -27 High standard error: 0.031		
24	14.50		High standard error: 0.030		
25	15.00	0.6	High angle: -23 Boundary QC is Poor; possible bo	oundary interference	

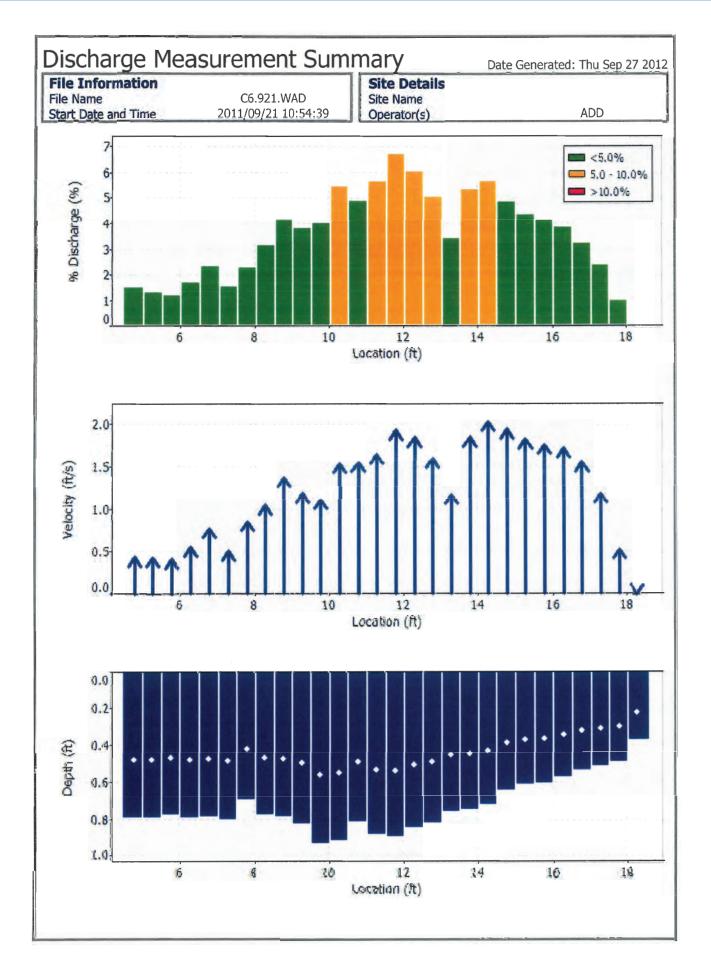


File	Name Name The Date a				W.920.WA 9/21 12:2		Site De Site Nam Operator	e			1	TUN		
Sy	stem In	nforma	tion			Units	(English L	Units)	Discharge Uncertainty					
	sor Type			FlowTra	cker	Distance	ft			Category	statement of the local division in which the local division in which the local division is not the local division of the local division in the local divis	statement of the local division in which the local division in which the local division in which the local division is not the local division in the local	Stats	
Ser	ial #			P301	2	/elocity	ft/s		Acc	Accuracy		1.0%	1.09	
CPL	J Firmwa	re Versi	on	3.7	14	Area	ft^2	2	De			0.1%	1.09	
Sof	tware Ve	r		2.30		Discharge	cfs			ocity		0.9%	2.49	
Mounting Correction			1	0.0%	6				Wi			0.1%	0.19	
_						Sector and	WARRAND COD	PRIATE -		thod		1.8%		
	mmary					-		And in case of the local division in which the local division in which the local division in the local divisio	Stations		2.0%			
	veraging Int. 30 # S						25			and the second se		3.0%	2.8%	
	rt Edge		RE		Total Widt		16.800		00	erall		3.0%	2.0%	
	an SNR			30.7 dB Total A 51.13 °F Mean I			18.312							
	in Temp						1.090							
Disc	ch. Equat	tion	Mid-Se		lean Velo		0.6398							
_	_				Total Dis	charge	11.716	54						
St	Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrFa	_	MeanV	Area	Flow	%	
0	12:25	1.30	None		0.0		0.0000		1.00	0.0000	0.000	0.000		
1	12:25	2.80	0.6	0.400	0,6	0.160	-0.0013		1.00	-0.0013	0.390	-0.000	_	
2	12:27	3.25	0.6	0.450	0.6		0.3058		1.00	0.3058	0.270	0.082		
2													9 0	
3			0.6		0.6	0.300	0.1936		1.00	0.1936	0.563	0.108		
4	12:30	4.75	0.6	0.880	0.6	0.352	0.3189		1.00	0.3189	0.660	0.210	5 1.	
4	12:30 12:31	4.75 5.50	0.6 0.6	0.880	0.6 0.6	0.352 0.408	0.3189 0.5125		1.00 1.00	0.3189 0.5125	0.660	0.210	5 1. 0 3.	
4 5 6	12:30 12:31 12:32	4.75 5.50 6.25	0.6 0.6 0.6	0.880 1.020 1.150	0.6 0.6 0.6	0.352 0.408 0.460	0.3189 0.5125 0.6575		1.00 1.00 1.00	0.3189 0.5125 0.6575	0.660 0.765 0.862	0.210 0.392 0.567	5 1. 0 3. 0 4.	
4 5 6 7	12:30 12:31 12:32 12:33	4.75 5.50 6.25 7.00	0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200	0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.480	0.3189 0.5125 0.6575 0.6909		1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909	0.660 0.765 0.862 0.900	0.210 0.392 0.567 0.621	5 1. 0 3. 0 4 9 5	
4 5 6 7 8	12:30 12:31 12:32 12:33 12:33	4.75 5.50 6.25 7.00 7.75	0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270	0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.480 0.508	0.3189 0.5125 0.6575 0.6909 0.7208		1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208	0.660 0.765 0.862 0.900 0.953	0.210 0.392 0.567 0.621 0.686	5 1. 0 3. 0 4 9 5 6 5.	
4 5 6 7	12:30 12:31 12:32 12:33	4.75 5.50 6.25 7.00	0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200	0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.480	0.3189 0.5125 0.6575 0.6909		1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909	0.660 0.765 0.862 0.900	0.210 0.392 0.567 0.621	5 1. 0 3. 0 4. 9 5. 6 5. 1 5.	
4 5 6 7 8 9 10	12:30 12:31 12:32 12:33 12:34 12:36	4.75 5.50 6.25 7.00 7.75 8.50	0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270 1.320	0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.480 0.508 0.528	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880		1.00 1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880	0.660 0.765 0.862 0.900 0.953 0.990	0.210 0.392 0.567 0.621 0.686 0.681	5 1. 0 3. 0 4 9 5 6 5. 1 5. 0 7.	
4 5 6 7 8 9 10 11	12:30 12:31 12:32 12:33 12:34 12:36 12:37	4.75 5.50 6.25 7.00 7.75 8.50 9.25	0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270 1.320 1.590	0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.480 0.508 0.528 0.636	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631		1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631	0.660 0.765 0.862 0.900 0.953 0.990 1.192	0.210 0.392 0.567 0.621 0.686 0.681 0.910	5 1. 0 3. 0 4 9 5 6 5. 1 5. 0 7. 8 7 3 5.	
4 5 6 7 8 9 10 11 12 13	12:30 12:31 12:32 12:33 12:34 12:36 12:37 12:38 12:40 12:44	4.75 5.50 6.25 7.00 7.75 8.50 9.25 10.00 10.50 11.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270 1.320 1.590 1.800 1.860 1.930	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.508 0.528 0.636 0.720 0.744 0.772	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890		1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723	0.660 0.765 0.862 0.900 0.953 0.990 1.192 1.125 0.930 0.965	0.210 0.392 0.567 0.621 0.686 0.681 0.910 0.868 0.630 0.664	5 1. 0 3. 0 4 9 5 6 5. 1 5. 0 7. 8 7 3 5. 9 5.	
4 5 6 7 8 9 10 11 12 13 14	12:30 12:31 12:32 12:33 12:34 12:36 12:37 12:38 12:40 12:44 12:47	4.75 5.50 6.25 7.00 7.75 8.50 9.25 10.00 10.50 11.00 11.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270 1.320 1.590 1.800 1.860 1.930 1.980	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.508 0.528 0.636 0.720 0.744 0.772 0.792	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322	0.660 0.765 0.862 0.900 0.953 0.990 1.192 1.125 0.930 0.965 0.990	0.210 0.392 0.567 0.621 0.686 0.681 0.910 0.868 0.630 0.664 0.625	5 1. 0 3. 0 4 9 5 6 5. 1 5. 0 7. 8 7 3 5. 9 5. 9 5. 9 5.	
4 5 6 7 8 9 10 11 12 13 14 15	12:30 12:31 12:32 12:33 12:34 12:36 12:37 12:38 12:40 12:44 12:47 12:52	4.75 5.50 6.25 7.00 7.75 8.50 9.25 10.00 10.50 11.00 11.50 12.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270 1.320 1.590 1.800 1.860 1.930 1.980 1.900	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.508 0.528 0.636 0.720 0.744 0.772 0.792 0.760	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536	0.660 0.765 0.862 0.900 0.953 0.990 1.192 1.125 0.930 0.965 0.990 0.950	0.210 0.392 0.567 0.621 0.686 0.681 0.910 0.868 0.630 0.664 0.625 0.715	5 1. 0 3. 0 4 9 5 6 5. 1 5. 0 7. 8 7 3 5. 9 5. 9 5. 9 5. 9 5.	
4 5 6 7 8 9 10 11 12 13 14 15 16	12:30 12:31 12:32 12:33 12:34 12:36 12:37 12:38 12:40 12:44 12:47 12:52 12:55	4.75 5.50 6.25 7.00 7.75 8.50 9.25 10.00 10.50 11.00 11.50 12.00 12.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270 1.320 1.590 1.800 1.860 1.930 1.980 1.900 1.750	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.508 0.528 0.636 0.720 0.744 0.772 0.792 0.760 0.700	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684	0.660 0.765 0.862 0.900 0.953 0.990 1.192 1.125 0.930 0.965 0.990 0.950 0.875	0.210 0.392 0.567 0.621 0.686 0.681 0.910 0.868 0.630 0.664 0.625 0.715 0.759	5 1. 0 3. 0 4 9 5 6 5. 1 5. 0 7. 8 7 3 5. 9 5	
4 5 6 7 8 9 10 11 12 13 14 15 16 17	12:30 12:31 12:32 12:33 12:34 12:36 12:37 12:38 12:40 12:44 12:47 12:52 12:55 12:55	4.75 5.50 6.25 7.00 7.75 8.50 9.25 10.00 10.50 11.00 11.50 12.00 12.50 13.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270 1.320 1.590 1.800 1.860 1.930 1.980 1.980 1.900 1.750 1.400	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.508 0.528 0.636 0.720 0.744 0.772 0.792 0.760 0.700 0.560	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239	0.660 0.765 0.862 0.900 0.953 0.990 1.192 1.125 0.930 0.965 0.990 0.950 0.875 0.875	0.210 0.392 0.567 0.621 0.686 0.681 0.910 0.868 0.630 0.664 0.625 0.715 0.759 0.808	5 1. 0 3. 0 4 9 5 6 5. 1 5. 0 7. 8 7 3 5. 9 5. 9 5. 9 5. 9 5. 9 6. 9 6. 9 6. 4 6	
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	12:30 12:31 12:32 12:33 12:34 12:36 12:37 12:38 12:40 12:44 12:47 12:52 12:55 12:55 12:55 12:57	4.75 5.50 6.25 7.00 7.75 8.50 9.25 10.00 10.50 11.00 11.50 12.00 12.50 13.00 13.75	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270 1.320 1.590 1.800 1.860 1.930 1.980 1.980 1.900 1.750 1.400 1.250	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.508 0.528 0.636 0.720 0.744 0.772 0.792 0.760 0.700 0.560 0.500	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239 0.8041		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239 0.8041	0.660 0.765 0.862 0.900 0.953 0.990 1.192 1.125 0.930 0.965 0.990 0.950 0.875 0.875 0.938	0.210 0.392 0.567 0.621 0.686 0.681 0.910 0.868 0.630 0.664 0.625 0.715 0.759 0.808 0.753	5 1. 0 3. 0 4 9 5 6 5. 1 5. 0 7. 8 7 3 5. 9 5. 9 5. 9 5. 9 5. 9 5. 9 6. 9 6. 9 6. 9 6. 9 6. 9 6. 9 6. 9 6. 9 5. 9 6. 9 5. 9 6. 9 5. 9 6. 9 6. 9 5. 9 6. 9 7. 9 7	
4 5 6 7 8 9 10 11 11 12 13 14 15 16 17 18 19	12:30 12:31 12:32 12:33 12:34 12:36 12:37 12:38 12:40 12:44 12:47 12:52 12:55 12:55 12:55 12:55 12:57 12:58 13:03	4.75 5.50 6.25 7.00 7.75 8.50 9.25 10.00 10.50 11.00 11.50 12.00 12.50 13.00 13.75 14.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270 1.320 1.590 1.800 1.860 1.930 1.980 1.980 1.900 1.750 1.400 1.250 1.100	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.508 0.528 0.636 0.720 0.744 0.772 0.792 0.760 0.700 0.560 0.500 0.440	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239 0.8041 0.7333		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239 0.8041 0.7333	0.660 0.765 0.862 0.900 0.953 0.990 1.192 1.125 0.930 0.965 0.990 0.950 0.875 0.875 0.875 0.938 0.825	0.210 0.392 0.567 0.621 0.686 0.681 0.910 0.868 0.630 0.664 0.625 0.715 0.759 0.808 0.753 0.753 0.605	5 1. 0 3. 0 4 9 5 6 5. 1 5. 0 7. 8 7 3 5. 9 5. 9 5. 9 5. 9 5. 9 5. 9 6 4 6 9 6 9 6. 9 5. 9 7. 9 5. 9 7. 9 7.	
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	12:30 12:31 12:32 12:33 12:34 12:36 12:37 12:38 12:40 12:44 12:47 12:52 12:55 12:55 12:55 12:55 12:55 12:57 12:58 13:03 13:07	4.75 5.50 6.25 7.00 7.75 8.50 9.25 10.00 10.50 11.00 11.50 12.00 12.50 13.00 13.75 14.50 15.25	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270 1.320 1.320 1.320 1.930 1.980 1.980 1.980 1.900 1.750 1.400 1.250 1.100 0.920	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.508 0.528 0.636 0.720 0.744 0.772 0.792 0.760 0.700 0.560 0.500 0.440 0.368	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239 0.8041 0.7333 0.5190		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239 0.8041 0.7333 0.5190	0.660 0.765 0.862 0.900 0.953 0.990 1.192 1.125 0.930 0.965 0.990 0.950 0.875 0.875 0.875 0.875 0.938 0.825 0.690	0.210 0.392 0.567 0.621 0.686 0.681 0.910 0.868 0.630 0.664 0.625 0.715 0.759 0.808 0.753 0.759 0.808 0.753 0.605 0.358	5 1. 0 3. 0 4. 9 5. 6 5. 1 5. 0 7. 18 7 3 5. 9 5. 9 5. 9 5. 9 6. 1 3. 1	
4 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	12:30 12:31 12:32 12:33 12:34 12:36 12:37 12:38 12:40 12:44 12:47 12:52 12:55 12:55 12:55 12:55 12:55 12:57 12:58 13:03 13:07 13:10	4.75 5.50 6.25 7.00 7.75 8.50 9.25 10.00 10.50 11.00 11.50 12.00 13.75 14.50 15.25 16.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.270 1.320 1.320 1.320 1.320 1.930 1.980 1.980 1.980 1.900 1.750 1.400 1.250 1.400 0.920 0.710	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.508 0.528 0.636 0.720 0.744 0.772 0.792 0.760 0.700 0.560 0.500 0.440 0.368 0.284	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239 0.8041 0.7333 0.5190 0.5135		1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239 0.8041 0.7333 0.5190 0.5135	0.660 0.765 0.862 0.900 0.953 0.990 1.192 1.125 0.930 0.965 0.990 0.950 0.875 0.875 0.875 0.875 0.875 0.875 0.938 0.825 0.690 0.532	0.210 0.392 0.567 0.621 0.686 0.681 0.910 0.868 0.630 0.664 0.625 0.715 0.759 0.808 0.753 0.759 0.808 0.753 0.605 0.358 0.273	5 1. 0 3. 0 4. 9 5. 6 5. 1 5. 0 7. 18 7 3 5. 9 5. 9 5. 9 6. 9 6. 9 6. 9 6. 9 6. 9 6. 9 6. 9 6. 1 3. 1 3. 1 3. 1 3. 14 2	
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	12:30 12:31 12:32 12:33 12:34 12:36 12:37 12:38 12:40 12:44 12:47 12:52 12:55 12:55 12:55 12:55 12:55 12:57 12:58 13:03 13:07	4.75 5.50 6.25 7.00 7.75 8.50 9.25 10.00 10.50 11.00 11.50 12.00 12.50 13.00 13.75 14.50 15.25	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.880 1.020 1.150 1.200 1.270 1.320 1.320 1.320 1.930 1.980 1.980 1.980 1.900 1.750 1.400 1.250 1.100 0.920	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.352 0.408 0.460 0.508 0.528 0.636 0.720 0.744 0.772 0.792 0.760 0.700 0.560 0.500 0.440 0.368	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239 0.8041 0.7333 0.5190		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.3189 0.5125 0.6575 0.6909 0.7208 0.6880 0.7631 0.7723 0.6778 0.6890 0.6322 0.7536 0.8684 0.9239 0.8041 0.7333 0.5190	0.660 0.765 0.862 0.900 0.953 0.990 1.192 1.125 0.930 0.965 0.990 0.950 0.875 0.875 0.875 0.875 0.938 0.825 0.690	0.210 0.392 0.567 0.621 0.686 0.681 0.910 0.868 0.630 0.664 0.625 0.715 0.759 0.808 0.753 0.759 0.808 0.753 0.605 0.358	5 1. 0 3. 0 4. 9 5. 6 5. 1 5. 0 7. 18 7. 3 5. 9 5. 9 5. 9 6. 9 6. 19 6. 10 5. 11 3. 12 3. 14 2. 17 2.	

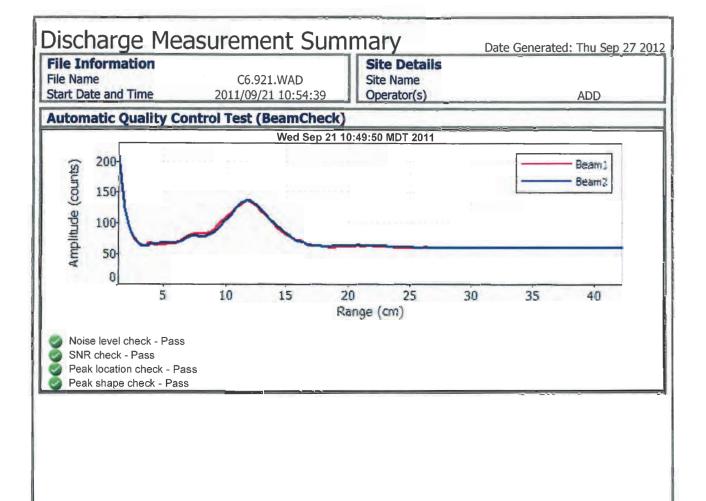


File N	Informal lame Date and 1		C7NEW.920.WAD 2011/09/21 12:25:44	Site Details Site Name Operator(s)	NJT
Qual	lity Cont	rol			
St	Loc	%Dep	n (2 n	Message	
1	2.80	0.6	SNR (55.4) is different from ty	pical SNR (30.7)	
4	4.75	0.6	High angle: -27		
5	5.50	0.6	High angle: -22		
8	7.75	0.6	High angle: -22		
9	8.50	0.6	High angle: -26		
10	9.25	0.6	High angle: -21		
12	10.50		High angle: -21		
13	11.00		High angle: -26		
14	11.50		High angle: -31		
15	12.00	0.6	High angle: -25		trans to the second sec
19	14.50	0.6	High angle: -23		
20	15.25		High angle: -28 High standard error: 0.031		
22	16.75	and the second s	High angle: -37	and a second	
23	17.50		High angle: -45		

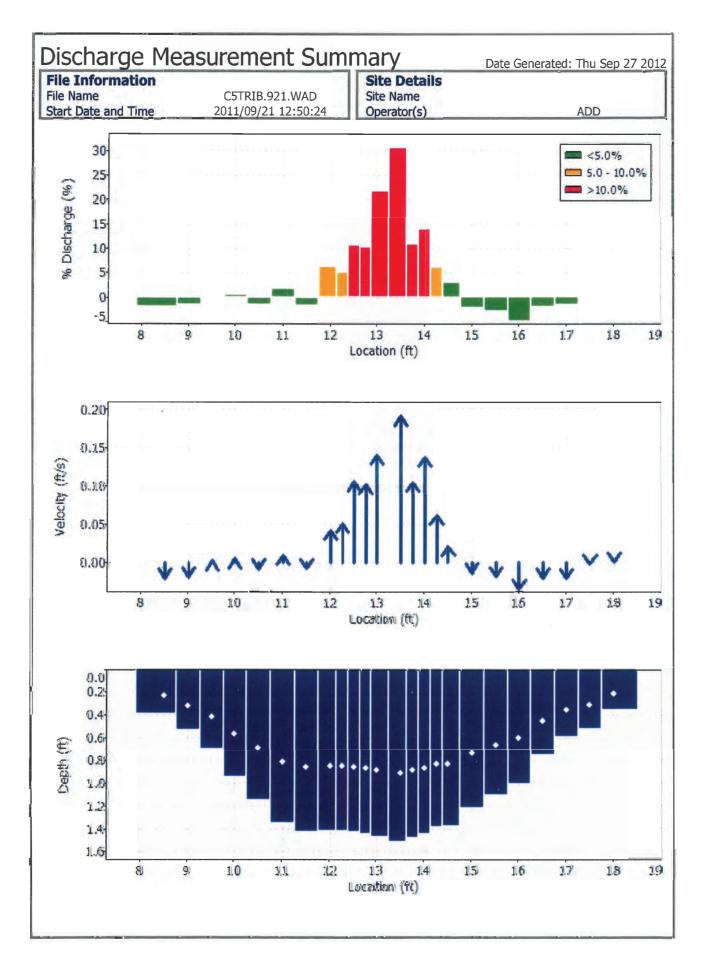
File	Name	mation and Time			921.WAD 9/21 10:54	4:39	Site Der Site Name Operator	е		ŀ	ADD			
Sys	tem II	nformatio	n			Units	(English U	inits)	Discharge Uncertainty					
	sor Type	8		FlowTrac	cker 🚺	Distance	ft		Category	I	SO S	tats		
	al #			P3532	2	/elocity	ft/s		Accuracy		1.0%	1.0%		
CPU	Firmwa	re Version	3.7			Area	ft^2		Depth		0.3%	0.9%		
	ware Ve			2.30		Discharge	cfs		/elocity		0.6%	2.39		
Mou	nting Co	orrection		0.0%	o l				Nidth		0.1%	0.19		
-							and a second	1	Method		1.6%			
	nmary		20		Chatiana		20	S Down	# Stations		1.7%			
5				# Stations		30		Overall			2.69			
	n SNR				otal Widt	1.2	14.850	in the second						
	n Temp		33.6 49.20		otal Area		10.423 0.702							
	h. Equa		49.20 Mid-Se		Aean Dep Aean Velo		1.2386							
JISC	n. Lqua	uon	mu-se		otal Dis		12.909							
					otar Dio			-						
Me	asuren	nent Res	lits			-7787								
-	Ciock		ethod	Depth	%Dep	MeasD	Vel	CorrFact	MeanV	Area	Flow	%		
0	10:54	4.15	None	0.000	0.0	0.0	0.0000	1.0		0.000	0.0000			
1	11:32	4.80	0.6	0.800	0.6		0.4367	1.0		0.460	0.2008			
2	11:38	5.30	0.6	0.800	0.6	0.320	0.4321	1.0		0.400	0.1728	1		
3	11:39	5.80	0.6	0.780	0.6	0.312	0.4134	1.0		0.390	0.1612			
4	11:40	6.30	0.6	0.800	0.6	0.320	0.5581	1.0	and the other design and the	0.400	0.2232			
5	11:42 11:45	6.80 7.30	0.6	0.790	0.6	0.316	0.7733 0.5082	1.0		0.395	0.3055			
7	11:45	7.80	0.6	0.810	0.6	0.324	0.8547	1.0		0.405	0.2050			
8	11:52	8.30	0.6	0.780	0.6	0.312	1.0535	1.0		0.390	0.4108			
9	11:53	8.80	0.6	0.790	0.6	0.316	1.3760	1.0	the subscription of the local division of th	0.395	0.5435			
10	11:54	9.30	0.6	0.830	0.6	0.332	1.1926	1.0		0.415	0.4950			
11	11:56	9.80	0.6	0.940	0.6	0.376	1.1148	1.0		0.470	0.5239			
12	11:57	10.30	0.6	0.920	0.6	0.368	1.5417	1.0		0.460	0.7091			
13	11:58	10.80	0.6	0.820	0.6	0.328	1.5509	1.0		0.410	0.6358			
14	11:59	11.30	0.6	0.890	0.6	0.356	1.6512	1.0		0.445	0.7349	5		
15	12:00	11.80	0.6	0.900	0.6	0.360	1.9357	1.0	0 1.9357	0.450	0.8710			
16	12:01	12.30	0.6	0.850	0.6	0.340	1.8497	1.0		0.425	0.7862			
17	12:02	12.80	0.6	0.820	0.6	0.328	1.6047	1.0		0.410	0.6578			
18	12:03	13.30	0.6	0.760	0.6		1.1768	1.0		0.380	0.4471			
19	12:04	13.80	0.6	0.750	0.6	0.300	1.8527	1.0		0.375	0.6948			
20	12:05	14.30	0.6	0.720	0.6	0.288	2.0348	1.0	suffrance of the local division in which the local division in the loc	0.360	0.7327			
21	12:06	14.80	0.6	0.650	0.6	0.260	1.9472	1.0		0.325	0.6328			
22	12:07	15.30	0.6	0.620	0.6	0.248	1.8278	1.0		0.310	0.5667			
23 24	12:08 12:09	15.80	0.6	0.610	0.6	0.244	1.7664	1.0		0.305	0.5387	_		
25	12:09	16.30 16.80	0.6	0.580	0.6	0.232	1.7247	1.0	and the survey of the survey o	0.290	0.5002			
26	12:10	17.30	0.6	0.540	0.6	0.210	1.1837	1.0		0.260	0.3078			
	12:12	17.80	0.6	0.520	0.6	0.200	0.5292	1.0		0.250	0.1323			
			0.0	0.000	0.0	0.200	the second division in	Tor	U.JEJE	0.2.00	ULULU			
27 28	12:12	18.30	0.6	0.380	0.6	0.152	-0.0007	1.0	0 -0.0007	0.228	-0.0001	0.		



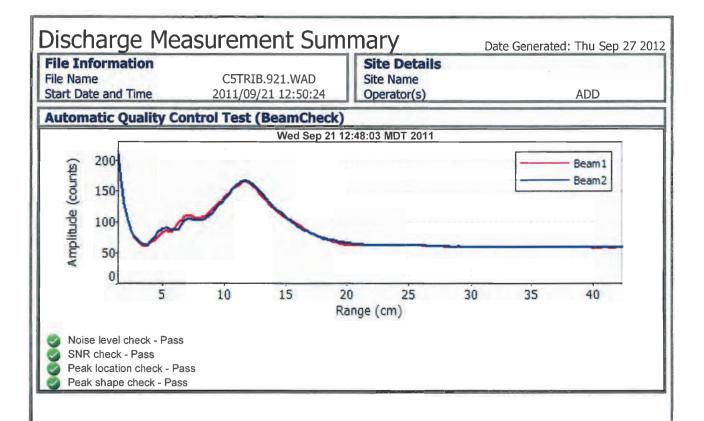
ischarge Me		Site Details	Date Generated: Thu Sep 27 2
ile Name	C6.921.WAD	Site Name	
tart Date and Time	2011/09/21 10:54:39	Operator(s)	ADD
uality Control			
t Loc %Dep		Message	
28 18.30 0	6 SNR (61.9) is different from ty	pical SNR (33.6)	Percel of the man
0	6 High SNR variation during mea	surement: 6.9,6.5	



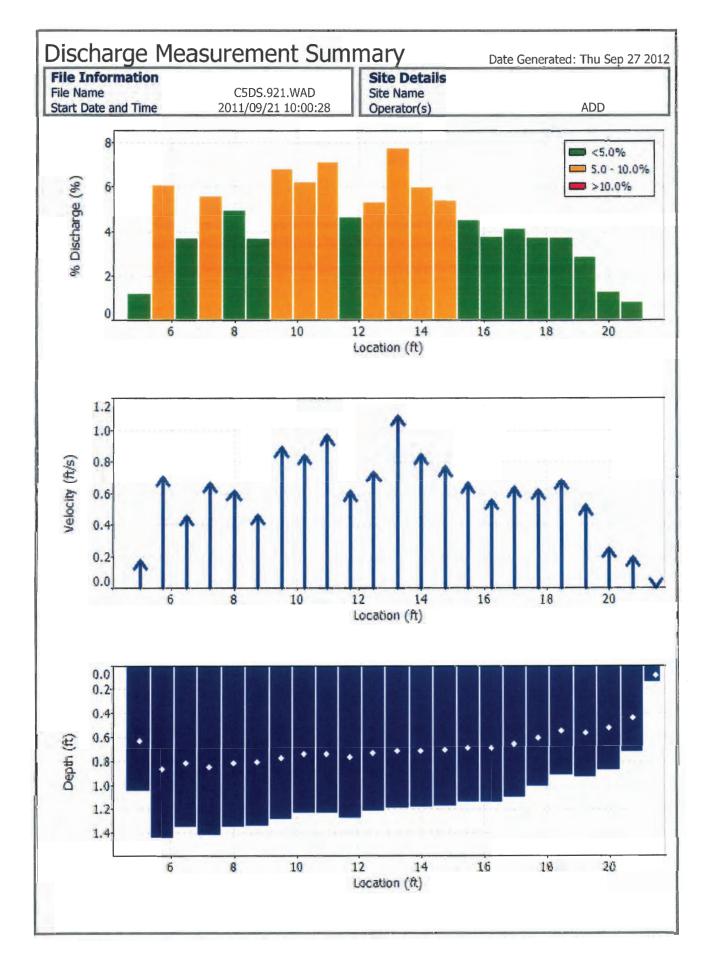
File	e Infor Name rt Date a				(B.921.W/ 9/21 12:5		Site De Site Nam Operator	ne				ADD		
Sy	stem In	nforma	ation			Units	(English	Units)	Discharge Uncertainty					
	sor Type			FlowTra	cker 🔢	Distance	ft		-	Category		the second s	tats	
	ial #			P3532		Velocity ft/s		5	Ac	curacy		1.0%	1.09	
CPL	J Firmwa	re Versi	ion	3.7		Area	ft^2		_	pth		0.2%	0.9	
Sof	tware Ve	r		2.30		Discharge cfs			in the second second	locity		2.2%	14.5	
Mo	unting Co	prrection	1	0.0%						idth		0.2%	0.2	
-			and the second s	-				1	lines and	ethod		3.4%		
	mmary					- 21			Stations	and the reason of the local division of the	2.0%			
	Averaging Int. 30 # Stat						26		and and a second	/erall	and the second se	No. of Concession, Name	14.5	
					Total Wid		11.70							
	ean SNR 36.4 dB Total Are						10.57							
	an Temp		55.71 Mid Co		Mean Dep		0.904							
DIS	ch. Equa	tion	Mid-Se		Mean Velo		0.033							
_					Fotal Dis	charge	0.357	4						
						pana) para	-	-						
	asuren	other Designation of the local division of t	No. of Concession, Name of Street, or other	Denth I	AL Day	Marco I	14-1 1	ComEn	the T	Manual		E 1	010	
0	12:50	Loc 7.30	Method None	Depth 0.000	%Dep 0.0	MeasD 0.0	Vel 0.0000	CorrFa	1.00	MeanV 0.0000	Area 0.000	Flow 0.0000	%0	
1	12:50	8.50	0.6		successive statements when it is not start of				1.00	0.0000		0.0000	ι U	
		0.50			10	0 150	-0.0210		00	-0.0210	1 2221	.0 0070	. 1	
1	12.52		the second se	0.390	0.6	0.156	-0.0210	the survey of the local division in which the local division is not the local division of the local division is not the local division of the local divisi	1.00	-0.0210	0.332	-0.0070		
23	12:52 12:54	9.00	0.6	0.530	0.6	0.212	-0.0197	1	1.00	-0.0197	0.265	-0.0052	-1	
3	12:54	<i>9.00</i> 9.50	0.6 0.6	0.530 0.700	<i>0.6</i> 0.6	0.212 0.280	<i>-0.019.</i> 7 0.0020		1.00	- <i>0,0197</i> 0.0020	0.265 0.350	- <i>0.0052</i> 0.0007	-1	
3	12:54 12:55	9.00 9.50 10.00	0.6 0.6 0.6	0.530 0.700 0.950	0.6 0.6 0.6	0.212 0.280 0.380	-0.0197 0.0020 0.0049		1.00	<i>-0,0197</i> 0.0020 0.0049	0.265 0.350 0.475	- <i>0.0052</i> 0.0007 0.0023	-1	
3 4 5	12:54	9.00 9.50 10.00 10.50	0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150	0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460	-0.0197 0.0020 0.0049 -0.0092		1.00	- <i>0,0197</i> 0.0020	0.265 0.350	- <i>0.0052</i> 0.0007	- <u>1</u> ((-1	
3	12:54 12:55 <i>12:56</i>	9.00 9.50 10.00	0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.350	0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540	-0.0197 0.0020 0.0049 -0.0092 0.0095		1.00 1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092	0.265 0.350 0.475 0.575 0.675	-0.0052 0.0007 0.0023 -0.0053 0.0064	-1 0 -1 1	
345678	12:54 12:55 <i>12:56</i> 12:58	9.00 9.50 10.00 10.50 11.00	0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150	0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460	-0.0197 0.0020 0.0049 -0.0092		1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092 0.0095	0.265 0.350 0.475 0.575	-0.0052 0.0007 0.0023 -0.0053	-1 (-1 1	
3456789	12:54 12:55 12:56 12:58 13:00 13:02 13:23	9.00 9.50 10.00 10.50 11.00 11.50 12.00 12.25	0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.350 1.430	0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572	-0.0197 0.0020 0.0049 -0.0092 0.0095 -0.0082		1.00 1.00 1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092 0.0095 -0.0082	0.265 0.350 0.475 0.575 0.675 0.715	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059	-1 0 -1 1 -1 6	
345678	12:54 12:55 12:56 12:58 13:00 13:02	9.00 9.50 10.00 10.50 11.00 11.50 12.00 12.25 12.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.350 1.430 1.420	0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568	-0.0197 0.0020 0.0049 -0.0092 0.0095 -0.0082 0.0420 0.0512 0.1060		1.00 1.00 1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092 0.0095 -0.0082 0.0420	0.265 0.350 0.475 0.575 0.675 0.715 0.532 0.355 0.358	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224	-1 () () () () () () () () () () () () ()	
3 4 5 6 7 8 9 10 11	12:54 12:55 12:56 12:58 13:00 13:02 13:23 13:03 13:25	9.00 9.50 10.00 10.50 11.00 11.50 12.00 12.25 12.50 12.75	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 1.150 1.350 1.430 1.420 1.420 1.420 1.430 1.450	0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568 0.558 0.572 0.580	-0.0197 0.0020 0.0049 -0.0092 0.0095 -0.0082 0.0420 0.0512 0.1060 0.1017		1.00 1.00 1.00 1.00 1.00 1.00	-0.0197 0.0020 0.0049 -0.0092 0.0095 -0.0082 0.0420 0.0512	0.265 0.350 0.475 0.575 0.675 0.715 0.532 0.355 0.355 0.358 0.363	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224 0.0182	-1 0 -1 1 -1 6 5 10 10	
3 4 5 6 7 8 9 10 11 12	12:54 12:55 12:56 12:58 13:00 13:02 13:03 13:03 13:25 13:04	9.00 9.50 10.00 10.50 11.00 11.50 12.00 12.25 12.50 12.75 13.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 1.150 1.350 1.430 1.420 1.420 1.420 1.420 1.420 1.430 1.450	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568 0.558 0.572 0.580 0.588	-0.0197 0.0020 0.0049 -0.0092 0.0095 -0.0082 0.0420 0.0512 0.1060 0.1017 0.1404		1.00 1.00 1.00 1.00 1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092 -0.0082 0.0420 0.0512 0.1060 0.1017 0.1404	0.265 0.350 0.475 0.575 0.675 0.715 0.532 0.355 0.355 0.358 0.363 0.551	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224 0.0182 0.0379 0.0369 0.0774	-1 0 -1 1 -1 6 5 10 10 21	
3 4 5 6 7 8 9 10 11 12 13	12:54 12:55 12:56 12:58 13:00 13:02 13:03 13:03 13:25 13:04 13:05	9.00 9.50 10.00 11.50 11.00 12.25 12.50 12.75 13.00 13.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 1.150 1.350 1.430 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568 0.558 0.558 0.572 0.580 0.588 0.588 0.588	-0.0197 0.0020 0.0049 -0.0092 0.0095 -0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092 -0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913	0.265 0.350 0.475 0.575 0.675 0.715 0.532 0.355 0.355 0.358 0.363 0.551 0.570	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224 0.0182 0.0379 0.0369 0.0774 0.1090	-1 0 -1 -1 -1 6 5 10 10 21 30	
3 4 5 6 7 7 8 9 10 11 12 13 14	12:54 12:55 12:56 12:58 13:00 13:02 13:23 13:03 13:25 13:04 13:05 13:28	9.00 9.50 10.00 11.50 11.00 12.25 12.50 12.75 13.00 13.50 13.75	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.430 1.430 1.420 1.430 1.430 1.450 1.450 1.450 1.480	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568 0.568 0.572 0.580 0.588 0.588 0.588 0.592	-0.0197 0.0020 0.0049 -0.0092 0.0095 -0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092 0.0095 -0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050	0.265 0.350 0.475 0.575 0.675 0.715 0.532 0.355 0.358 0.363 0.363 0.551 0.570 0.370	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224 0.0182 0.0379 0.0369 0.0774 0.1090 0.0388	-1 0 -1 -1 -1 6 5 10 10 21 30 10	
3 4 5 6 7 8 9 10 11 12 13 14 15	12:54 12:55 12:56 12:58 13:00 13:02 13:23 13:03 13:25 13:04 13:05 13:28 13:07	9.00 9.50 10.00 11.50 11.00 12.25 12.50 12.75 13.00 13.50 13.75 14.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.430 1.430 1.420 1.430 1.450 1.450 1.450 1.480 1.480	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568 0.572 0.580 0.588 0.608 0.592 0.580	-0.0197 0.0020 0.0049 -0.0092 0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092 0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378	0.265 0.350 0.475 0.575 0.675 0.715 0.532 0.355 0.358 0.363 0.551 0.570 0.370 0.370 0.363	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224 0.0182 0.0379 0.0369 0.0774 0.1090 0.0388 0.0500	$ \begin{array}{r} -1 \\ 0 \\ 0 \\ -1 \\ 1 \\ -1 \\ 6 \\ 5 \\ 100 \\ 100 \\ 211 \\ 300 \\ 14 \\ 14 \\ 14 \\ 14 \\ 14 \\ 14 \\ 14 \\ 14$	
3 4 5 6 7 8 9 10 11 12 13 14 15 16	12:54 12:55 12:56 12:58 13:00 13:02 13:03 13:23 13:03 13:25 13:04 13:05 13:28 13:07 13:28 13:07	9.00 9.50 10.00 11.00 11.00 12.25 12.50 12.75 13.00 13.50 13.75 14.00 14.25	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.350 1.430 1.420 1.420 1.430 1.450 1.450 1.450 1.480 1.480 1.480 1.480 1.490	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568 0.572 0.580 0.588 0.608 0.592 0.580 0.556	-0.0197 0.0020 0.0049 -0.0092 0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378 0.0620		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092 -0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378 0.0620	0.265 0.350 0.475 0.575 0.675 0.715 0.532 0.355 0.358 0.363 0.551 0.570 0.370 0.370 0.363 0.348	-0.0052 0.0007 0.0023 -0.0053 0.0059 0.0224 0.0182 0.0379 0.0369 0.0774 0.1090 0.0388 0.0500 0.0215	-1 0 0 -1 1 -1 6 5 5 10 10 21 30 10 10 21 30 10 14 6	
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3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	12:54 12:55 12:56 12:58 13:00 13:02 13:03 13:23 13:03 13:25 13:04 13:05 13:28 13:07 13:28 13:07 13:30 13:08 13:11	9.00 9.50 10.00 10.50 11.00 12.25 12.50 12.75 13.00 13.50 13.75 14.00 14.25 14.50 15.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.350 1.430 1.420 1.420 1.420 1.420 1.450 1.450 1.450 1.450 1.390 1.380 1.220	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568 0.558 0.572 0.580 0.588 0.608 0.592 0.580 0.556 0.556 0.555 0.552 0.488	-0.0197 0.0020 0.0049 -0.0092 0.0095 -0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378 0.0620 0.0213 -0.0141		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092 0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378 0.0620 0.0213 -0.0141	0.265 0.350 0.475 0.575 0.675 0.715 0.532 0.355 0.358 0.363 0.551 0.570 0.370 0.370 0.363 0.348 0.517 0.610	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224 0.0182 0.0379 0.0369 0.0774 0.1090 0.0388 0.0500 0.0215 0.0110 -0.0086	-11 0 0 0 1 1 1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	
3 4 5 6 7 8 9 9 10 11 12 13 14 15 16 17 18 19	12:54 12:55 12:56 12:58 13:00 13:02 13:03 13:03 13:25 13:04 13:05 13:05 13:28 13:07 13:30 13:07 13:30 13:08 13:11 13:12	9.00 9.50 10.00 11.00 11.50 12.25 12.50 12.75 13.00 13.50 13.75 14.00 14.25 14.50 15.00 15.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.350 1.430 1.420 1.430 1.420 1.430 1.450 1.450 1.450 1.480 1.480 1.480 1.390 1.380 1.220 1.200	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.540 0.572 0.568 0.572 0.580 0.588 0.592 0.588 0.592 0.580 0.592 0.580 0.555 0.555 0.488 0.440	-0.0197 0.0020 0.0049 -0.0092 0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378 0.0620 0.0213 -0.0141 -0.0187		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092 0.0082 0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378 0.0620 0.0213 -0.0141 -0.0187	0.265 0.350 0.475 0.575 0.675 0.532 0.355 0.358 0.363 0.551 0.570 0.370 0.363 0.348 0.517 0.610 0.550	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224 0.0182 0.0379 0.0369 0.0774 0.1090 0.0388 0.0500 0.0215 0.0110 -0.0086 -0.0103	-11 0 0 -11 1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	12:54 12:55 12:56 12:58 13:00 13:02 13:03 13:03 13:03 13:05 13:04 13:05 13:04 13:05 13:28 13:07 13:30 13:08 13:11 13:12 13:14	9.00 9.50 10.00 11.00 11.50 12.25 12.50 12.75 13.00 13.50 13.75 14.00 14.25 14.50 15.50 15.50 16.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.350 1.430 1.420 1.420 1.430 1.450 1.450 1.450 1.450 1.480 1.450 1.380 1.380 1.220 1.200 1.200 1.200	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568 0.558 0.572 0.580 0.588 0.592 0.588 0.592 0.580 0.556 0.555 0.555 0.488 0.440 0.404	-0.0197 0.0020 0.0049 -0.0092 0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378 0.0620 0.0213 -0.0141 -0.0187 -0.0354		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	-0,0197 0.0020 0.0049 -0.0092 0.0082 0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378 0.0620 0.0213 -0.0141 -0.0187 -0.0354	0.265 0.350 0.475 0.575 0.675 0.532 0.355 0.358 0.363 0.551 0.570 0.370 0.363 0.348 0.517 0.610 0.550 0.505	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224 0.0182 0.0379 0.0369 0.0774 0.1090 0.0388 0.0500 0.0215 0.0110 -0.0086 -0.0103 -0.0179	-11 00 00 -1.1 1 -1 6 5 5 5 100 100 100 100 100 100 144 6 6 3 3 2 -2 2 -2 2 -5	
3 4 5 6 7 7 8 9 9 10 11 12 13 14 15 16 17 18 19 20 21	12:54 12:55 12:56 12:58 13:00 13:02 13:03 13:03 13:25 13:04 13:05 13:28 13:07 13:28 13:07 13:30 13:08 13:11 13:12 13:14 13:15	9.00 9.50 10.00 11.50 11.00 11.50 12.25 12.50 12.75 13.00 13.50 13.75 14.00 14.25 14.50 15.50 15.50 16.00 16.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.350 1.430 1.420 1.420 1.420 1.450 1.450 1.450 1.450 1.450 1.450 1.480 1.450 1.380 1.380 1.220 1.100 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.380 1.220 1.20 1.20 1.20 1.380 1.220 1.20 1.20 1.20 1.380 1.20 1.380 1.20 1.380 1.20 1.380 1.20 1.380 1.380 1.20 1.380 1.380 1.20 1.380 1.380 1.20 1.380 1.20 1.380 1.20 1.380 1.380 1.380 1.20 1.50 1.380 1.20 1.380 1.20 1.50 1.380 1.20 1.50 1.380 1.20 1.50 1.380 1.20 1.50 1.50 1.50 1.380 1.20 1.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568 0.558 0.572 0.580 0.588 0.608 0.592 0.580 0.556 0.555 0.555 0.488 0.440 0.404 0.300	-0.0197 0.0020 0.0049 -0.0092 0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378 0.0620 0.0213 -0.0141 -0.0187 -0.0354 -0.0210		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	-0,0197 0,0020 0,0049 -0,0092 0,0082 0,0082 0,0420 0,0512 0,1060 0,1017 0,1404 0,1913 0,1050 0,1378 0,0620 0,0213 -0,0141 -0,0354 -0,0210	0.265 0.350 0.475 0.575 0.675 0.532 0.355 0.355 0.358 0.363 0.551 0.570 0.370 0.363 0.348 0.517 0.610 0.550 0.505 0.375	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224 0.0182 0.0379 0.0369 0.0774 0.1090 0.0388 0.0500 0.0215 0.0110 -0.0086 -0.0179 -0.0079	-11 0 0 0 0 0 0 0 1 1 1 1 0 0 10 0 10 0	
3 4 5 6 7 8 9 9 10 11 12 13 14 15 16 17 18 19 20 21 22	12:54 12:55 12:56 12:58 13:00 13:02 13:03 13:03 13:25 13:04 13:05 13:28 13:07 13:30 13:08 13:10 13:10 13:11 13:11 13:12 13:14 13:15 13:16	9.00 9.50 10.00 11.50 11.00 11.50 12.25 12.50 12.75 13.00 13.50 13.75 14.00 14.25 14.50 15.50 15.50 16.00 16.50 17.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.350 1.430 1.420 1.420 1.420 1.420 1.450 1.450 1.450 1.450 1.480 1.450 1.380 1.380 1.220 1.380 1.220 1.200 1.450 1.520	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568 0.558 0.572 0.580 0.588 0.608 0.592 0.580 0.556 0.555 0.555 0.488 0.440 0.404 0.300 0.236	-0.0197 0.0020 0.0049 -0.0092 0.0095 -0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378 0.0620 0.0213 -0.0141 -0.0187 -0.0354 -0.0210 -0.0213		1.00 1.00	-0,0197 0,0020 0,0049 -0,0092 0,0082 0,0082 0,0420 0,0512 0,1060 0,1017 0,1404 0,1913 0,1050 0,1378 0,0620 0,0213 -0,0141 -0,0354 -0,0210 -0,0213	0.265 0.350 0.475 0.575 0.675 0.532 0.355 0.355 0.355 0.355 0.355 0.355 0.363 0.551 0.570 0.370 0.363 0.348 0.517 0.610 0.550 0.555 0.375 0.295	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224 0.0182 0.0379 0.0369 0.0774 0.1090 0.0388 0.0500 0.0215 0.0110 -0.0086 -0.0103 -0.0179 -0.0079 -0.0063	-11 00 00 -1.1 1 -1 6 5 5 5 100 100 100 100 144 6 6 3.3 -2 -2 -2 -5 5 -2 -2 -1	
3 4 5 6 7 7 8 9 9 10 11 12 13 14 15 16 17 18 19 20 21	12:54 12:55 12:56 12:58 13:00 13:02 13:03 13:03 13:25 13:04 13:05 13:28 13:07 13:28 13:07 13:30 13:08 13:11 13:12 13:14 13:15	9.00 9.50 10.00 11.50 11.00 11.50 12.25 12.50 12.75 13.00 13.50 13.75 14.00 14.25 14.50 15.50 15.50 16.00 16.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.530 0.700 0.950 1.150 1.350 1.430 1.420 1.420 1.420 1.450 1.450 1.450 1.450 1.450 1.450 1.480 1.450 1.380 1.380 1.220 1.100 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.380 1.220 1.20 1.20 1.20 1.380 1.220 1.20 1.20 1.380 1.220 1.20 1.380 1.220 1.380 1.220 1.380 1.220 1.380 1.250 1.380 1.250 1.380 1.250 1.380 1.380 1.250 1.380 1.380 1.380 1.250 1.380 1.380 1.250 1.380 1.380 1.380 1.220 1.380 1.220 1.380 1.380 1.380 1.220 1.380 1.380 1.220 1.380 1.220 1.380 1.380 1.220 1.380 1.220 1.380 1.200 1.380 1.220 1.380 1.220 1.380 1.220 1.380 1.220 1.520 1	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.212 0.280 0.380 0.460 0.540 0.572 0.568 0.558 0.572 0.580 0.588 0.608 0.592 0.580 0.556 0.555 0.555 0.488 0.440 0.404 0.300	-0.0197 0.0020 0.0049 -0.0092 0.0082 0.0420 0.0512 0.1060 0.1017 0.1404 0.1913 0.1050 0.1378 0.0620 0.0213 -0.0141 -0.0187 -0.0354 -0.0210		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	-0,0197 0,0020 0,0049 -0,0092 0,0082 0,0082 0,0420 0,0512 0,1060 0,1017 0,1404 0,1913 0,1050 0,1378 0,0620 0,0213 -0,0141 -0,0354 -0,0210	0.265 0.350 0.475 0.575 0.675 0.532 0.355 0.355 0.358 0.363 0.551 0.570 0.370 0.363 0.348 0.517 0.610 0.550 0.505 0.375	-0.0052 0.0007 0.0023 -0.0053 0.0064 -0.0059 0.0224 0.0182 0.0379 0.0369 0.0774 0.1090 0.0388 0.0500 0.0215 0.0110 -0.0086 -0.0179 -0.0079	-11 0 0 1 1 1 -1 1 6 5 5 5 5 100 100 100 100 101 100 100 104 3 3 3 -2 2 -2 2 -5 5 -2 2 -1 1 -0 0	



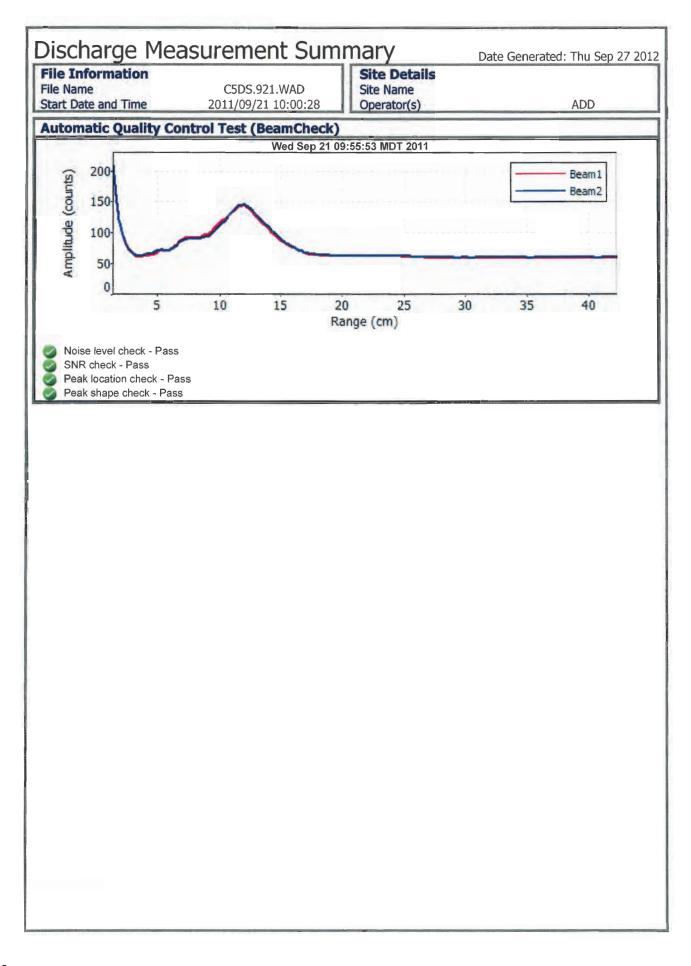
			asurement Sum	ind y	Date Generated: Thu Sep 27 201
	Informa Name	ation	C5TRIB.921.WAD	Site Details Site Name	
Start	Date and	Time	2011/09/21 12:50:24	Operator(s)	ADD
Qua	lity Con	trol			
St	Loc	%Dep		Message	
1	8.50	0.6	High angle: -150		
2	9.00	0.6	Boundary QC is Good; possible bo	oundary interference	
5	10.50		High SNR variation during measu		
8	12.00	0.6	High SNR variation during measu	rement: 6.0,5.6	
9	12.25	0.6	High SNR variation during measu	rement: 7.7,6.5	
10	12.50		SNR (26.2) is different from typic		
11	12.75		SNR (26.2) is different from typic		
12	13.00		SNR (24.9) is different from typic		
13	13.50		SNR (24.9) is different from typic		
15	14.00		SNR (24.7) is different from typic		
16	14.25		High SNR variation during measured		
17	14.50		High angle: 23		
19	15.50		SNR (47.0) is different from typic	al SNR (36.4)	
20	16.00	0.6	High angle: -151 SNR (50.5) is different from typic		
21	16.50	0.6	High angle: -179 SNR (50.1) is different from typic		
22	17.00	0.6	High angle: 171 High SNR variation during measu		
23	17.50		High SNR variation during measur		
24	18.00		High differences in beam SNR: 29		



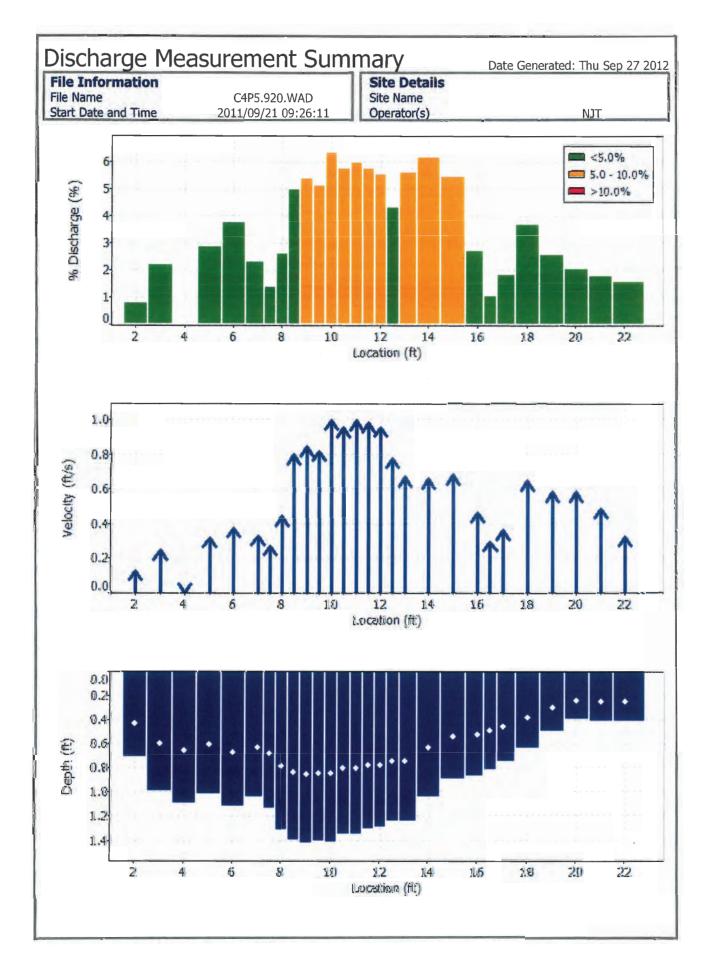
File	Name t Date a				5.921.WA		Site Der Site Nam Operator	e			А	ADD .	
Sys	tem In	forma	ation			Units	(English L	Inits)	Di	scharge	Uncerta	ainty	
	sor Type			FlowTrac	cker	Distance	ft		Category		the second day of the	and the second se	tats
Seri	al #			P3532	2	/elocity	ft/s		Accuracy			1.0%	1.09
CPU	Firmwa	re Versi	on	3.7	1	Area	ft^2		Depth			0.1%	1.20
	ware Ve			2.30		Discharge	cfs		Velocity			0.8%	4.7
Mou	inting Co	prrection	1	0.0%	0				Wie			0.1%	0.1
-	limmary								-	thod		1.7%	
	veraging Int 30 # Stations						0.5			Stations		2.0%	-
Averaging Int.				30 # Stations			25		-	erall		3.0%	5.09
Start Edge Mean SNR			RE		Total Widt		17.700						
			31.4		Total Area		19.44(
	n Temp	ion	46.46 Mid-So		lean Dep		1.098 0.6512						
JISC	h. Equat	1011	Mid-Se		fean Velo		12.659						
_	_				otal Dis	charge	12.035	4	_			and a low	
Mo	asuren	ont D	oculte										
	Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrFa	ct	MeanV	Area	Flow	%
0	10:00	4.10	None	0.000	0.0	0.0	0.0000	AL [*] A REAL PROPERTY AND ADDRESS OF TAXABLE PARTY.	1.00	0.0000	0.000	0.0000	
1	10:00	5.00	0.6	1.050	0.6	0.420	0.1831		1.00	0.1831	0.866	0.1586	Street, Square, Sq
2	10:02	5.75	0.6	1.450	0.6	0.580	0.7087		1.00	0.7087	1.088	0.7707	
3	10:04	6.50	0.6	1.360	0.6	0.544	0.4610		1.00	0.4610	1.020	0.4701	3.
4	10:05	7.25	0.6	1.420	0.6	0.568	0.6690		1.00	0.6690	1.065	0.7124	
5	10:10	8.00	0.6	1.360	0.6	0.544	0.6204		1.00	0.6204	1.020	0.6328	5.
	and the second s												
6	10:11	8.75	0.6	1.350	0.6	0.540	0.4665		1.00	0.4665	1.013	0.4724	
67	10:11 10:12	8.75 9.50	0.6 0.6	1.350 1.290	0.6	0.516	0.8947		1.00	0.8947	0.968	0.4724	6
6 7 8	10:11 10:12 10:13	8.75 9.50 10.25	0.6 0.6 0.6	1.350 1.290 1.240	0.6	0.516	0.8947		1.00 1.00	0.8947	0.968	0.4724 0.8656 0.7885	6
6 7 8 9	10:11 10:12 10:13 10:14	8.75 9.50 10.25 11.00	0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240	0.6 0.6 0.6	0.516 0.496 0.496	0.8947 0.8478 0.9715		1.00 1.00 1.00	0.8947 0.8478 0.9715	0.968 0.930 0.930	0.4724 0.8656 0.7885 0.9036	6
6 7 8 9 10	10:11 10:12 10:13 10:14 10:19	8.75 9.50 10.25 11.00 <i>11.75</i>	0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.280	0.6 0.6 0.6 0.6	0.516 0.496 0.496 0.512	0.8947 0.8478 0.9715 0.6168		1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168	0.968 0.930 0.930 0.960	0.4724 0.8656 0.7885 0.9036 0.5921	6 6 7 4
6 7 8 9 <i>10</i> 11	10:11 10:12 10:13 10:14 <i>10:19</i> 10:20	8.75 9.50 10.25 11.00 <i>11.75</i> 12.50	0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.280 1.220	0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.496 0.512 0.488	0.8947 0.8478 0.9715 0.6168 0.7385		1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385	0.968 0.930 0.930 0.960 0.915	0.4724 0.8656 0.7885 0.9036 0.5921 0.6758	6 6 7 4
6 7 8 9 10 11 12	10:11 10:12 10:13 10:14 <i>10:19</i> 10:20 10:21	8.75 9.50 10.25 11.00 <i>11.75</i> 12.50 13.25	0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.280 1.220 1.200	0.6 0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.496 0.512 0.488 0.488	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945		1.00 1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945	0.968 0.930 0.930 0.960 0.915 0.900	0.4724 0.8656 0.7885 0.9036 <i>0.5921</i> 0.6758 0.9851	6 6 7 4 5 7
6 7 8 9 10 11 12 13	10:11 10:12 10:13 10:14 <i>10:19</i> 10:20 10:21 10:23	8.75 9.50 10.25 11.00 <i>11.75</i> 12.50 13.25 14.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.240 1.220 1.220 1.200 1.190	0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.496 0.512 0.488 0.480 0.476	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517		1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517	0.968 0.930 0.930 0.960 0.915 0.900 0.892	0.4724 0.8656 0.7885 0.9036 0.5921 0.6758 0.9851 0.7601	6 6 7 4 5 7 6
6 7 8 9 10 11 12 13 14	10:11 10:12 10:13 10:14 <i>10:19</i> 10:20 10:21 10:23 10:25	8.75 9.50 10.25 11.00 <i>11.75</i> 12.50 13.25 14.00 14.75	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.220 1.220 1.200 1.190 1.180	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.512 0.488 0.488 0.480 0.476 0.472	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736	0.968 0.930 0.930 0.960 0.915 0.900 0.892 0.885	0.4724 0.8656 0.7885 0.9036 0.5921 0.6758 0.9851 0.7601 0.6847	6 6 7 4 5 7 6 5
6 7 8 9 10 11 12 13 14 15	10:11 10:12 10:13 10:14 10:19 10:20 10:21 10:23 10:25 10:26	8.75 9.50 10.25 11.00 <i>11.75</i> 12.50 13.25 14.00 14.75 15.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.220 1.220 1.200 1.190 1.180 1.150	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.512 0.488 0.480 0.476 0.472 0.460	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657	0.968 0.930 0.930 0.960 0.915 0.900 0.892 0.885 0.862	0.4724 0.8656 0.7885 0.9036 0.5921 0.6758 0.9851 0.7601 0.6847 0.5741	6 6 7 4 5 7 6 5 5 4
6 7 8 9 10 11 12 13 14 15 16	10:11 10:12 10:13 10:14 10:19 10:20 10:21 10:23 10:25 10:26 10:27	8.75 9.50 10.25 11.00 <i>11.75</i> 12.50 13.25 14.00 14.75 15.50 16.25	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.220 1.220 1.200 1.190 1.180 1.150 1.150	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.512 0.488 0.480 0.476 0.472 0.460 0.460	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614	0.968 0.930 0.930 0.960 0.915 0.900 0.892 0.885 0.862 0.862	0.4724 0.8656 0.7885 0.9036 0.5921 0.6758 0.9851 0.7601 0.6847 0.5741 0.4841	6 6 7 4. 5 7 6 5 4 3
6 7 8 9 10 11 12 13 14 15 16 17	10:11 10:12 10:13 10:14 10:19 10:20 10:21 10:23 10:25 10:26	8.75 9.50 10.25 11.00 <i>11.75</i> 12.50 13.25 14.00 14.75 15.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.220 1.220 1.200 1.190 1.180 1.150	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.512 0.488 0.480 0.476 0.472 0.460	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657	0.968 0.930 0.930 0.960 0.915 0.900 0.892 0.885 0.862	0.4724 0.8656 0.7885 0.9036 0.5921 0.6758 0.9851 0.7601 0.6847 0.5741	6 6 7 4 5 7 6 5 4 3 4
6 7 8 9 10 11 12 13 14 15 16 17 18	10:11 10:12 10:13 10:14 10:19 10:20 10:21 10:23 10:25 10:26 10:27 10:28	8.75 9.50 10.25 11.00 11.75 12.50 13.25 14.00 14.75 15.50 16.25 17.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.220 1.200 1.200 1.190 1.180 1.150 1.150 1.100	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.512 0.488 0.480 0.476 0.472 0.460 0.460 0.440	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614 0.6411 0.6250		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614 0.6411	0.968 0.930 0.930 0.960 0.915 0.900 0.892 0.885 0.862 0.862 0.862 0.825	0.4724 0.8656 0.7885 0.9036 0.5921 0.6758 0.9851 0.7601 0.6847 0.5741 0.4841 0.5289	6 6 7 4 5 7 6 5 4 3 4 3 4 3
6 7 8 9 10 11 12 13 14 15 16 17 18 19	10:11 10:12 10:13 10:14 10:19 10:20 10:21 10:23 10:25 10:26 10:27 10:28 10:29	8.75 9.50 10.25 11.00 11.75 12.50 13.25 14.00 14.75 15.50 16.25 17.00 17.75	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.220 1.200 1.200 1.190 1.180 1.150 1.150 1.150 1.100	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.512 0.488 0.480 0.476 0.472 0.460 0.460 0.460 0.440	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614 0.6411 0.6250 0.6900 0.5256		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614 0.6411 0.6250	0.968 0.930 0.930 0.960 0.915 0.900 0.892 0.885 0.862 0.862 0.862 0.825 0.757	0.4724 0.8656 0.7885 0.9036 0.5921 0.6758 0.9851 0.7601 0.6847 0.5741 0.4841 0.5289 0.4734	6 6 7 4 5 7 6 5 7 6 5 7 6 5 7 6 5 7 4 3 3 3
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	10:11 10:12 10:13 10:14 10:20 10:21 10:23 10:25 10:26 10:27 10:28 10:29 10:31	8.75 9.50 10.25 11.00 11.75 12.50 13.25 14.00 14.75 15.50 16.25 17.00 17.75 18.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.220 1.200 1.200 1.190 1.180 1.150 1.150 1.150 1.100 1.010 0.920	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.496 0.512 0.488 0.480 0.476 0.472 0.460 0.460 0.460 0.440 0.404 0.368	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614 0.6411 0.6250 0.6900		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614 0.6411 0.6250 0.6900	0.968 0.930 0.930 0.960 0.915 0.900 0.892 0.885 0.862 0.862 0.862 0.825 0.757 0.690	0.4724 0.8656 0.7885 0.9036 0.5921 0.6758 0.9851 0.7601 0.6847 0.5741 0.4841 0.5289 0.4734 0.4760	6 6 7 4 5 7 6 5 4 3 4 3 3 2
6 7 8	10:11 10:12 10:13 10:14 10:19 10:20 10:21 10:23 10:25 10:26 10:27 10:28 10:29 10:31 10:32	8.75 9.50 10.25 11.00 11.75 12.50 13.25 14.00 14.75 15.50 16.25 17.00 17.75 18.50 19.25	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.220 1.200 1.200 1.190 1.180 1.150 1.150 1.150 1.100 1.010 0.920 0.940	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.496 0.512 0.488 0.488 0.488 0.476 0.476 0.472 0.460 0.440 0.440 0.404 0.368 0.376	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614 0.6411 0.6250 0.6900 0.5256		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614 0.6411 0.6250 0.6900 0.5256	0.968 0.930 0.930 0.960 0.915 0.900 0.892 0.885 0.862 0.862 0.862 0.862 0.825 0.757 0.690 0.705	0.4724 0.8656 0.7885 0.9036 0.5921 0.6758 0.9851 0.7601 0.6847 0.5741 0.4841 0.5289 0.4734 0.4760 0.3705	6 6 7 4 5 7 6 5 5 7 6 6 5 5 4 3 3 3 2 1
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	10:11 10:12 10:13 10:14 10:20 10:21 10:23 10:25 10:26 10:27 10:28 10:29 10:31 10:32 10:34	8.75 9.50 10.25 11.00 <i>11.75</i> 12.50 13.25 14.00 14.75 15.50 16.25 17.00 17.75 18.50 19.25 20.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.350 1.290 1.240 1.240 1.280 1.220 1.200 1.190 1.180 1.150 1.150 1.150 1.100 1.010 0.920 0.940 0.880	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.516 0.496 0.496 0.512 0.488 0.480 0.476 0.476 0.472 0.460 0.460 0.460 0.440 0.404 0.368 0.376 0.352	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614 0.6411 0.6250 0.6900 0.5256 0.2572		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.8947 0.8478 0.9715 0.6168 0.7385 1.0945 0.8517 0.7736 0.6657 0.5614 0.6411 0.6250 0.6900 0.5256 0.2572	0.968 0.930 0.930 0.960 0.915 0.900 0.892 0.885 0.862 0.862 0.862 0.825 0.757 0.690 0.705 0.660	0.4724 0.8656 0.7885 0.9036 0.5921 0.6758 0.9851 0.7601 0.6847 0.5741 0.4841 0.5289 0.4734 0.4760 0.3705 0.1697	66 66 77 4. 55 77 66 55 55 44 33 33 22 11



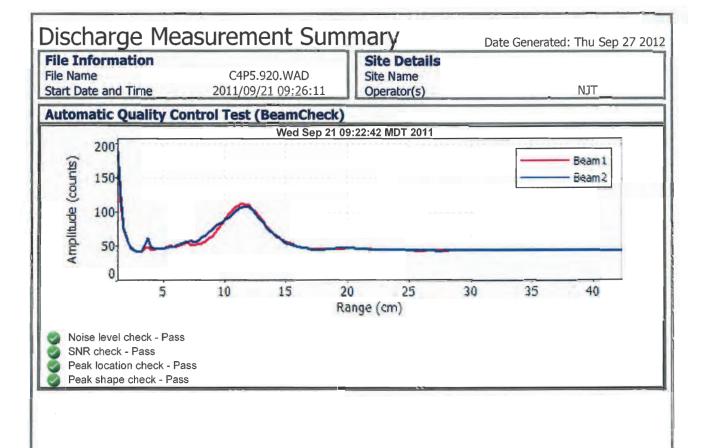
	criary	C TICU	surement Sur	innary	Date Generated: Thu Sep 27 2012		
File Information File Name Start Date and Time			C5DS.921.WAD 2011/09/21 10:00:28	28 Operator(s) ADD			
Qua	lity Cont	rol					
St	Loc	%Dep		Message			
1	5.00	0.6	SNR (42.6) is different from typ	pical SNR (31.4)			
3	6.50	0.6	High standard error: 0.032				
5	8.00	0.6	High standard error: 0.031				
10	11.75	0.6	High standard error: 0.032				
23	21.50		SNR (58.7) is different from typ High SNR variation during mea				



File	Name	mation			5.920.WAI 9/21 09:20		Site Der Site Name Operator	e				TLN	
Sys	stem In	nforma	tion			Units	(English U	Inits)	Discharge Uncertainty				
Sen	sor Type	1		FlowTrac	cker	Distance	ft		Category		1	ISO St	
Seri	al #			P3012	2	/elocity	ft/s		AC	curacy		1.0%	1.09
CPU	Firmwa	re Versio	n	3.7 Area		Area	and the local division of the local division		Depth		0.2%	0.8	
Soft	ware Ve	r				Discharge	cfs			locity		0.9%	3.09
Mou	inting Co	prrection		0.0%	o 🔰					dth		0.1%	0.1
				- Charlen Colores		-	and a state	in the second		thod		1.6%	012
	mmary									Stations		1.7%	
			30		# Stations		30						2 20
Start Edge			RE		Total Widt		22.600		0	erall		2.7%	3.39
	IN SNR		30.6		otal Area		20.117	7					
Mean Temp			45.94		lean Dep		0.890						
Disch. Equation			Mid-Se		lean Velo		0.5554						
				1	otal Dis	charge	11.172	0					
	Sugar		Constant in the	-	1				-				-
the second s	Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrFa	ct T	MeanV	Area	Flow	%
0	09:26	1.00	None		0.0		and the second division of the local divisio	The second se	1.00	0.0000	0.000	0.0000	
1	09:26	2.00	0.6	0.720	0.6	0.288	0.1250	-	.00	0.1250	0.720	0.0900	0.
2	09:27	3.00	0.6		0.6	0.400	0.2461	the second se	1.00	0.2461	1.000	0.2461	
3	09:28	4.00	0.6	1.100	0.6	0.440	-0.0052	3	.00	-0.0052	1.100	-0.0058	-0.
4	09:31	5.00	0.6	1.020	0.6	0.408	0.3169		1.00	0.3169	1.020	0.3233	
5	09:32	6.00	0.6	1.120	0.6	0.448	0.3753		1.00	0.3753	1.120	0.4204	
6	09:33	7.00	0.6	1.050	0.6	0.420	0.3291		.00	0.3291	0.787	0.2591	2.
7	10:11	7.50	0.6		0.6	0.456	0.2730		1.00	0.2730	0.570	0.1556	
8	09:37	8.00	0.6	1.320	0.6	0.528	0.4432	1	.00	0.4432	0.660	0.2925	2
9	09:40	8.50	0.6		0.6	0.560	0.7963		1.00	0.7963	0.700	0.5574	
10	09:41	9.00	0.6		0.6	0.572	0.8448		1.00	0.8448	0.715	0.6041	
11	09:43	9.50	0.6		0.6	0.564	0.8173	seed of the local division of the local divi	1.00	0.8173	0.705	0.5762	
12	09:45	10.00	0.6		0.6	0.568	0.9980	and the second s	1.00	0.9980	0.710	0.7086	
13	09:46	10.50	0.6		0.6	0.540	0.9528		1.00	0.9528	0.675	0.6431	
14	09:47	11.00	0.6		0.6	0.540	0.9934		1.00	0.9934	0.675	0.6706	
15	09:49	11.50	0.6		0.6	0.524	0.9843		1.00	0.9843	0.655	0.6447	
16	09:50	12.00	0.6		0.6	0.520	0.9567		1.00	0.9567	0.650	0.6218	
17	09:51	12.50	0.6		0.6	0.500	0.7772		.00	0.7772	0.625	0.4858	
18	09:52	13.00	0.6	1.250	0.6	0.500	0.6699		.00	0.6699	0.938	0.6281	5.
	09:54	14.00	0.6	and the second division of the second divisio	0.6	0.420	0.6565		1.00	0.6565	1.050	0.6892	
	09:55		0.6	and the second se		0.360	0.6804		1.00	the state of the second s	0.900	0.3049	
20		16.00 16.50	0.6		0.6	0.350	0.4646		1.00	0.4646	0.656	0.3049	
20 21	10.14		0.6		0.6	0.304	0.3612		1.00	0.3612	0.410	0.2059	
20 21 22	10:14		0.0		0.6	0.256	0.6460		1.00	0.3812	0.640	0.4135	
20 21 22 23	09:59	17.00	0.6	0 640		0.230			1.00	0.5820	0.500	0.4135	
20 21 22 23 24	09:59 10:00	18.00	0.6			0 200							
20 21 22 23 24 25	09:59 10:00 10:02	18.00 19.00	0.6	0.500	0.6	0.200	0.5820	the state is not set to be in the set					
19 20 21 22 23 24 25 26 27	09:59 10:00 10:02 10:03	18.00 19.00 20.00	0.6 0.6	0.500	0.6	0.160	0.5817		1.00	0.5817	0.400	0.2326	2
20 21 22 23 24 25	09:59 10:00 10:02	18.00 19.00	0.6	0.500 0.400 0.420	0.6								



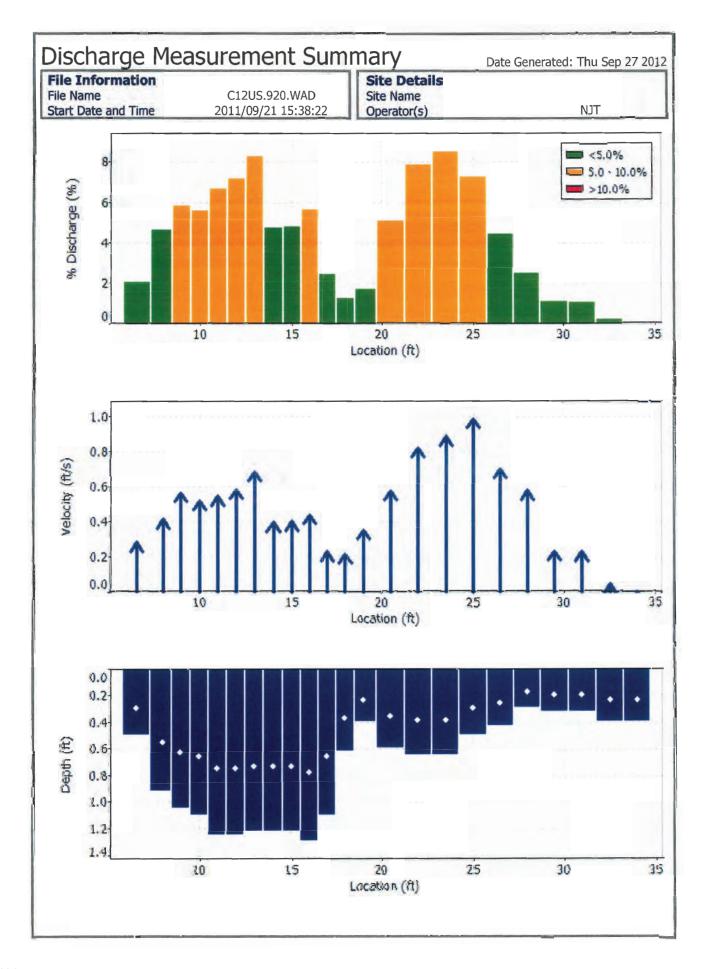
	File Information File Name Start Date and Time		C4P5.920.WAD	Site Details Site Name	
Start			2011/09/21 09:26:11	Operator(s)	NJT
Qua	lity Con	trol			
St	Loc	%Dep		Message	
1	2.00	0.6	High SNR variation during measure	surement: 5.2,5.2	
3	4.00	0.6 0.6	SNR (47.9) is different from typ High SNR variation during meas	ical SNR (30.6) surement: 11.2,9.5	
6	7.00	0.6	High standard error: 0.032		
8	8.00	0.6	High standard error: 0.045		
17	12.50	0.6	High angle: -22		
18	13.00	0.6	High angle: -25		
23	17.00	0.6	High standard error: 0.039		



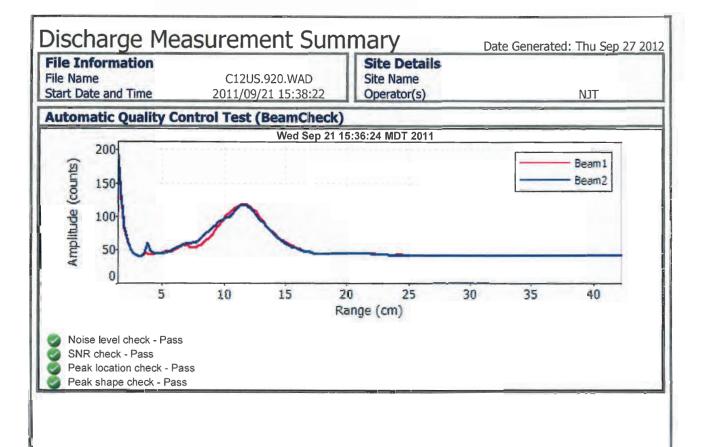
File	Name T Date a				.920.WAE /21 1 <u>0:3</u> (Site Details Site Name Operator(s)					NJT	
Sys	stem In	forma	tion			Inits	(English L	Jnits)	Discharge Uncertainty				
Sen	sor Type			FlowTrac	cker	Distance	ft		Category			and the second se	Stats
	al #			P3012		elocity	ft/s		Accuracy			1.0%	1.00
CPL	Firmwa	re Versio	on	3.7		rea	ft^2		Depth			0.1%	1.19
	ware Ve			2.30)ischarge	cfs		Ve	locity		0.9%	2.09
Mounting Correction				0.0%	0				and the second distance of the second distanc	dth		0.1%	0,19
Cumming									Me	thod		2.0%	
Summary					Chatt				and the second second	Stations		2.3%	-
Averaging Int. Start Edge			30		Stations		22		-	rall		3.3%	2.5%
			RE		otal Widt	n	20.20						
	IN SNR		29.6		otal Area	h	31.35						
	n Temp	ion	47.17 Mid-So		lean Dept lean Velo		1.552 0.3919						
DISC	ch. Equat	1011	Mid-Se		otal Dis		0.3919 12.285						
Me	asurem	ent R	esulte										
St	asuren Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrFa	No. of Concession, name	MeanV	Area	Flow	%0
St 0	Clock 10:30	Loc 1.00	Method None	0.000	0.0	0.0	0.0000		1.00	0.0000	0.000	0.000	0 0
St 0	Clock 10:30 10:30	Loc 1.00 2.00	Method None 0.6	0.000	0.0	0.0 0.320	0.0000		1.00	0.0000	0.000	0.000	0 0
0 1 2	Clock 10:30 10:30 10:31	Loc 1.00 2.00 3.00	Method None 0.6 0.6	0.000 0.800 1.350	0.0 0.6 0.6	0.0 0.320 0.540	0.0000 0.1430 0.2835		1.00 1.00 1.00	0.0000 0.1430 0.2835	0.000 0.800 1.350	0.000 0.114 0.382	0 0 4 0 7 3
0 1 2 3	Clock 10:30 10:30 10:31 10:32	Loc 1.00 2.00 3.00 4.00	Method None 0.6 0.6 0.6	0.000 0.800 1.350 1.430	0.0 0.6 0.6 0.6	0.0 0.320 0.540 0.572	0.0000 0.1430 0.2835 0.3301		1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301	0.000 0.800 1.350 1.430	0.000 0.114 0.382 0.472	0 0 4 0 7 3 0 3
St 0 1 2 3 4	Clock 10:30 10:30 10:31 10:32 10:34	Loc 1.00 2.00 3.00 4.00 5.00	Method None 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.430 1.620	0.0 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648	0.0000 0.1430 0.2835 0.3301 0.4386		1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386	0.000 0.800 1.350 1.430 1.620	0.000 0.114 0.382 0.472 0.710	0 0 4 0 7 3 0 3 6 5
St 0 1 2 3 4 5	Clock 10:30 10:30 10:31 10:32 10:34 10:35	Loc 1.00 2.00 3.00 4.00 5.00 6.00	Method None 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.430 1.620 1.650	0.0 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875		1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875	0.000 0.800 1.350 1.430 1.620 1.650	0.000 0.114 0.382 0.472 0.710 0.804	0 0 4 0 7 3 0 3 6 5 4 6
St 0 1 2 3 4	Clock 10:30 10:30 10:31 10:32 10:34	Loc 1.00 2.00 3.00 4.00 5.00	Method None 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.430 1.620 1.650 1.700	0.0 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115		1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115	0.000 0.800 1.350 1.430 1.620 1.650 1.700	0.000 0.114 0.382 0.472 0.710 0.804 0.869	0 0 4 0 7 3 0 3 6 5 4 6 6 7
St 0 1 2 3 4 5 6	Clock 10:30 10:31 10:32 10:34 10:35 10:36	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00	Method None 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.430 1.620 1.650	0.0 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875		1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875	0.000 0.800 1.350 1.430 1.620 1.650	0.000 0.114 0.382 0.472 0.710 0.804	0 0 4 0 7 3 0 3 6 5 4 6 7 0 8
St 0 1 2 3 4 5 6 7	Clock 10:30 10:31 10:32 10:34 10:35 10:36 10:37	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680 0.704	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790	0.000 0.114 0.382 0.472 0.710 0.804 0.869 1.030	0 0 4 0 7 3 0 3 6 5 4 6 6 7 6 7 0 8 8 8 8 8 5 9
St 0 1 2 3 4 5 6 7 8 9 10	Clock 10:30 10:31 10:32 10:34 10:35 10:36 10:37 10:38 10:39 10:41	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.620 1.650 1.700 1.760 1.800 1.790 1.600	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680 0.704 0.720 0.716 0.640	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600	0.000 0.114 0.382 0.472 0.710 0.804 0.869 1.030 1.071 1.150 0.990	0 0 4 0 7 3 0 3 6 5 4 6 6 7 0 8 8 8 8 5 9 6 8
St 0 1 2 3 4 5 6 7 7 8 9 10 11	Clock 10:30 10:31 10:32 10:34 10:35 10:36 10:37 10:38 10:39 10:41 10:42	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680 0.704 0.720 0.716 0.640 0.680	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700	0.000 0.114 0.382 0.472 0.710 0.804 0.869 1.030 1.071 1.150 0.990 0.905	0 0 4 0 7 3 0 3 6 5 4 6 6 7 0 3 8 8 5 9 6 8 5 9 6 8 3 7
St 0 1 2 3 4 5 6 7 7 8 9 10 11 12	Clock 10:30 10:30 10:31 10:32 10:34 10:35 10:36 10:37 10:38 10:39 10:41 10:42 10:43	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700 1.860	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680 0.704 0.720 0.716 0.640 0.680 0.744	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700 1.800	0.000 0.114 0.382 0.472 0.710 0.804 0.869 1.030 1.071 1.150 0.990 0.905 0.835	0 0 4 0 7 3 0 3 6 5 4 6 7 6 7 0 8 8 8 8 5 9 6 8 5 9 6 8 3 7 4 6 6 7 7 0 8 8 8 8 9 7 6 8 8 8 8 8 9 7 6 8 8 8 9 7 6 8 8 8 9 7 6 8 8 8 8 8 9 7 6 8 8 8 8 8 8 8 9 7 6 8 8 8 8 8 9 7 6 8 8 8 8 8 8 8 8 8 8 8 9 7 6 8 8 8 8 8 8 8 8 8 8 8 9 9 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
St 0 1 2 3 4 5 6 7 8 9 10 11 11 12 13	Clock 10:30 10:30 10:31 10:32 10:34 10:35 10:36 10:37 10:38 10:39 10:41 10:42 10:43 10:44	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700 1.800 2.000	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680 0.704 0.720 0.716 0.640 0.680 0.744 0.800	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491 0.4501		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491 0.4501	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700 1.860 2.000	0.000 0.114 0.382 0.472 0.710 0.804 0.869 1.030 1.071 1.150 0.990 0.905 0.835 0.900	0 0 4 0 7 3 0 3 6 5 4 6 6 7 0 3 8 8 8 8 5 9 6 8 3 7 4 6 3 7 4 6 3 7
St 0 1 2 3 4 5 6 7 7 8 9 10 11 12 13 14	Clock 10:30 10:30 10:31 10:32 10:34 10:35 10:36 10:37 10:38 10:39 10:41 10:42 10:43 10:44 10:45	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700 1.800 1.700 1.860 2.000 1.800	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680 0.704 0.720 0.716 0.640 0.680 0.744 0.800 0.720	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491 0.4501 0.4088		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491 0.4501 0.4088	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700 1.800 1.800 1.800	0.000 0.114 0.382 0.472 0.710 0.804 0.869 1.030 1.071 1.150 0.990 0.905 0.835 0.900 0.735	0 0 7 3 0 3 6 5 4 6 6 7 0 3 8 8 8 5 9 6 8 8 5 9 6 8 8 3 7 4 6 3 7 4 6 3 7 8 6
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 15	Clock 10:30 10:31 10:32 10:34 10:35 10:36 10:37 10:38 10:39 10:41 10:42 10:43 10:44 10:45 10:46	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700 1.860 2.000 1.800 1.720	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680 0.704 0.720 0.716 0.640 0.680 0.744 0.800 0.720 0.720 0.720	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491 0.4501 0.4088 0.3074		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491 0.4501 0.4088 0.3074	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.700 1.600 1.700 1.800 1.700 1.800 1.800 1.800 1.800 1.800 1.800 1.720	0.000 0.114 0.382 0.472 0.710 0.804 0.869 1.030 1.071 1.150 0.990 0.905 0.835 0.900 0.735 0.528	0 0 4 0 7 3 0 3 6 5 4 6 6 7 0 3 8 8 8 8 5 9 6 8 3 7 4 6 3 7 4 6 3 7 8 6 8 4
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	Clock 10:30 10:31 10:32 10:34 10:35 10:36 10:37 10:38 10:39 10:41 10:42 10:43 10:44 10:45 10:46 10:47	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700 1.860 2.000 1.800 1.720 1.570	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680 0.704 0.720 0.716 0.640 0.680 0.744 0.800 0.720 0.720 0.688 0.628	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491 0.4501 0.4088 0.3074 0.3094		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491 0.4501 0.4088 0.3074 0.3094	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700 1.860 2.000 1.800 1.720 1.570	0.000 0.114 0.382 0.472 0.710 0.804 0.869 1.030 1.071 1.150 0.990 0.905 0.835 0.900 0.735 0.528 0.485	0 0 4 0 7 3 0 3 6 5 4 6 6 7 0 3 8 8 8 8 5 9 6 8 8 5 9 6 8 8 3 7 4 6 3 7 4 6 3 7 4 6 8 8 8 4 7 4 7 4
St 0 0 1 2 3 4 5 6 7 7 8 9 10 11 12 13 14 15 16 17 17	Clock 10:30 10:31 10:32 10:34 10:35 10:36 10:37 10:38 10:39 10:41 10:42 10:43 10:44 10:45 10:46 10:47 10:48	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.620 1.650 1.700 1.760 1.700 1.600 1.700 1.600 1.700 1.800 1.700 1.800 1.720 1.500	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680 0.704 0.720 0.716 0.640 0.680 0.744 0.800 0.720 0.688 0.628 0.600	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491 0.4501 0.4501 0.4088 0.3074 0.3094 0.1749		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.6427 0.6191 0.5325 0.4491 0.4501 0.4088 0.3074 0.3094 0.1749	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.700 1.600 1.790 1.600 1.700 1.800 1.700 1.800 1.720 1.570 1.500	0.000 0.114 0.382 0.472 0.710 0.804 0.869 1.030 1.071 1.150 0.990 0.905 0.835 0.900 0.735 0.528 0.485 0.262	0 0 4 0 7 3 0 3 6 5 4 6 6 7 0 3 8 8 8 9 9 6 8 8 9 9 6 8 3 7 4 6 3 7 4 6 3 7 4 6 8 8 9 9 6 8 8 9 9 6 8 8 9 7 7 3 7 7 3 8 8 8 9 9 6 8 8 9 7 7 8 8 8 9 7 7 8 8 8 9 7 7 8 8 8 8 9 7 7 3 8 8 8 9 7 7 8 8 8 8 9 7 7 4 8 8 8 8 8 8 9 7 7 4 8 8 8 8 9 7 7 4 8 8 8 8 9 7 7 4 8 8 8 8 8 8 9 7 7 4 8 8 8 8 9 7 7 4 8 8 8 8 9 7 7 4 8 8 8 8 8 8 9 7 7 4 8 8 8 8 8 8 8 8 8 8 9 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	Clock 10:30 10:30 10:31 10:32 10:34 10:35 10:36 10:37 10:38 10:39 10:41 10:42 10:43 10:44 10:45 10:46 10:47 10:48 10:49	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700 1.800 1.700 1.800 1.720 1.570 1.500 1.520	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680 0.704 0.720 0.716 0.640 0.680 0.744 0.800 0.720 0.688 0.628 0.628 0.600 0.608	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491 0.4501 0.4501 0.4088 0.3074 0.3094 0.1749 0.0922		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.6427 0.6191 0.5325 0.4491 0.4501 0.4088 0.3074 0.3094 0.1749 0.0922	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.800 1.790 1.600 1.700 1.860 2.000 1.800 1.720 1.570 1.520	0.000 0.114 0.382 0.472 0.710 0.804 0.869 1.030 1.071 1.150 0.990 0.905 0.835 0.900 0.735 0.528 0.485 0.262 0.140	0 0 4 0 7 3 0 3 6 5 4 6 6 7 0 3 8 8 8 8 5 9 6 8 8 3 7 4 6 3 7 4 6 3 7 8 6 8 4 7 4 2 3 2 1 1
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	Clock 10:30 10:31 10:32 10:34 10:35 10:36 10:37 10:38 10:39 10:41 10:42 10:43 10:44 10:45 10:46 10:47 10:48	Loc 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.800 1.350 1.620 1.650 1.700 1.760 1.700 1.600 1.700 1.600 1.700 1.800 1.700 1.800 1.720 1.500	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.320 0.540 0.572 0.648 0.660 0.680 0.704 0.720 0.716 0.640 0.680 0.744 0.800 0.720 0.688 0.628 0.600	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.4491 0.4501 0.4501 0.4088 0.3074 0.3094 0.1749		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.0000 0.1430 0.2835 0.3301 0.4386 0.4875 0.5115 0.5853 0.5955 0.6427 0.6191 0.5325 0.6427 0.6191 0.5325 0.4491 0.4501 0.4088 0.3074 0.3094 0.1749	0.000 0.800 1.350 1.430 1.620 1.650 1.700 1.760 1.700 1.600 1.790 1.600 1.700 1.800 1.700 1.800 1.720 1.570 1.500	0.000 0.114 0.382 0.472 0.710 0.804 0.869 1.030 1.071 1.150 0.990 0.905 0.835 0.900 0.735 0.528 0.485 0.262	0 0. 4 0. 7 3 0 3. 6 5. 4 6. 6 7. 0 3. 8 8 8 9 9 9 6 8 3 7 4 6 3 7 4 7 4 7 4 7 4 7 4 7 4 7 4 7 4

File	e Inform Name rt Date an			C9US.920.WAD 2011/09/21 16:24:08			Site Details Site Name Operator(s) NJT					
Sy	stem In	format	tion		U	nits (English U	nits) D	Discharge Uncertainty			
Sen	sor Type			FlowTrac	ker Di	stance	ft		Category	IS	ISO St	
	ial #			P3012		locity			Accuracy		1.0%	1.0
-	J Firmwai	2 2 2 2 1 2 1	n				ft^2	D	epth		0.4%	2.8
C	tware Ver			2.30	Di	scharge	cfs	Ve	locity		0.8%	5.0
Mo	unting Co	rrection	1/1-1-1-D-1-1-0-0-35	0.0%				V	idth		0.1%	0.1
Cu	mmary	and the second s				a da antiga		M	ethod	1	1.9%	
Averaging Int.			30	4	Stations		22	#	Stations		2.3%	
Start Edge			REW		otal Width		39.600	0	verall		3.2%	5.80
	an SNR		27.4 (otal Area		26.000	and the second se				
	an Temp		53.91		ean Depth	1	0.657					
	ch. Equat	ion	Mid-Sec		ean Veloci		0.4776					
-					otal Disci		12.417					
-	asurer Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrFact	MeanV	Area	Flow	%
Me St	the second se	of the local division in which the	the survey of the local division in which the local division in which the local division is not the local division in which the local division is not the local division in which the local division is not the local division in which the local division is not the local division in which the local division is not the local division in which the local division is not the local division in which the local division is not the local division is not the local division in which the lo	Depth 0.000	%Dep 0.0	MeasD 0.0	0.0000	CorrFact		0.000	0.000	
0 1	Clock 16:24 16:24	Loc 1.00 <i>3.00</i>	Method None 0.6	0.000	0.0	0.0 0.184	0.0000	1.0 1.0	0 <u>0.0000</u> 7 <i>0.3173</i>	0.000	0.0000	
0 1 2	Clock 16:24 16:24 16:25	Loc 1.00 3.00 5.00	Method Norie 0.6 0.6	0.000 0.460 0.620	0.0 0.6 0.6	0.0 0.184 0.248	0.0000 0.3173 0.6873	1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873	0.000 0.920 1.240	0.0000	0 0 7 2. 4 6
0 1 2 3	Clock 16:24 16:24 16:25 16:26	Loc 1.00 3.00 5.00 7.00	Method None 0.6 0.6 0.6	0.000 0.460 0.620 0.700	0.0 0.6 0.6 0.6	0.0 0.184 0.248 0.280	0.0000 0.3173 0.6873 0.6030	1.0 1.0 1.0 1.0 1.0	0 0.0000 0 0.3173 0 0.6873 0 0.6030	0.000 0.920 1.240 1.050	0.0000 0.2919 0.8524 0.6333	0 0 0 2 2 4 6 3 5
0 1 2 3 4	Clock 16:24 16:25 16:25 16:26 16:27	Loc 1.00 3.00 5.00 7.00 8.00	Method None 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670	0.0 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268	0.0000 0.3173 0.6873 0.6030 0.6667	1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873 0 0.6030 0 0.6667	0.000 0.920 1.240 1.050 0.670	0.0000 0.2919 0.8524 0.6333 0.4460	0 0 2 2 4 6 3 5 6 3
St 0 1 2 3 4 5	Clock 16:24 16:25 16:26 16:27 16:28	Loc 1.00 3.00 5.00 7.00 8.00 9.00	Method Norie 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.700	0.0 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387	1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873 0 0.6030 0 0.6667 0 0.5387	0.000 0.920 1.240 1.050 0.670 1.050	0.0000 0.2919 0.8524 0.6333 0.4466 0.5658	0 0 2 2 4 6 3 5 6 3 8 4
St 0 1 2 3 4 5 6	Clock 16:24 16:25 16:26 16:27 16:28 16:30	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.700 0.550	0.0 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873 0 0.6030 0 0.6667 0 0.5387 0 0.4091	0.000 0.920 1.240 1.050 0.670 1.050 1.100	0.0000 0.2919 0.8524 0.6333 0.4460 0.5658 0.4499	0 0 2 2 4 6 3 5 6 3 8 4 9 3
St 0 1 2 3 4 5 6 7	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.700 0.550 0.670	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873 0 0.6030 0 0.6667 0 0.5387 0 0.4091 0 0.5030	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340	0.000 0.2919 0.8524 0.6333 0.4460 0.5655 0.4469 0.4499 0.6733	0 0 7 2 4 6 3 5 6 3 8 4 9 3 9 5
St 0 1 2 3 4 5 6 7 8	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.700 0.550 0.670 0.670	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268 0.268	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873 0 0.6030 0 0.6667 0 0.5387 0 0.4091 0 0.5030 0 0.5801	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340 1.340	0.0000 0.2919 0.8524 0.6333 0.4460 0.5658 0.4469 0.5658 0.4499 0.6739	0 0 7 2 4 6 3 5 6 3 8 4 9 3 9 5 2 6
St 0 1 2 3 4 5 6 7	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.700 0.550 0.670	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873 0 0.6030 0 0.6667 0 0.5387 0 0.4091 0 0.5030 0 0.5801 0 0.7490	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340	0.000 0.2919 0.8524 0.6333 0.4460 0.5655 0.4469 0.4499 0.6733	0 0 7 2 4 6 3 5 5 6 3 8 4 9 3 9 5 2 6 6 8
St 0 1 2 3 4 5 6 7 8 9	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.670	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268 0.268 0.268	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 0 0.3173 0 0.6873 0 0.6030 0 0.6667 0 0.5387 0 0.4091 0 0.5030 0 0.5801 0 0.7490 0 0.5768 0 0.2064	0.000 0.920 1.240 1.050 1.050 1.100 1.340 1.340 1.340	0.0000 0.2915 0.852 0.633 0.4460 0.5658 0.4499 0.673 0.777 1.003 0.777 1.003	0 0 7 2 4 6 3 5 6 3 8 4 9 3 9 5 2 6 8 8 6 8 6 8 6 8 6 5 4 2
St 0 1 2 3 4 5 6 7 8 9 10 11 12	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.630 0.820 0.520	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268 0.268 0.268 0.268 0.252 0.328 0.208	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952	1.0 <i>1.0</i> 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 0 0.3173 0 0.6873 0 0.6030 0 0.6667 0 0.5387 0 0.4091 0 0.5030 0 0.5030 0 0.5801 0 0.7490 0 0.5768 0 0.2064 0 0.1952	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340 1.340 1.340 1.260	0.0000 0.2915 0.8522 0.6333 0.4460 0.5658 0.4499 0.6733 0.777 1.0030 0.7260 0.338 0.2030	0 0 2 2 4 6 3 55 6 3 8 4 9 3 5 5 2 6 8 4 9 5 2 6 6 55 6 5 6 2 6 8 6 5 4 2 0 1
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 13	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.550 0.670 0.670 0.670 0.630 0.820 0.520 0.600	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.228	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873 0 0.6030 0 0.6030 0 0.6667 0 0.5387 0 0.4091 0 0.5030 0 0.5030 0 0.5801 0 0.7490 0 0.5768 0 0.2064 0 0.1952 7 0.2628	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340 1.340 1.340 1.260 1.640 1.040 1.200	0.0000 0.2919 0.8522 0.6333 0.4460 0.5658 0.4499 0.6733 0.777 1.0030 0.777 1.0030 0.7260 0.338 0.2030	0 0 0 0 2 2 4 6 3 55 6 33 5 3 6 3 9 5 2 6 8 4 9 5 6 8 6 5 6 8 6 5 6 8 6 5 6 8 6 5 6 8 6 5 7 2 6 8 6 5 7 2 7 2 7 2 7 2 7 2 8 4 2
St 0 1 2 3 4 5 6 7 8 9 10 11 12 12 13 14 14	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40 16:41	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.670 0.670 0.670 0.670 0.630 0.820 0.520 0.600 0.680	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.220 0.328 0.208 0.240 0.272	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873 0 0.6030 0 0.6667 0 0.5387 0 0.4091 0 0.5030 0 0.5801 0 0.7490 0 0.5768 0 0.2064 0 0.1952 7 0.2628 7 0.3337	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360	0.0000 0.2919 0.8524 0.633 0.4460 0.5658 0.4499 0.6739 0.7777 1.0030 0.7260 0.3384 0.2033 0.3154 0.4539	0 0 0 2 4 66 3 5 6 3 8 4 9 3 9 5 2 6 8 4 2 6 6 8 6 5 4 2 0 1 4 2 9 3
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 15	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40 16:41 16:42	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00 29.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.670 0.670 0.670 0.670 0.630 0.820 0.520 0.600 0.680 0.970	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.220 0.328 0.208 0.240 0.272 0.388	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873 0 0.6030 0 0.6067 0 0.5387 0 0.4091 0 0.5030 0 0.5030 0 0.5801 0 0.7490 0 0.5768 0 0.2064 0 0.1952 7 0.2628 7 0.3337 0 0.5092	0.000 0.920 1.240 1.050 0.670 1.050 1.100 1.340 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360 1.940	0.0000 0.2919 0.8524 0.633 0.4460 0.56550 0.4499 0.6739 0.7777 1.0030 0.7260 0.3384 0.2030 0.3154 0.4539 0.9880	0 0 0 0 0 2 4 66 3 55 6 3 9 3 9 5 2 66 8 4 2 66 6 8 6 5 6 8 6 5 6 8 6 7 7 3 0 8
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	Clock 16:24 16:25 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40 16:41 16:42 16:43	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00 29.00 31.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.670 0.670 0.670 0.670 0.630 0.820 0.520 0.600 0.680 0.970 1.050	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.280 0.220 0.268 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.220 0.228 0.228 0.228 0.228 0.228 0.238 0.240 0.272 0.388 0.420	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873 0 0.6030 0 0.6667 0 0.5387 0 0.4091 0 0.5030 0 0.5801 0 0.7490 0 0.5768 0 0.2064 0 0.1952 7 0.2628 7 0.3337 0 0.5092 0 0.4984	0.000 0.920 1.240 1.050 1.050 1.050 1.050 1.340 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360 1.940 2.100	0.0000 0.2919 0.8522 0.633 0.4460 0.5658 0.4499 0.6739 0.777 1.0030 0.7260 0.338 0.2033 0.3154 0.4539 0.9880 1.0464	0 0 0 0 0 2 4 6 3 55 6 3 8 4 9 3 9 55 2 66 8 6 5 2 6 8 6 5 4 2 7 3 0 8 4 8
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 16	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40 16:41 16:42 16:43 16:44	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00 29.00 31.00 33.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.670 0.670 0.670 0.670 0.670 0.630 0.820 0.520 0.680 0.520 0.680 0.970 1.050 0.900	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.220 0.268 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.220 0.328 0.208 0.240 0.272 0.388 0.420 0.360	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984 0.6644	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 7 0.3173 0 0.6873 0 0.6030 0 0.6667 0 0.5387 0 0.4091 0 0.5030 0 0.5801 0 0.7490 0 0.5768 0 0.2064 0 0.1952 7 0.2628 7 0.3337 0 0.5092 0 0.4984 0 0.6644	0.000 0.920 1.240 1.050 1.050 1.050 1.340 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360 1.940 2.100 1.800	0.0000 0.2919 0.852 0.633 0.4460 0.5658 0.4499 0.6739 0.777 1.0030 0.7260 0.338 0.2030 0.315 0.2030 0.315 0.4539 0.9880 1.046 1.1950	D 0 0 Q 2 2 0 A4 6 3 5 5 S 5 5 5 5 S 6 5 5 6 8 G 8 9 3 5 5 6 6 5 5 6 6 5 5 6 6 5 5 6 6 5 5 6 6 5 5 6 6 5 7 7 3 7 7 3 7 7 3 7 7 3 7 7 3 7 7 3 7 7 3 7 7 3 7 7 3 7 7 3 7 7 7 3 7 7 3 7 7 3 3 7 7 3 3 3 3 3 3 3
St 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40 16:41 16:42 16:43 16:44 16:44 16:45	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00 29.00 31.00 33.00 35.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.670 0.670 0.670 0.670 0.630 0.820 0.520 0.660 0.680 0.970 1.050 0.900 0.800	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.220 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.220 0.328 0.208 0.272 0.388 0.272 0.388 0.220	0.0000 0.3173 0.6873 0.6030 0.5030 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984 0.6644 0.5066	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 0 0.3173 0 0.6873 0 0.6030 0 0.6030 0 0.6067 0 0.5387 0 0.4091 0 0.5030 0 0.5030 0 0.5801 0 0.7490 0 0.5768 0 0.2064 0 0.1952 7 0.2628 7 0.3337 0 0.5092 0 0.4984 0 0.6644 0 0.5066	0.000 0.920 1.240 1.050 1.050 1.050 1.340 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360 1.940 2.100 1.800 1.600	0.0000 0.2919 0.8524 0.633 0.4460 0.56550 0.4499 0.6739 0.7777 1.0030 0.7260 0.3384 0.2030 0.3154 0.4539 0.2030 0.3154 0.4539 0.9880 1.0460 1.1950 0.810	D 0 0 Q 2 2 0 A4 6 3 5 5 S 5 5 6 8 4 O 3 5 5 6 8 6 5 5 6 6 8 6 5 5 6 6 8 6 5 5 6 6 8 6 5 5 6 6 8 6 5 5 7 7 3 7 7 3 7 7 3 7 7 3 7 7 3 7 7 7 3 7 7 3 7 7 3 7 7 3 3 7 7 3
St 0 1 2 3 4 5 6 7 7 8 9 10 11 12 13 14 15 16	Clock 16:24 16:25 16:26 16:27 16:28 16:30 16:31 16:32 16:33 16:36 16:37 16:38 16:40 16:41 16:42 16:43 16:44	Loc 1.00 3.00 5.00 7.00 8.00 9.00 11.00 13.00 15.00 17.00 19.00 21.00 23.00 25.00 27.00 29.00 31.00 33.00	Method None 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.000 0.460 0.620 0.700 0.670 0.670 0.670 0.670 0.670 0.670 0.630 0.820 0.520 0.680 0.520 0.680 0.970 1.050 0.900	0.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.0 0.184 0.248 0.280 0.268 0.220 0.268 0.268 0.268 0.268 0.268 0.252 0.328 0.208 0.220 0.328 0.208 0.240 0.272 0.388 0.420 0.360	0.0000 0.3173 0.6873 0.6030 0.6667 0.5387 0.4091 0.5030 0.5801 0.7490 0.5768 0.2064 0.1952 0.2628 0.3337 0.5092 0.4984 0.6644	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 0.0000 0 0.3173 0 0.6873 0 0.6030 0 0.6030 0 0.6067 0 0.5387 0 0.4091 0 0.5030 0 0.5030 0 0.5801 0 0.7490 0 0.5768 0 0.2064 0 0.1952 7 0.2628 7 0.3337 0 0.5092 0 0.4984 0 0.6644 0 0.5066 0 0.5348	0.000 0.920 1.240 1.050 1.050 1.050 1.050 1.340 1.340 1.340 1.340 1.260 1.640 1.040 1.200 1.360 1.940 2.100 1.800	0.0000 0.2919 0.852 0.633 0.4460 0.5658 0.4499 0.6739 0.777 1.0030 0.7260 0.338 0.2030 0.315 0.2030 0.315 0.4539 0.9880 1.046 1.1950	D 0 0 D 0 0 0 D 2 2 0 33 5 5 3 5 5 3 5 5 5 5 5 5 5 5 5 5 5 5 5 6 8 9 3 3 9 3 3 5 5 6 8 9 3 3 9 3 3 5 5 9 3 3 5 5 9 3 3 5 5 9 3 3 5 5 9 3 3 5 5 9 3 3 5 5 9 3 4 6 5 9 3 4 6 5

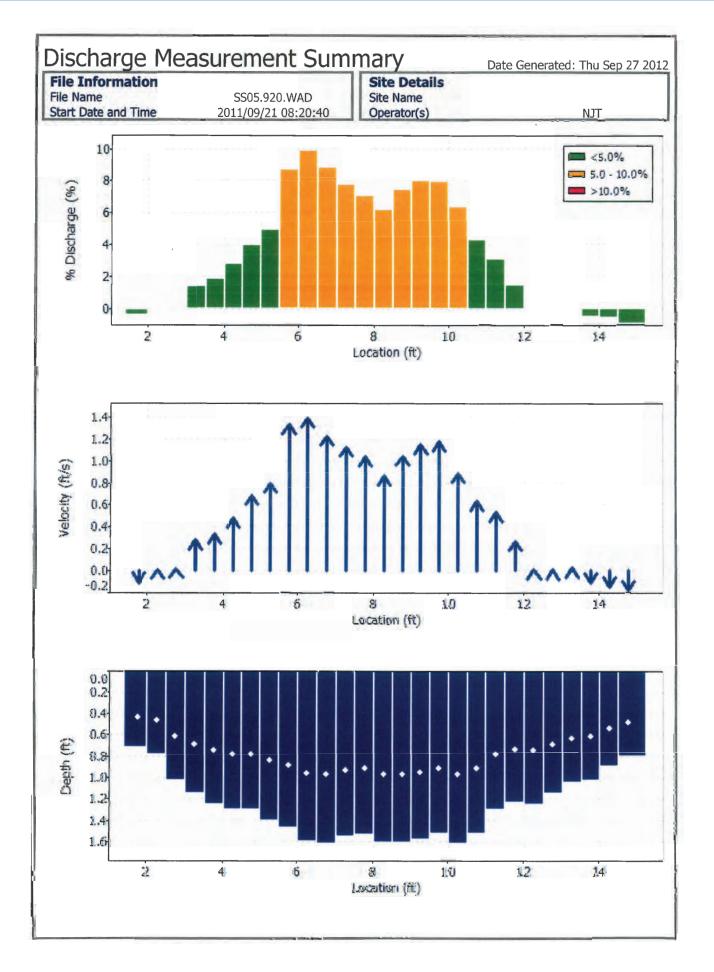
File	e Inform Name t Date an				.920.WAD 21 15:38:		Site Det Site Name Operator(s	1			N	<u></u>	_	
Sys	tem In	forma	tion		U	nits	(English U	nits)	Dis	Discharge Uncertainty				
	sor Type			- lowTracl	ker Di	stance	ft		-	Category			Stats	
Seri	al #			P3012	Ve	elocity	ft/s	- 1		uracy		1.0%	1,09	
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	ware Ver			2.30	Di	scharge	cfs		Velo	NAMES OF TAXABLE PARTY.		0.9%	3.79	
Mou	inting Co	rrection	u 1	0.0%					Wid			0.1%	0.14	
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	nmary			CLUB .				the state of the s	tations	1	2.0%			
	veraging Int. 30 # Stat						25			erall	-	3.1%	4.49	
	t Edge		REW		tal Width		30.400		0.70					
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-	_	a manufacture of		10	otal Disc	narge	10.123	8						
	asurem	ent Re	esults			200 PACE								
_	Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrF		MeanV	Area	Flow	%	
0	15:38	5.00	None	0.000	0.0	0.0	of the local division in which the local division in which the local division is not the local division of the local division in the		1.00	0.0000	0.000	0.000		
1	15:38	6.50	0.6	0.500	0.6	0.200			1.00	0.2822	0.750	0.211		
2	15:39 15:41	8.00	0.6	0.920	0.6	0.368			1.00	0.4140	1.150	0.476		
	12:41	9.00	0.6	1.050	0.6	04/0			1.00	0.0000	1.050	0.594		
3		10.00	0.6								and the second se			
4	15:42	10.00	0.6	1.100	0.6	0.440	0.5203	-	1.00	0.5203	1.100	0.572		
4	15:42 15:43	11.00	0.6	1.100	0.6	0.440	0.5203		1.00	0.5203	1.100	0.572	8 6	
456	15:42 15:43 15:44	11.00 12.00	0.6 0.6	1.100 1.250 1.250	0.6 0.6 0.6	0.440 0.500 0.500	0.5203 0.5463 0.5840		1.00 1.00 1.00	0.5203 0.5463 0.5840	1.100 1.250 1.250	0.572 0.682 0.730	8 6	
4 5 6 7	15:42 15:43 15:44 15:45	11.00 12.00 13.00	0.6 0.6 0.6	1.100 1.250 1.250 1.220	0.6 0.6 0.6 0.6	0.440 0.500 0.500 0.488	0.5203 0.5463 0.5840 0.6877		1.00 1.00 1.00 1.00	0.5203 0.5463 0.5840 0.6877	1.100 1.250 1.250 1.220	0.572 0.682 0.730 0.839	8 6 0 7 0 8	
4 5 6 7 8	15:42 15:43 15:44 15:45 15:46	11.00 12.00 13.00 14.00	0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220	0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.500 0.488 0.488	0.5203 0.5463 0.5840 0.6877 0.3957		1.00 1.00 1.00 1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957	1.100 1.250 1.250 1.220 1.220	0.572 0.682 0.730 0.839 0.482	8 6 0 7 0 8 8 4	
4 5 6 7 8 9	15:42 15:43 15:44 15:45 15:46 15:47	11.00 12.00 13.00 14.00 15.00	0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.220	0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.500 0.488 0.488 0.488	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016		1.00 1.00 1.00 1.00 1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016	1.100 1.250 1.250 1.220 1.220 1.220	0.572 0.682 0.730 0.839 0.482 0.490	8 6 0 7 0 8 8 4 0 4	
4 5 6 7 8 9 10	15:42 15:43 15:44 15:45 15:46 15:47 15:48	11.00 12.00 13.00 14.00 15.00 16.00	0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.220 1.220 1.300	0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.500 0.488 0.488 0.488 0.520	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409		1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409	1.100 1.250 1.250 1.220 1.220 1.220 1.220 1.300	0.572 0.682 0.730 0.839 0.482 0.490 0.573	8 6 0 7 0 8 8 4 0 4 2 5	
4 5 6 7 8 9 10 11	15:42 15:43 15:44 15:45 15:46 15:47 15:48 15:49	11.00 12.00 13.00 14.00 15.00 16.00 <i>17.00</i>	0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i>	0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.500 0.488 0.488 0.488 0.488 0.520 0.440	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293		1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293	1.100 1.250 1.220 1.220 1.220 1.220 1.220 1.300 1.100	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252	8 6 0 7 0 8 8 4 0 4 2 5 3 2	
4 5 6 7 8 9 10 11 12	15:42 15:43 15:44 15:45 15:46 15:47 15:48	11.00 12.00 13.00 14.00 15.00 16.00	0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.220 1.220 1.300	0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.500 0.488 0.488 0.488 0.520 0.440 0.248	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175	1.100 1.250 1.220 1.220 1.220 1.220 1.300 1.100 0.620	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252 0.134	8 6 0 7 0 8 8 4 0 4 2 5 3 2 9 1.	
4 5 6 7 8 9 10 11	15:42 15:43 15:44 15:45 15:46 15:47 15:48 15:49 15:50	11.00 12.00 13.00 14.00 15.00 16.00 <i>17.00</i> <i>18.00</i>	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.220 1.220 1.220 1.200 <i>0.620</i>	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.500 0.488 0.488 0.488 0.488 0.520 0.440	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553		1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553	1.100 1.250 1.220 1.220 1.220 1.220 1.220 1.300 1.100	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252	8 6 0 7 0 8 4 0 4 2 5 3 9 1 6 1	
4 5 6 7 8 9 10 11 12 13 14	15:42 15:43 15:44 15:45 15:46 15:47 15:48 15:49 15:50 15:52	11.00 12.00 13.00 14.00 15.00 16.00 <i>17.00</i> <i>18.00</i> 19.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.400	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.500 0.488 0.488 0.488 0.520 0.440 0.248 0.160	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175	1.100 1.250 1.250 1.220 1.220 1.220 1.300 1.100 0.620 0.500	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252 0.134 0.177	8 6 0 7 0 8 4 0 42 5 3 2 9 1 6 1 6 5	
4 5 6 7 8 9 10 11 12 13 14 15 16	15:42 15:43 15:44 15:45 15:46 15:47 15:48 <i>15:49</i> <i>15:50</i> 15:52 15:53 15:54 15:55	11.00 12.00 13.00 14.00 15.00 16.00 <i>17.00</i> <i>18.00</i> 19.00 20.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.400 0.600	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.500 0.488 0.488 0.488 0.520 0.440 0.248 0.160 0.240	0.5203 0.5463 0.5840 0.6877 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901	1.100 1.250 1.250 1.220 1.220 1.220 1.300 <i>1.100</i> <i>0.620</i> 0.500 0.900	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252 0.134 0.177 0.518	8 6 0 7 0 8 4 4 10 4 12 5 3 2 9 1 16 5 11 7	
4 5 6 7 8 9 10 11 12 13 14 15 16	15:42 15:43 15:44 15:45 15:46 15:47 15:48 15:49 15:50 15:52 15:53 15:54 15:55 15:55	11.00 12.00 13.00 14.00 15.00 16.00 <i>17.00</i> 18.00 19.00 20.50 22.00 23.50 25.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.300 <i>1.100 0.620</i> 0.400 0.600 0.650 0.650 0.500	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.488 0.488 0.488 0.520 0.440 0.248 0.160 0.240 0.260 0.260 0.200	0.5203 0.5463 0.5840 0.6877 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901		1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238	1.100 1.250 1.250 1.220 1.220 1.220 1.300 1.100 0.620 0.500 0.900 0.975	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252 0.134 0.177 0.518 0.803	8 6 0 7 0 8 4 0 4 2 5 3 3 2 9 1 6 1 6 5 11 7 8 8 26 7	
4 5 6 7 9 10 11 12 13 14 15 16 17 18	15:42 15:43 15:44 15:45 15:46 15:47 15:48 15:49 15:50 15:52 15:53 15:54 15:55 15:55 15:56 15:57	11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 20.50 22.00 23.50 25.00 26.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.300 <i>1.100 0.620</i> 0.400 0.650 0.650 0.650 0.500 <i>0.430</i>	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.488 0.488 0.488 0.520 0.440 0.248 0.160 0.240 0.260 0.260 0.200 0.172	0.5203 0.5463 0.5840 0.6877 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047		1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8201 0.9902 0.7047	1.100 1.250 1.220 1.220 1.220 1.220 1.300 <i>0.620</i> 0.500 0.900 0.975 0.975 0.750 <i>0.645</i>	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252 0.134 0.177 0.518 0.803 0.867 0.742 0.454	8 6 0 7 0 8 4 0 4 2 5 3 3 2 9 1 6 1 6 5 11 7 8 8 16 7 7 4	
4 5 6 7 10 11 12 13 14 15 16 17 18 19	15:42 15:43 15:44 15:45 15:46 15:47 15:48 15:49 15:50 15:52 15:53 15:54 15:55 15:56 15:57 15:58	11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 20.50 22.00 23.50 25.00 26.50 28.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.300 1.100 0.620 0.400 0.650 0.650 0.650 0.650 0.500 0.430 0.300	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.488 0.488 0.488 0.520 0.440 0.248 0.160 0.240 0.260 0.260 0.260 0.200 0.172 0.120	0.5203 0.5463 0.5840 0.6877 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047 0.5791		1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047 0.5791	1.100 1.250 1.220 1.220 1.220 1.220 1.300 0.620 0.500 0.900 0.975 0.975 0.750 0.645 0.450	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252 0.134 0.177 0.518 0.803 0.867 0.742 0.454	8 6 0 7 0 8 4 0 4 2 3 2 9 1 16 5 511 7 7 4 15 2	
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	15:42 15:43 15:44 15:45 15:46 15:47 15:48 15:49 15:50 15:52 15:53 15:54 15:55 15:56 15:57 15:58 15:59	11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 20.50 22.00 23.50 25.00 26.50 28.00 29.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.300 1.100 0.620 0.400 0.650 0.650 0.650 0.650 0.500 0.430 0.300 0.330	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.488 0.488 0.488 0.520 0.440 0.248 0.160 0.240 0.260 0.260 0.260 0.200 0.172 0.120 0.132	0.5203 0.5463 0.5840 0.6877 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047 0.5791 0.2339		1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047 0.5791 0.2339	1.100 1.250 1.220 1.220 1.220 1.220 1.300 0.620 0.500 0.900 0.975 0.975 0.975 0.750 0.645 0.450 0.495	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252 0.134 0.177 0.518 0.803 0.867 0.742 0.454 0.260 0.115	8 6 0 7 0 8 4 4 2 5 3 2 9 1 16 5 17 7 8 8 6 7 7 4 15 2 8 1	
4 5 6 7 10 11 12 13 14 15 16 17 18 19 20 21	15:42 15:43 15:44 15:45 15:46 15:47 15:48 15:49 15:50 15:52 15:53 15:54 15:55 15:56 15:55 15:56 15:55 15:58 15:59 16:00	11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 20.50 22.00 23.50 25.00 26.50 28.00 29.50 31.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.220 1.300 1.100 0.620 0.400 0.650 0.650 0.650 0.650 0.500 0.430 0.330 0.330	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.488 0.488 0.488 0.520 0.440 0.248 0.160 0.240 0.260 0.260 0.260 0.260 0.200 0.172 0.120 0.132	0.5203 0.5463 0.5840 0.6877 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047 0.5791 0.2339 0.2320		1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047 0.5791 0.2339 0.2320	1.100 1.250 1.220 1.220 1.220 1.220 1.300 1.100 0.620 0.500 0.900 0.975 0.975 0.975 0.750 0.645 0.450 0.495 0.495	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252 0.134 0.177 0.518 0.803 0.867 0.742 0.454 0.260 0.115 0.114	8 6 0 7 0 8 4 0 4 2 3 2 9 1 6 5 11 7 8 8 6 7 7 4 15 2 8 1	
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	15:42 15:43 15:44 15:45 15:46 15:47 15:48 15:49 15:50 15:52 15:53 15:54 15:55 15:55 15:56 15:55 15:58 15:59 16:00 16:02	11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 20.50 22.00 23.50 25.00 26.50 28.00 29.50 31.00 32.50	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.220 1.220 1.300 <i>0.620</i> 0.400 0.650 0.650 0.650 0.650 0.650 0.500 0.430 0.330 0.330 0.330	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.500 0.488 0.488 0.520 0.440 0.248 0.160 0.240 0.260 0.260 0.260 0.260 0.200 0.172 0.120 0.132 0.132	0.5203 0.5463 0.5840 0.6877 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047 0.5791 0.2339 0.2320 0.0472		1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047 0.5791 0.2339 0.2320 0.0472	1.100 1.250 1.220 1.220 1.220 1.220 1.220 1.300 0.620 0.500 0.900 0.975 0.975 0.975 0.750 0.645 0.450 0.495 0.495 0.495	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252 0.134 0.177 0.518 0.803 0.867 0.742 0.454 0.260 0.115 0.114 0.028	8 6 0 7 0 8 4 0 4 2 3 2 9 1 6 5 11 7 8 8 8 6 7 4 15 2 8 1 3 0	
4 5 6 7 1 8 9 10 11 12 13 14 15 16 17 18 19	15:42 15:43 15:44 15:45 15:46 15:47 15:48 15:49 15:50 15:52 15:53 15:54 15:55 15:56 15:55 15:56 15:55 15:58 15:59 16:00	11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 20.50 22.00 23.50 25.00 26.50 28.00 29.50 31.00	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1.100 1.250 1.250 1.220 1.220 1.220 1.300 1.100 0.620 0.400 0.650 0.650 0.650 0.650 0.500 0.430 0.330 0.330	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.440 0.500 0.500 0.488 0.488 0.488 0.520 0.440 0.248 0.160 0.240 0.260 0.260 0.260 0.260 0.200 0.172 0.120 0.132	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047 0.5791 0.2339 0.2320 0.0472 0.0007		1.00 1.00	0.5203 0.5463 0.5840 0.6877 0.3957 0.4016 0.4409 0.2293 0.2175 0.3553 0.5761 0.8238 0.8901 0.9902 0.7047 0.5791 0.2339 0.2320	1.100 1.250 1.220 1.220 1.220 1.220 1.300 1.100 0.620 0.500 0.900 0.975 0.975 0.975 0.750 0.645 0.450 0.495 0.495	0.572 0.682 0.730 0.839 0.482 0.490 0.573 0.252 0.134 0.177 0.518 0.803 0.867 0.742 0.454 0.260 0.115 0.114	8 6 0 7 0 8 4 0 4 2 3 2 9 1 76 1 76 1 76 1 76 2 8 8 16 5 7 4 15 2 8 1 3 0 4 0	



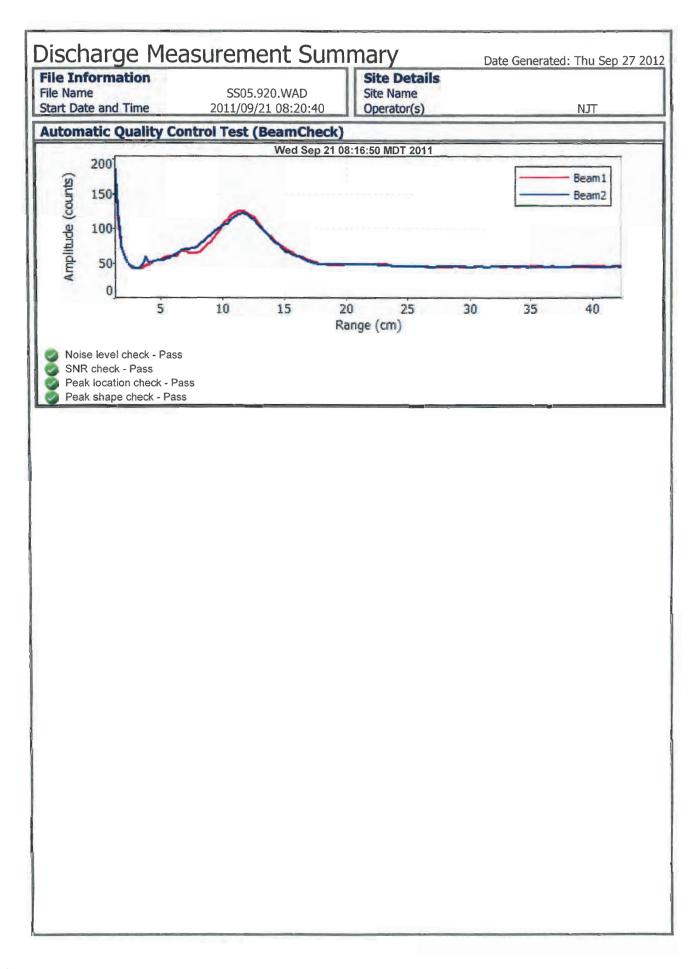
File I	Inform Name Date and		C12US.920.WAD 2011/09/21 15:38:22	NJT	
Qua	lity Con	trol			
St	Loc	%Dep		Message	
11	17.00	0.6	High angle: -21		
12	18.00		High angle: -31 Boundary QC is Good; possible bo	oundary interference	
18	26.50		High angle: -23		
22	32.50	0.6	Boundary QC is Fair; possible bou	indary interference	
	34.00		SNR (60.2) is different from typic		



File	e Infor Name t Date a				5.920.WAI 9/21 08:20		Site De Site Nam Operator	e					
Sys	stem I	nforma	ation			Units	(English L	Jnits)	Discharge Uncertainty				
Sen	sor Type	2		FlowTra	cker	Distance	ft		Category	_	and the owner water of the local division of	tats	
	al #			P301		/elocity	ft/s		Accuracy		1.0%	1.09	
CPL	Firmwa	re Versi	ion	3.7		Area			Depth		0.1%	0.79	
	ware Ve			2.30		Discharge	cfs		Velocity		1.3%	2.5%	
Mou	inting Co	orrection	n	0.0%	6				Width		0.1%	0.19	
-					- ways again and a damage	Marrie Martin	- 10 - 11 - 11 - 11 - 11 - 11 - 11 - 11		Method		2.0%		
	mmary		24				20		# Stations		1.8%		
				# Stations		29		Overall		3.1%	2.89		
	t Edge In SNR				Total Widt		14.70				and the second		
			31.4 45.3		Total Area Mean Dep		17.704 1.204						
Mean Temp Disch. Equation							0.6368						
Disch. Equation			mu-Se	Mid-Section Mean Velocity Total Dischar			11.274						
-					iotal Dis	charge	1112/					-	
Me	asuren	nent R	esults								-	-	
	Clock	Loc	Method	Depth	%Dep	MeasD	Vel	CorrFact	MeanV	Area	Flow	%	
0	08:20	1.00	None			0.0	0.0000	1.		0.000	0.0000	0.	
1	08:20	1.75	0.6	the second day in the second day is not the	0.6	0.288	-0.1076	1.0	-0.1076		-0.0484	Name of Column 2 is not	
2	08:22	2.25	0.6				0.0102	1.			0.0040		
3	08:25	2.75	0.6		0.6	0.412	0.0210	1.0		0.515	0.0108	0.	
4	08:26	3.25	0.6		0.6	0.460	0.2831	1.0		0.575	0.1628		
5	08:28	3.75	0.6	1.250	0.6	0.500	0.3379	1.0			0.2112	1.	
6	08:32	4.25	0.6		0.6	0.520	0.4829	1.0	Name of Street or other Designation of Street or other Designa		0.3139 0.4478		
8	08:37 08:38	5.25	0.6	the second se	0.6	0.520	0.6890	1.	The Party Name of Street, or other Designation of Street, or o		0.4478		
9	08:41	5.75	0.6	and the second se	0.6		1.3356	1.			0.9818	-	
10	08:43	6.25	0.6	1.600	0.6	0.580	1.3957	1.		0.800	1.1166		
11	08:44	6.75	0.6	NAME AND ADDRESS OF TAXABLE PARTY.	0.6	0.648	1.2290	1.			0.9955		
12	08:45	7.25	0.6	the state of the s	0.6	Name of Concession, Name of Street, or other	1.1312	1.			0.8766		
13	08:48	7.75	0.6	1.530	0.6	0.612	1.0407	1.0		0.765	0.7960	7.	
14	08:49	8.25	0.6		0.6		0.8675	1.			0.6983	6	
15	08:51	8.75	0.6		0.6	0.644	1.0453	1.			0.8414		
16	08:52	9.25	0.6		0.6		1.1503	1.			0.9087	8	
17	08:54	9.75	0.6				1.1798	1.			0.8966		
18	08:55	10.25	0.6		0.6	0.648	0.8927	1.0		0.810	0.7231	6.	
19 20	08:56	10.75	0.6	and the second se	0.6	- The subscription of the local division of	0.6411	1.	And in case of the local division in which the local division in which the local division in which the local division in the local din the local division in the local division in the local din the l	the second se	0.4872	-	
20	08:57 08:59	11.25 11.75	0.6		0.6	0.520	0.5367	1.			0.3488	_	
	09:00	12.25	0.6		0.6	Concession in which the Real Property lies in which the Real Property lies in the Real Property	0.2087	1.			0.1052		
	09:01	12.25	0.6				0.0043	1.			0.0027		
22		13.25	0.6	1.050	0.6	0.420	0.0243	1.0			0.0127	0.	
22 23	09:02		0.6	1.030	0.6	0.412	-0.1188	1.0			-0.0612	-0.	
22 23 24	09:02 09:04	13.75	0,01										
22	09:02 09:04 09:05	13.75	0.6	0.900	0.6	0.360	-0.1549	1.0	-0.1549	0.450	-0.0697	-0.	
22 23 24 25	09:04			0.900		0.360	-0.1549 -0.1883	1.0			-0.0697 -0.1092	-0. -1.	



			the state of the s		Date Generated: Thu Sep 27 2012
File N	Information ame Date and Tir		SS05.920.WAD 2011/09/21 08:20:40	Site Details Site Name Operator(s)	NJT
Qual	ity Contro	bl			
St	Loc	%Dep		Message	
1	1.75		High angle: 165 High differences in beam S	NR: 39.1,27.5	
3	2.75		High angle: 57		
4	3.25	0.6	High angle: -20		
5	3.75	0.6	High angle: -25		
6	4.25	0.6	High angle: -37		
10	6.25	0.6	High angle: -21		
13	7.75	0.6	High standard error: 0.065		
18	10.25	0.6	High angle: -25		
24	13.25	0.6	High angle: 71		
25	13.75	0.6	High angle: -154		
26	14.25	0.6	High angle: -172		
27	14.75	0.6	High angle: 170		



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